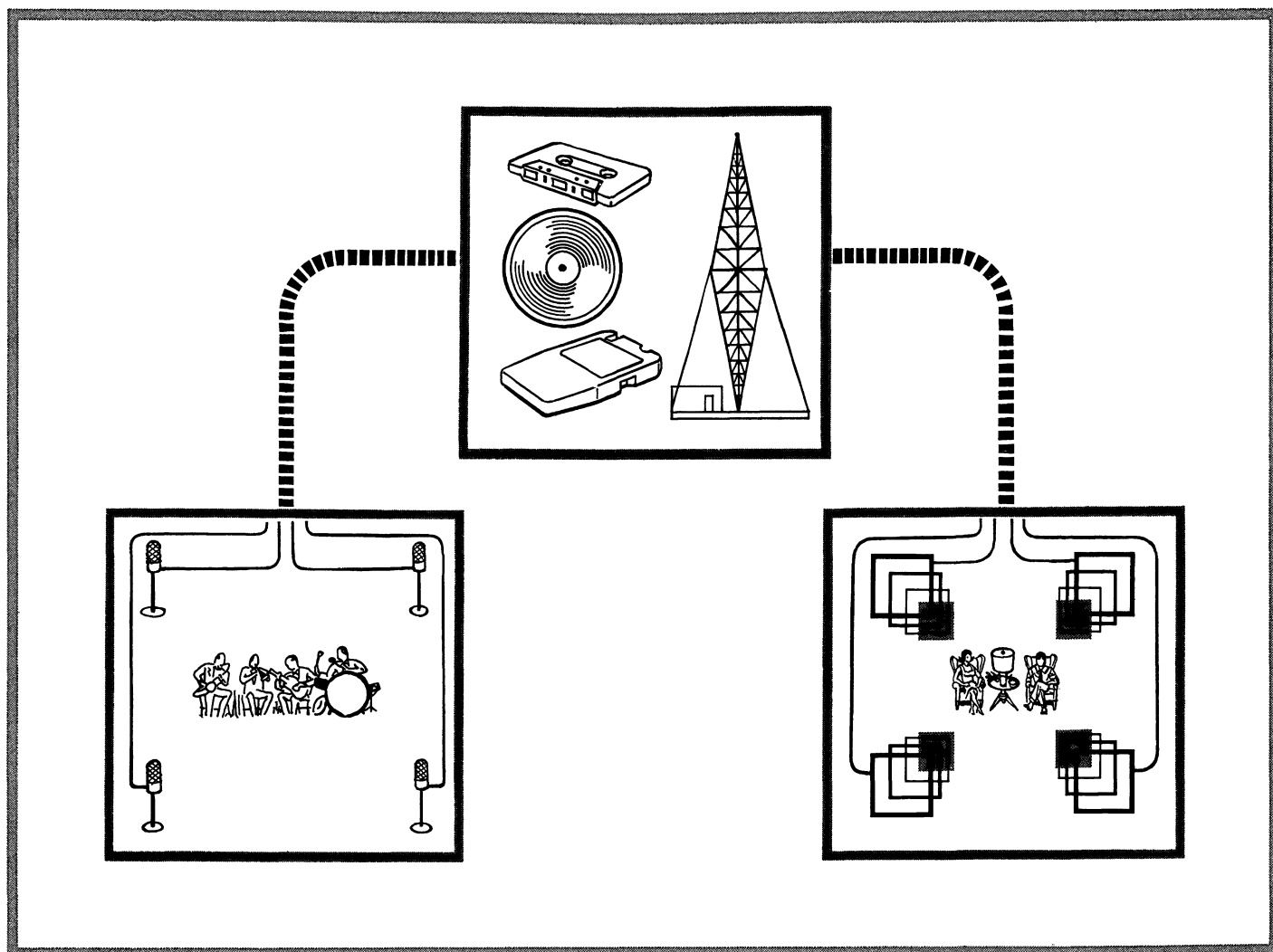


HF-31

HF-31

ZENITH

SERVICE MANUAL



MODULAR AND CONSOLE AUDIO PRODUCTS

ZENITH RADIO CORPORATION

1900 N. AUSTIN AVENUE

CHICAGO, ILLINOIS 60639

To the Service Technician

PRODUCT SAFETY SERVICING GUIDELINES FOR ALL AUDIO AMPLIFIERS AND RADIO RECEIVERS

CAUTION: No modification of the circuit should be attempted. Service work should be performed only after you are thoroughly familiar with all of the following precautions. To do otherwise increases the risk of potential hazards and injury to the user.

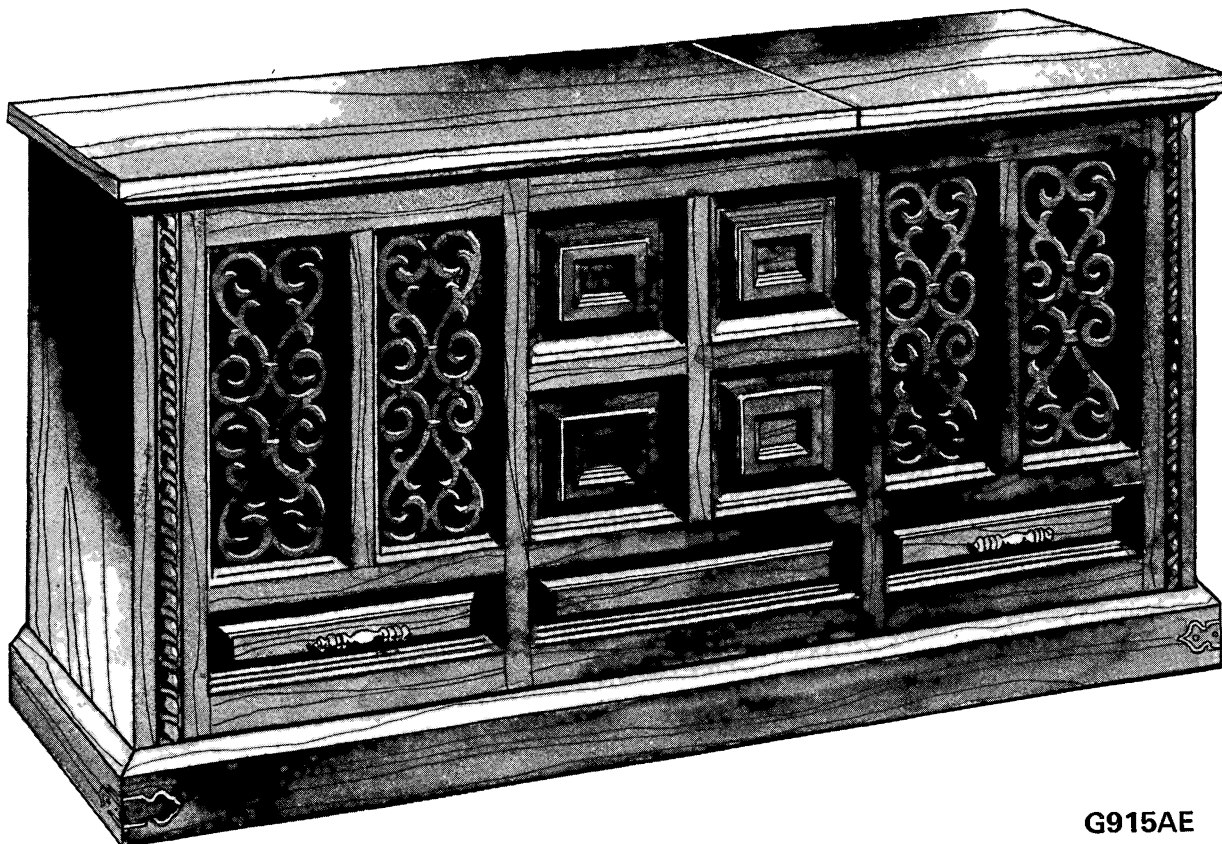
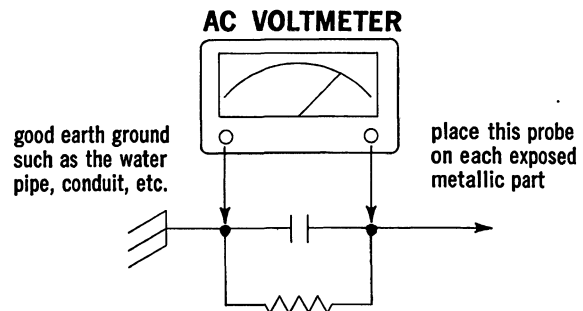
SAFETY CHECKS

SUBJECT: Fire & Shock Hazard

1. Be sure that all components are positioned in such a way to avoid possibility of adjacent components shorts. This is especially important on those chassis which are transported to and from the repair shop.
2. Always replace all protective devices such as insulators and barriers after working on a set.
3. Check for frayed insulation on wires including the AC cord.
4. Check across-the-line components for damage and replace if necessary.
5. After re-assembly of the set always perform an AC leakage test on the exposed metallic parts of the cabinet such as the knobs, antenna terminals, etc. to be sure the set is safe to operate without danger of electrical shock. Do not use a line isolation transformer during this test. Use an AC voltmeter having 5000 ohms per volt or more sensitivity in the following

manner: Connect a 1500 ohm 10 watt resistor, paralleled by .15 mfd. AC type capacitor, between a known good earth ground (water pipe, conduit, etc.) and the exposed metallic parts, one at a time. Measure the AC voltage across the combination 1500 ohm resistor and .15 mfd. capacitor. Reverse the AC plug on the set and repeat AC voltage measurements again for each exposed metallic part. Voltage measured must not exceed .3 volts RMS. This corresponds to 0.2 milliamp AC.

Any value exceeding this limit constitutes a potential shock hazard and must be corrected immediately.



G915AE

REPRESENTATIVE MODEL ILLUSTRATION

INDEX

CHASSIS OR MODEL	INFORMATION ON PAGE	PRIOR DATA CONTAINED IN	CHASSIS OR MODEL	INFORMATION ON PAGE	PRIOR DATA CONTAINED IN
1WDA10	—	HF 26	29CT20	—	HF 22, 24
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1WEA11 (Z1)	—	HF 28S1, 29, 30	29CT21Z2	—	HF 26, 27
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5WER53	—	HF 30	G3000W	37	—
5WFR53	—	HF 30, 30S1	D9011W	—	HF 26, 29, 29S1
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6WGR57	59, 60, 61	—	E9014X (1)	—	HF 29S1, 30
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15WER55	—	HF 29, 29S1, 29S2, 30, 30S1	E9029W	—	HF 29S1
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HF 18 is Part No. 923-558

HF 19 is Part No. 923-606

HF 22 is Part No. 923-642

HF 25 is Part No. 923-669

HF 28 is Part No. 923-718

HF 29S1 is Part No. 923-762

HF 30S1 is Part No. 923-841

HF 18S1 is Part No. 923-576

HF 20 is Part No. 923-610

HF 23 is Part No. 923-646

HF 26 is Part No. 923-702

HF 28S1 is Part No. 923-734

HF 29S2 is Part No. 923-784

HF 18S2 is Part No. 923-592

HF 21 is Part No. 923-626

HF 24 is Part No. 923-653

HF 27 is Part No. 923-707

HF 29 is Part No. 923-740

HF 30 is Part No. 923-809

Solid State Device Theory and Circuit Applications are found in the following Service Manuals:

HF 18: Theory — Diodes (Including Zener and SCR), Transistors, (PNP, NPN, Darlington, and JFET). Applications — Chassis 29AT24 (JFET FM-RF, Multiplex, Electronic Touch Switching), Complementary Symmetry, Chassis 11ZT27 (Electronic Filter).

HF 22: Theory — JFET, IGFET, MOSFET, Applications — Dual Gate MOSFET FM-RF, JFET Bplex Detector, Quasi-Complementary Symmetry.

HF 23: Applications — Model C9029/Chassis 15WCA10 Four Channel Decoder.

HF 26: Applications — Chassis 15WDR51 (JFET Meter Circuit, Multiplex IC, Four Channel Decoding).

HF 27: Applications — Model SD2568 Speaker Switching Circuitry.

HF 28: Applications — Model D9013W Allegro Speaker System.

HF 29: Theory — Light Emitting Diodes (LED), Applications — Three Light Tuning (Target Tuning), Multiplex IC.

HF 29S1: Applications — Snap-off Escutcheon and Out Front Chassis Removal, "E" Line Models.

HF 30: Applications — Snap-off Escutcheon and Out Front Chassis Removal, "F" Line Models.

HF 31: Theory and Applications — Chassis 12WGR59 (Ceramic Filters, IF IC, Quadrature Detector, Interstation Muting, PLL Multiplex IC),

General Product Information — Audio Circuitry (including Two on Two Speaker Matrix, Allegro Speaker Systems), Disassembly Procedures.

PRODUCT FEATURES
SEE NOTES ON PAGE 4

CABINET			CHASSIS		SPEAKERS			RECORD CHANGER	OTHER FEATURES		
MODEL	COLOUR	NOTE A	MODEL	TYPE	PART NUMBER	IMPED. (In Ohms)	QTY. AND SIZE (In Inches)	PART NUMBER	TAPE PROVISION NOTE B	SPEAKER PROVISION NOTE C	MISC. NOTE D
G584W1	Walnut	M,LL	3WGR52	FM/AM/Phono	Note C	—	—	169-511	TM	2 on 2, A1,A2,A3	DGL, H, PL
G587W2	Walnut	M,LL	3WGR52	FM/AM/Phono/ Tape	Note C	—	—	169-511	8TK-P 169-492	2 on 2, A1,A2,A3	DGL, H, PL
GR587W1	Walnut	M,LL	3WGR52	FM/AM/Phono/ Tape	Note C	—	—	169-511	8TK-R/P 169-472	2 on 2, A1,A2,A3	DGL, H, PL
G590W	Walnut	M,LL	6WGR57	FM/AM/Phono/ Tape	Note C	—	—	169-512	8TK-P 169-510 or 169-510A or 169-510B	2 on 2, A1,A2,A3	AUX,DGL, F, H, PL,T
GR590W	Walnut	M,LL	6WGR57	FM/AM/Phono/ Tape	Note C	—	—	169-512	8TK-R/P 169-507 or 169-507A	2 on 2, A1,A2,A3	AUX,DGL, F,H,PL,T
GR591W	Walnut	M,LL	6WGR57	FM/AM/Phono/ Tape	Note C	—	—	169-512	Cass.-R/P 169-519	2 on 2, A1,A2,A3	AUX,DGL, F,H,PL,T
G596W	Walnut	M,LL	12WGR59	FM/AM/Phono/ Tape	Note C	—	—	169-513	8TK-P 169-505 or 169-505A	2 on 2, A1,A2,A3	AUX,F,H, PL,T
GR596W	Walnut	M,LL	12WGR59	FM/AM/Phono/ Tape	Note C	—	—	169-513	8TK-R/P 169-506	2 on 2, A1,A2,A3	AUX,F,H, PL,T
G680W2	Walnut	M	3WGR54	FM/AM/Tape	Note C	—	—	—	8TK-P 169-492	2 on 2, A1,A2,A3	DGL,H,PL
GR684W	Walnut	M	6WGR56	FM/AM/Tape	Note C	—	—	—	8TK-R/P 169-507 or 169-507A	2 on 2, A1,A2,A3	AUX,DGL, H,PL
G904P	Pecan	C,LL	5WFR50	FM/AM/Phono/ Tape	49-1224-01 49-1094	8 45	2-6x9 2-3½	169-502	8TK-P 169-490 or 169-490A	2 on 2 A1,A2,A3	H,RS
G914P	Pecan	C,LL	3WGR50	FM/AM/Phono/ Tape	49-1261-01 49-1237	8 8	2-8 2-3	169-515	8TK-P 169-521 or 169-521A	2 on 2 A1,A2,A3	A,H,PL, RS
G915AE	Antique Oak	C,LL	3WGR50	FM/AM/Phono/ Tape	49-1261-01 49-1237	8 8	2-8 2-3	169-515	8TK-P 169-521 or 169-521A	2 on 2 A1,A2,A3	A,H,PL, RS
G916M	Maple	C,LL	3WGR50	FM/AM/Phono/ Tape	49-1261-01 49-1237	8 8	2-8 2-3	169-515	8TK-P 169-521 or 169-521A	2 on 2 A1,A2,A3	A,H,PL, RS
G920AE	Antique Oak	C,LL	6WGR55	FM/AM/Phono/ Tape	49-1217 49-1166	8 8	2-10 2-3½	169-516	8TK-P 169-521 or 169-521A	2 on 2 A1,A2,A3	A,AUX, H,PL,T, RS

PRODUCT FEATURES
SEE NOTES ON PAGE 4

CABINET			CHASSIS		SPEAKERS			RECORD CHANGER	OTHER FEATURES		
MODEL	COLOR	NOTE A	MODEL	TYPE	PART NUMBER	IMPED. (In Ohms)	QTY. AND SIZE (In Inches)	PART NUMBER	TAPE PROVISION NOTE B	SPEAKER PROVISION NOTE C	MISC. NOTE D
G921P	Pecan	C,LL	6WGR55	FM/AM/Phono/ Tape	49-1217 49-1166	8 8	2-10 2-3½	169-516	8TK-P 169-521 or 169-521A	2 on 2 A1,A2,A3	A,AUX, H,PL,T, RS
G922M	Maple	C,LL	6WGR55	FM/AM/Phono/ Tape	49-1217 49-1166	8 8	2-10 2-3½	169-516	8TK-P 169-521 or 169-521A	2 on 2 A1,A2,A3	A,AUX, H,PL,T, RS
GR936AE	Antique Oak	C,LL	12WGR58	FM/AM/Phono/ Tape	49-1217 49-1166	8 8	2-10 2-3½	169-513	8TK-R/P 169-523 or 169-487	2 on 2 A1,A2,A3	A,F,H, PL,T, RS
GR937P	Pecan	C,LL	12WGR58	FM/AM/Phono/ Tape	49-1217 49-1166	8 8	2-10 2-3½	169-513	8TK-R/P 169-523 or 169-487	2 on 2 A1,A2,A3	A,F,H, PL,T, RS
G1000W	Walnut	M,SP	—	—	49-1249 49-1168	8 8	1-6½ 1-3½	—	—	—	A1
G2000W	Walnut	M,SP	—	—	49-1254-01 49-1168	8 8	1-8 1-3½	—	—	—	A2
G3000W	Walnut	M,SP	—	—	49-1265 49-1168	8 8	1-10 1-3½	—	—	—	A3
G9019W	Walnut	M,SP	—	—	49-1241 49-1168	8 8	1-10 1-3½	—	—	—	A
G9026W	Walnut	M	—	—	—	—	—	169-512	—	—	—

PRODUCT FEATURES

RECORD CHANGER FEATURES

Part No.	Mfg. Code	Stylus Pressure - Grams -	Cartridge & Stylus	45 RPM Adapter	Turntable		Record Size/ Selector	Record Stack Capacity	Base-Plate Color	Turntable Pad Color	Pressure Arm Color	Misc. Features
					Speeds RPM	Diameter Inches						
169-502	VM 1272	2-2.9	142-167 D-S S-82621	S-82964	16, 33, 45, 78	11"	7, 10, 12, M Manual	1/2"	Black	Black	Black	Cue Lever
169-511	BSR	2-2.9	142-182 D 56-632	S-72910	33, 45, 78	11"	7, 10, 12 Manual	1/2"	Black	Black	Black	Cue Lever
169-512	BSR	2-2.9	142-182 D 56-632	S-72910	33, 45, 78	11"	7, 10, 12 Manual	1/2"	Black	Black	Black	Cue Lever
169-513	BSR	2-2.9	142-182 D 56-632	S-72910	33, 45, 78	11"	7, 10, 12 Manual	1/2"	Black	Black	Black	Cue Lever
169-515	VM	2-2.9	142-182 D 56-632	S-82964	16, 33, 45, 78	11"	7, 10, 12 Auto	1/2"	Black	Black	Black	Cue Lever
169-516	VM	2-2.9	142-182 D 56-632	S-82964	16, 33, 45, 78	11"	7, 10, 12 Auto	1/2"	Black	Black	Black	Cue Lever

NOTE: All record changers have 120VAC motors. See "Misc Features" for those with overwinds. D = Diamond, S = Manufactured Sapphire.

NOTES

NOTE A – CABINET STYLE:

C = Console, M = Modular, LL = Lift Lid, SP = Speaker System.

NOTE B – TAPE INPUT AND OUTPUT PROVISION:

Factory Installed: 8 TK = Eight Track Cartridge,
Cass = Cassette, P = Play, R = Record,
TM = Top of Set Model for installation with the designated console of modular models:
Model F635 - Cartridge Tape Player.
Model E637 - Cassette Tape Player/ Recorder.
Model F638 - Cartridge Tape Player/Recorder.

NOTE C – SPEAKER PROVISIONS:

2 on 2 = Speaker Matrix or Conventional Stereo Extension Speaker System Provisions.
A1 = Model G1000W Allegro 1000 Speaker System may be used.
A2 = Model G2000W Allegro 2000 Speaker System may be used.
A3 = Model G3000W Allegro 3000 Speaker System may be used.

NOTE: Models G1000W, G2000W, and G3000W (and the prior E9012 series) are 8 ohm Allegro Speaker Systems. Allegro Models in the E9014 and E9018 series were 16 ohm systems.

NOTE D – MISCELLANEOUS FEATURES:

A = Speaker System is Allegro.
A1 = Speaker System is Allegro 1000.
A2 = Speaker System is Allegro 2000.
A3 = Speaker System is Allegro 3000.
AUX = Auxiliary input accepts Record Changer Model E9026W or Tape Units listed under Note B.
DGL = Digilite Dial Scale.
F = Flywheel Tuning.
H = Headphone Jack (Stereo).
HH = Headphone Jack (Four Channel).
PL = Power Indicator Light.
RS = Record Storage.
T = Tuning Meter.

SECTION TWO

GENERAL INFORMATION

THEORY

From time to time Zenith includes the use of new components and circuit applications in product design. Theory and explanation of such components and circuits is included in various manuals. Refer to the index on page 1 for further information.

CIRCUIT BOARD COMPONENT IDENTIFICATION

In order to assist the Service Technician, most circuit boards are marked to identify the location of components, test points, etc., using the schematic reference symbols and numbers. We have also prepared a drawing of the foil side of the circuit board showing the relationship between the components and the foil. This will aid the Technician in quickly tracing circuits, as not only are the components shown, but also the voltages at various check points. Components are identified by a letter/number combination. A letter prefix to indicate the type of component: C=Capacitor, L=Coil, R=Resistor, CR=Diode, etc. The numbers are assigned, in blocks, to identify the circuit in which it is used:

Block	Stage	Example
1 - 99	FM Tuner	R1, C1, L1.
101 - 199	AM Tuner	R101, C101, L101.
201 - 299	IF	R201, C201, L201.
301 - 399	Multiplex	R301, C301, L301.
401 - 449	Audio, Right Channel	R401, C401, L401.
451 - 499	Audio, Left Channel	R451, C451, L451.
501 - 599	Power Supply	R501, C501, L501.
601 - 699	Switching Circuits	R601, C601, L601.
701 - 799	Special Applications	R701, C701, L701.
801 - 849	Audio, Right Back Channel	R801, C801, L801.
851 - 899	Audio, Left Back Channel	R851, C851, L851.

POWER AMPLIFIERS

When servicing these products, the Service Technician must consider the following:

1. Each channel of the following amplifiers use a pair of matched power transistors in the final output stage. Therefore, should one transistor fail, both transistors must be replaced simultaneously, since they will not perform properly unless matched. (In chassis using complementary symmetry circuits a matched pair consists of one NPN and one PNP transistor.): 3WGR50, 3WGR52, 3WGR54, 5WFR50, 6WGR55, 6WGR56, 6WGR57, 12WGR58, 12WGR59.
2. When a power transistor is replaced the insulator (when used) between the transistor and the heat sink should also be replaced. On the following be certain to apply Dow Corning No. 340 heat conductive grease between the

transistor and the insulator. Also between the insulator and the chassis. The Dow Corning grease can be obtained in 1 c.c. quantities by ordering Part No. 205-5 1: 3WGR50, 3WGR52, 3WGR54, 5WFR50, 6WGR55, 6WGR56, 6WGR57, 12WGR58, 12WGR59.

3. Do not operate these amplifiers without their proper speaker load.
4. Do not short out the audio output of either channel when the amplifier is operating.
5. Should a power transistor fail (short) be certain to replace the emitter resistors for the specific channel. Also be certain to check the condition of the silicon diode rectifiers, and driver transistors.
6. Remove plug-in transistors from their sockets before doing any soldering to the socket lugs.

SIGNAL STRENGTH CHART

There are certain minimum voltages necessary for proper stereo FM reception. To help determine if there is sufficient signal available, the following developed AGC voltage versus micro-volt input voltage charts have been compiled. Since the desired FM Station may not always be operating in the stereo mode when an installation is made, these AGC voltage measurements have been taken with a monaural FM signal. The point "*" of minimum AGC voltage necessary for good stereo FM reception has been indicated on these charts.

AGC voltages are to be measured with a V.T.V.M. connected to the following Test Points.

Chassis 3WGR50, 3WGR52, 3WGR54, 5WFR50 — Test Point "C" at base of Q1; located between Transistors Q101 (A.M. Converter) and Q201 (1st I.F.)

Chassis 6WGR55, 6WGR56, 6WGR57 — Test Point at junction of R2 and R229; either end of orange wire at pulley end of gang.

Chassis 12WGR58 — Test Point at junction of R2 and R229; either end of violet wire at pulley end of gang.

Chassis 12WGR59 — AGC voltages do not provide significant information.

**Chassis 3WGR50, 3WGR52,
3WGR54, 5WFR50**

**Chassis 6WGR55,
6WGR56, 6WGR57**

Chassis 12WGR58

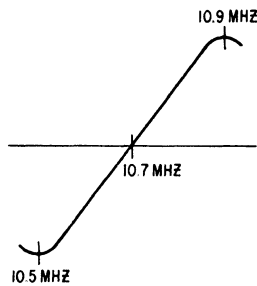
Micro Volts Input	Voltage AGC Voltage at Test Point "C"	Micro Volts Input	Reverse AGC Voltage _{eq} At Gate 2 of FM RF	Micro Volts Input	Reverse AGC Voltage At Gate 2 of FM RF
0	1.23	0	5.4	0	5.7
25	1.10	25	4.5	25	4.5
100	0.88	100	3.3	100	2.8
200	0.79	200	2.85	200	2.2
500	0.71	500	2.5	500	1.5
1K	*0.67	1K	*2.1	1K	*-0.96
5K	0.60	5K	1.22	5K	-0.22
50K	0.12	50K	0.15	50K	-1.10
100K	0.06	100K	-0.08	100K	-1.20

**MINIMUM RATED POWER OUTPUT PER CHANNEL INTO 8 OHMS
(SINE WAVE CONTINUOUS AVERAGE POWER - OFTEN CALLED RMS POWER)**

Chassis	Number of Channels	Watts Per Channel	Power Bandwidth	Total Harmonic Distortion (THD) No More Than
3WGR50	2	2.5	100Hz - 10kHz	1.0%
3WGR52	2	2.5	100Hz - 10kHz	1.0%
3WGR54	2	2.5	100Hz - 10kHz	1.0%
6WGR55	2	6.0	80Hz - 12kHz	1.0%
6WGR56	2	6.0	80Hz - 12kHz	1.0%
6WGR57	2	6.0	80Hz - 12kHz	1.0%
12WGR58	2	12.0	40Hz - 15kHz	1.0%
12WGR59	2	12.0	40Hz - 15kHz	0.5%

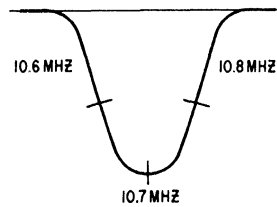
SECTION THREE

FM/AM/MULTIPLEX ALIGNMENT



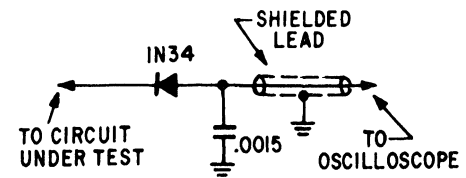
Scope Pattern A — Ratio Detector

Adjust for maximum amplitude while maintaining linearity and symmetry. 10.7 MHz marker must be on the curve at base line.



Scope Pattern-B — IF

10.6 and 10.8 MHz markers must be symmetrically positioned with 10.7 MHz at center of curve. This point must be adjusted for maximum.



Detector Probe - C

If your oscilloscope is not equipped with a detector probe, one can easily be constructed. For best results the probe should be shielded.

GENERAL

These receivers have been properly aligned at the factory and normally will not require further adjustment. As a result, it is not recommended that any attempt be made to alter the stages. If any components are replaced or if anyone tampers with the adjustments, realignment may be necessary.

FM ALIGNMENT

Because of the wide band pass required in a FM Multiplex tuner, it is desirable to use an FM signal generator having a deviation of 400 kHz as well as an oscilloscope, when aligning both the FM IF and RF portions of this receiver. It is not only necessary to obtain maximum amplitude in the IF amplifier stages, but also necessary to maintain symmetry. It is desirable to use 10.6, 10.7 and 10.8 Megahertz markers in obtaining IF curve symmetry.

Capacitors mentioned in the alignment procedure should be as small in size as possible and the ground lead of the generator must be connected to ground as close as possible to the point of injection.

AM ALIGNMENT

A V.T.V.M. on low AC scale connected across the speaker voice coil output terminals (either left or right channels), will be satisfactory for AM, IF and RF adjustments.

MULTIPLEX ALIGNMENT

Before any attempt is made to align, or service, FM Multiplex circuitry, the technician must be certain that the RF, IF, and Detector alignment is correct, and that the receiver functions normally on monaural signals.

Most Multiplex generators are excellent troubleshooting devices because they provide a composite Multiplex signal as well as an RF signal (which is FM modulated by the composite multiplex signal). The composite signal is very useful since it can be used in signal tracing the Multiplex portion of the receiver. We do not recommend that Multiplex alignment be

made using the composite signal injected at the output terminal of the Detector since there is always some phase shift occurring in the RF, IF or Detector circuits. As a result, Multiplex alignment made by a signal injected at the Ratio Detector input would not be correct. For proper Multiplex alignment the composite signal must FM modulate the RF carrier and then be fed into the FM antenna terminals. With the signal injected in this manner, the Multiplex alignment would then be the best that could possibly be obtained.

RF signals should be injected at a point in the FM band where no signal is present. If at all possible this should be at a frequency near the middle of the FM band. Tune the FM receiver to this point and adjust the RF frequency adjustment on the generator to this same frequency. The AGC voltage developed in the receiver should be maximum. AGC voltage substantially less than this may indicate the RF frequency adjustment is tuned to an image.

GENERAL TROUBLE-SHOOTING PROCEDURE

Should a problem arise in aligning the FM Multiplex portion of the receiver, the technician must determine whether the difficulty lies in the RF, IF, and Detector portions of the receiver, or whether the difficulty lies in the Multiplex portion. The composite output of the multiplex generator can be injected at the output of the Detector to help determine the area of difficulty. To reduce possible extraneous signals coming through a Ratio Detector, short the Ratio Detector primary with a jumper lead. The wave forms and their magnitude may vary slightly from chassis to chassis, however, they are quite indicative of what will be seen when signal tracing the Multiplex circuitry.

If all the waveforms are similar in form and magnitude to those indicated, it can be assumed that the Multiplex portion of the receiver is functioning properly and the problem lies ahead of this in the FM receiver. If any of the waveforms are missing at a latter point but are apparent at a previous point, circuitry between the two test points should be checked.

RF AND IF ALIGNMENT PROCEDURE

CHASSIS 3WGR50, 3WGR52, 3WGR54, 5WFR50, 6WGR55, 6WGR56, 6WGR57

STEP	CONNECT GEN ERATOR TO	DUMMY ANTENNA	CONNECT VTVM/ SCOPE TO	INPUT SIGNAL FREQUENCY	SET DIAL TO	ADJUST	PURPOSE	
NOTE: For AM Alignment Use A Signal With 400 Hertz Modulation, Bandswitch In AM.								
1	One turn loosely coupled to wavemagnet.	None	VTVM Speaker Voice Coil	455 KHz	600 KHz	L203, L204 (T202) L207 (T204) L210 (T206)	Align IF channel for maximum output.	
2				1600 KHz	1600 KHz	C1G	Set Oscillator to dial scale.	
3				600 KHz	600 KHz	T101		
4				Repeat Steps No. 2 & 3 for minimum change.				
5				1400 KHz	1400 KHz	C1D	Align Antenna stage.	
NOTE: For FM Alignment Use A Signal With 400 KHz Deviation, Bandswitch In FM. AFC "Off".								
6	Term. No. 5 of T205 3rd IF Trans. Test Point "G"	47 ohm in shunt with gen. output. Then from hot lead a 27 ohm in series with a .001 MF capacitor.	Scope Ratio Detector Test Point "H"	10.7 MHz	Gang Closed	L212 (T207)	Adjust Primary and Secondary of Ratio Detector for maximum amplitude and symmetry as shown in Scope Pattern "A".	
7						L214 (T207)		
8	Term. No. 3 of T203 2nd IF Trans. Test Point "F"		Scope Last FM IF Test Point "G"			L208 & L209 (T205)	Align I.F. transformer for maximum output and symmetry. This pattern is not necessarily identical to the overall Scope Pattern "B".	
9	Term. No. 3 of T201 1st IF Trans. Test Point "E"					L205 & L206 (T203)		
10	Test Point "D"					L201 & L202 (T201)		
11						Readjust L201, L202, L205, L206, L208, L209		Align I.F. transformer for maximum output and symmetry as indicated in Scope Pattern "B".
NOTE: In Steps 10 and 11 Generator Ground MUST be Connected On Braid As Close To Gang As Possible.								
12	FM Antenna Post (Disconnect Antenna) Test Point "A"	300 ohm	Scope Last FM IF Test Point "G"	106 MHz	106 MHz	C13	Set Oscillator to dial scale.	
13				90 MHz	90 MHz	L4		
14				Repeat Steps 12 and 13 for minimum change.				
15				106 MHz	106 MHz	C1A	Align FM Detector stage for maximum.	
16				90 MHz	90 MHz	L2 if necessary		
17				106 MHz	106 MHz	C1H	Align FM Antenna stage for maximum.	
18				90 MHz	90 MHz	L1 if necessary		
19				Repeat Steps 15 thru 18 for minimum change.				
NOTE: The Following Applies Only To Chassis 6WGR55, 6WGR56, 6WGR57, No Signal Input.								
20	None	None	None	None	None	R233	Zero center tuning meter.	

MULTIPLEX ALIGNMENT PROCEDURE

CHASSIS 3WGR50, 3WGR52, 3WGR54, 5WFR50, 6WGR55, 6WGR56, 6WGR57

Before Aligning or Servicing Multiplex Circuits Be Certain That RF, IF And Ratio Detector Are Correctly Aligned And That Operation Is Normal On Monaural FM Signals.

Normal On Monaural FM Signal:							
STEP	CONNECT GENERATOR TO	DUMMY ANTENNA	CONNECT SCOPE AND/OR ACVTVM	INPUT SIGNAL FREQUENCY	SET DIAL TO	ADJUST	PURPOSE
NOTE: Place Bandswitch In FM STEREO Position.							
1	FM Antenna Post (Disconnect Antenna) Test Point "A"	300 ohm	Test Point "M"	98 MHz 10% Pilot	98 MHz	T301	Adjust 19 kHz Amp for maximum.
2				98 MHz 5% Pilot		R302	Adjust mute control to point where stereo lamp lights up.
3			"L" Tape Output	98 MHz 10% Pilot L+R, L-R, (Mod. L. Only)		T302	Adjust for maximum L Channel Reading
4			"R" Tape Output			T302 if necessary	Adjust for minimum R Channel Reading
5				Repeat Steps 4 and 5 for minimum change.			To provide maximum separation.

RF AND IF ALIGNMENT PROCEDURE – CHASSIS 12WGR58

STEP	CONNECT GENERATOR TO	DUMMY ANTENNA	CONNECT VTVM/ SCOPE TO	INPUT SIGNAL FREQUENCY	SET DIAL TO	ADJUST	PURPOSE			
NOTE: For AM Alignment Use A Signal With 400 Hertz Modulation, Bandswitch In AM.										
1	One turn loosely coupled to wavemagnet.	None	VTVM Speaker Voice Coil	455 KHz	600 KHz	L203, L204 (T202) L207, L215 (T204) L210 (T206)	Align IF channel for maximum output.			
2				1600 KHz	1600 KHz	C1K	Set Oscillator to dial scale.			
3				600 KHz	600 KHz	L103 (T102)				
4				Repeat Steps No. 2 and 3 for minimum change.						
5				1400 KHz	1400 KHz	C1H	Align RF stage.			
6				600 KHz	600 KHz	L106 (T101)				
7				Repeat Steps No. 5 and 6 for minimum change.						
8				1400 KHz	1400 KHz	C1F	Align antenna stage.			
NOTE: For FM Alignment Use A Signal With 400 KHz Deviation, Bandswitch In FM, AC "Off".										
9	Term. No. 5 of T205 3rd IF Trans. Test Point "G"	47 ohm in shunt with generator output. Then from hot lead a 27 ohm in series with a .001 MF Capacitor.	Scope Ratio Detector Test Point "H"	10.7 MHz	Gang Closed	L212 (T207)	Adjust Primary and Secondary of Ratio Detector for maximum amplitude and symmetry, as shown in Scope Pattern "A".			
10						L214 (T207)				
11	Term. No. 3 of T203 2nd IF Trans. Test Point "F"		Scope Last FM IF Test Point "G"			L208 & L209 (T205)	Align I.F. Transformer for maximum output and symmetry. This pattern is not necessarily identical to the overall Scope Pattern "B".			
12	Term. No. 4 of T201 1st IF Trans. Test Point "E"					L205 & L206 (T203)				
13	Test Point "D"					L201 & L202 (T201)				
14						Readjust L201, L202, L205, L206, L208 & L209	Align I.F. Transformer for maximum output and symmetry as indicated in Scope Pattern "B".			
NOTE: In Steps 13B and 14B Generator Ground Must Be Connected On Braid As Close To Gang As Possible.										
15	FM Antenna Post (Disconnect Antenna) Test Point "A"		300 ohm			Scope Last FM IF Test Point "G"	106 MHz	106 MHz	C13	Set Oscillator to dial scale.
16		90 MHz		90 MHz	L4					
17		Repeat Steps 15 and 16 for minimum change.					Align FM Detector stage for maximum.			
18		106 MHz		106 MHz	C1C					
19		90 MHz		90 MHz	L2 if necessary					
20		106 MHz		106 MHz	C1A		Align FM Antenna stage for maximum.			
21		90 MHz		90 MHz	L1 if necessary					
22		Repeat Steps 15 thru 21 for minimum change.								
23	None	None	None	None	None	R233	Zero center tuning meter.			

FM—MULTIPLEX ALIGNMENT PROCEDURE – CHASSIS 12WGR58

Before Aligning Or Servicing Multiplex Circuits Be Certain That RF, IF, And Ratio Detector Are Correctly Aligned And That Operation Is Normal On Monaural FM Signals.

STEP	CONNECT GENERATOR TO	DUMMY ANTENNA	CONNECT SCOPE AND/OR VTVM	INPUT SIGNAL FREQUENCY	SET DIAL TO	ADJUST	PURPOSE
NOTE: Place Bandswitch In FM Position And Stereo/Mono Switch In Stereo.							
1	FM Antenna Post (Disconnect Antenna) Test Point "A"	300 ohm	VTVM(DC) Doubler Test Point "N"	98 MHz, 10% Pilot	98 MHz	T301, T302, R308	Adjust 19 kHz Amp and Doubler for maximum.
2				98 MHz, 5% Pilot		R308	Adjust mute control to point where stereo lamp lights up.
3			VTVM(AC) "L" Audio Output (After 38kHz filter)	98 MHz, 10% Pilot L+R, L-R, (Mod. L Only)		T303	Adjust 38 kHz Detector for maximum at "L" Output. NOTE:—"L" Output should be approximately 10 (or greater) times "R" Output.
4			VTVM(AC) "R" Audio Output (After 38kHz filter)	Check "R" channel output.			

RF, IF AND MPX ALIGNMENT PROCEDURE FOR CHASSIS 12WGR59

STEP	CONNECT GENERATOR TO	DUMMY ANTENNA	CONNECT VTVM/ SCOPE TO	INPUT SIGNAL FREQ.	SET DIAL TO	ADJUST	PURPOSE		
NOTE: For AM Alignment Use A Signal With 400 Hertz Modulation, Bandswitch In AM.									
1	One Turn Loosely coupled to AM Wave magnet Antenna	None	VTVM Speaker Voice Coil	455 KHz	Gang Closed	L203, L204 (T202)	Align IF for maximum output.		
2						L207, L208 (T203)			
3						L209 (T204)			
4						1600 KHz	1600 KHz	C109	Set Oscillator to dial scale.
5						600 KHz	600 KHz	L105 (T102)	
6						Repeat Steps No. 4 & 5 for minimum change.			Align RF stage.
7						1400 KHz	1400 KHz	C1H	
8						600 KHz	600 KHz	L103 (T101)	
9						Repeat Steps No. 7 & 8 for minimum change.			Align Antenna stage.
10						1400 KHz	1400 KHz	C1F	
11						600 KHz	600 KHz	L101 if necessary	
12						Repeat Steps 10 & 11 for minimum change.			
NOTE: For FM IF Alignment Use A Signal Of 250 KHz Deviation, 50 Hertz Modulation For Full Bandpass Display. FM In MONO, AFC OFF, Preset R213, R308 and R317 To Mid Rotation Before Connecting Generator. Connect Generator Cable Ground To Gang Frame.									
13	Test Point "D" FM IF Input	47 Ohm in shunt with gen. output. Then from hot lead a 27 Ohm in series with a .01 MF capacitor. See Fig. 1.	Scope Test Point "G" Thru Diode Detector Probe, See Fig. 2.	10.7 MHz	Gang Closed	L201, L202 (T201)	Align I.F. transformer for maximum output and symmetry as indicated in Scope Pattern "B".		
NOTE: For FM Detector Alignment Use A Signal Of 75 KHz Deviation, 1 KHz Modulation. Also Connect Generator Modulation Frequency To Scope Horizontal. Adjust Generator IF Frequency To Center Total Bandpass Waveform. Do Not Change Generator IF Frequency For Remainder Of IF Alignment. (If Your Generator Does Not Provide Output For Audio Modulation Frequency Use Horizontal Output From Generator, Or Scope Horizontal Sweep, And Follow Step 14C.) Minimum Distortion Can Only Be Achieved By Use Of Step 14A Below.									
14	Test Point "D" FM IF Input	47 Ohm in shunt with gen. output. Then from hot lead a 27 Ohm in series with a .01 MF capacitor.	A. Distortion Analyzer (thru a 100 usec de-emphasis network) and/or Scope. See Fig. 3.	Center Frequency of Ceramic Filters Y201 and Y202. See Fig. 4.	Gang Closed	L205	A. Preferred Method: Distortion Analyzer at Test Point "H" should read minimum distortion, approx. 50 to 55 dB below 0 dB set level.		
			B. Scope				B. Alternate Method: Adjust L205 for linear scope trace - no curve at ends of trace. Disregard meter reading.		
			C. Scope				C. Alternate Method: Adjust L205 for maximum length and symmetry, Similar to Scope Pattern "A".		
			Test Point "H"						
15						R213	Adjust for center reading on Tuning Meter.		
16	Test Point "A" FM Antenna Post (Disconnect Antenna)	300 Ohm		106 MHz	106 MHz	C15	Set Oscillator to dial scale.		
17				90 MHz	90 MHz	L4			
18				Repeat Steps 16 & 17 for minimum change.					
19				106 MHz	106 MHz	C1C	Align FM Detector stage for maximum.		
20				90 MHz	90 MHz	L2 if necessary			
21				106 MHz	106 MHz	C1A	Align FM Antenna stage for maximum.		
22				90 MHz	90 MHz	L1 if necessary			
23				Repeat Steps 19 thru 22 for minimum change.					

RF, IF, AND MPX ALIGNMENT PROCEDURE FOR CHASSIS 12WGR59 – CONT'D.

STEP	CONNECT GENERATOR TO	DUMMY ANTENNA	CONNECT VTVM/SCOPE TO	INPUT SIGNAL FREQ.	SET DIAL TO	ADJUST	PURPOSE
NOTE: Apply Sufficient Signal Level — Approx. 100 Microvolts — To Obtain Full Limiting At Point Near 98 MHz.							
24	Test Point "A" FM Antenna Post (Disconnect Antenna)	300 Ohm	Scope Test Point "H"	98 MHz	98 MHz	—	Turn Modulation "ON". Adjust generator RF frequency to obtain center indication on Tuning Meter. Adjust VTVM for "0" dB reading.
25							Turn modulation "OFF". Reduce RF level to get -4.5 dB quieting (approx. 3 to 4 microvolts).
26						R308	Turn Mute "ON". Rotate R308 (Mute) full clockwise. Audio will mute. Slowly adjust R308 counter-clockwise until audio just turns "ON". Do not over adjust. This will be approximately 45 dB S/N. To check, tune generator off frequency and then back on frequency from both sides.
27			Frequency Counter and/or Scope Test Point "M"	No Signal Input. Mute "ON".		R317	A. Frequency Counter should read 19 KHz, ± 100 Hz. B. Alternate Method: Connect Test Point "M" Signal to scope vertical and an accurate 19 KHz signal to scope horizontal input. Adjust R317 for one square synchronized waveform.
28			Scope and/or AC VTVM Left Tape Output	98 MHz 10% Pilot (L+R) (L-R) (L Only)		—	Check for separation. Maximum left output.
29			Right Tape Output.				Check for separation. Minimum right output.
NOTE: Do Not Readjust Control R317 After Step 27.							

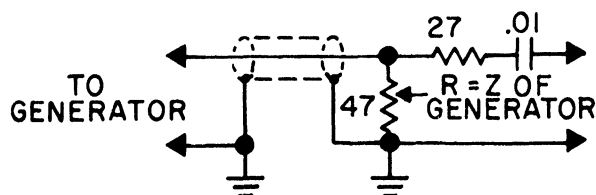


FIGURE 1 – RF INPUT PROBE

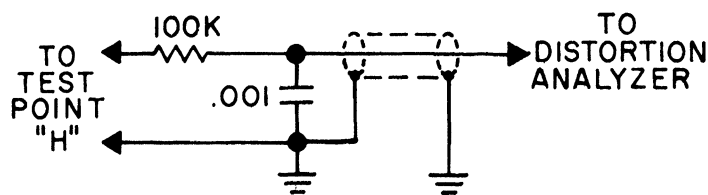


FIGURE 3 – DE-EMPHASIS PROBE

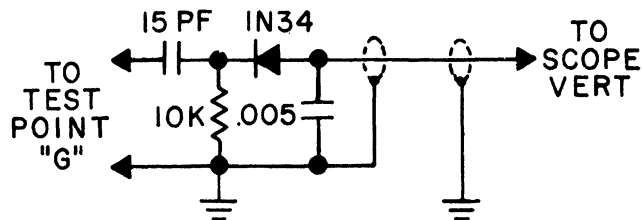


FIGURE 2 – DIODE DETECTOR PROBE

CERAMIC FILTERS – CHASSIS 12WGR59			
PART NO.	COLOR CODE	NOMINAL CENTER FREQUENCY	FREQUENCY RANGE
224-1	Black	10.64 MHz \pm	10.61 to 10.67 MHz
224-1-01	Blue	10.67 MHz \pm	10.64 to 10.70 MHz
224-1-02	Red	10.70 MHz \pm	10.67 to 10.73 MHz
224-1-03	Orange	10.73 MHz \pm	10.70 to 10.76 MHz
224-1-04	White	10.76 MHz \pm	10.73 to 10.79 MHz

FIGURE 4 – CERAMIC FILTER TABLE

NOTES

SECTION FOUR

THEORY AND APPLICATIONS

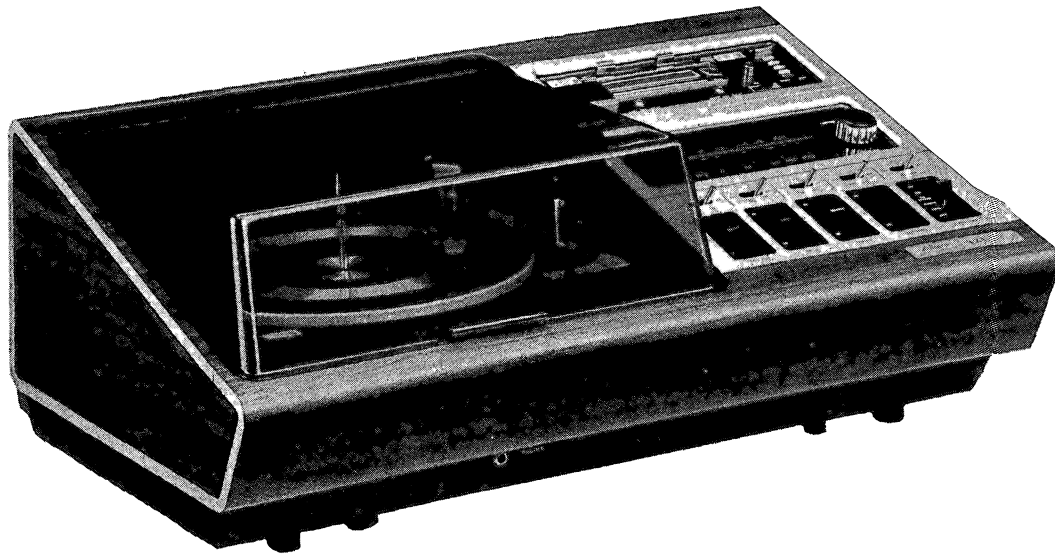


FIGURE 1 – MODEL GR596W

INTRODUCTION

Chassis 12WGR59 (Used in Models G596W and GR596W) incorporates several features which are new to Zenith's Stereo Audio Product Line. These features include:

1. Cabinet Styling (See Figure 1).
2. Separate IF circuits for AM and FM (See Block Diagrams in Figures 2 and 3).
3. Improved Sensitivity and Selectivity.
4. AM Oscillator Trimmer mounted separately (C109).
5. FM IF uses Two Ceramic Filters (Y201 and Y202 and only one IF Transformer - T201).
6. FM IF Gain Block in IC201.
7. FM IF Limiter and Quadrature Detector in IC202 (only one coil, - L205).
8. FM Interstation Muting.

9. Phase Locked Loop (PPL) Multiplex Detector (IC301) (one variable resistor adjustment - R317).

AM RF/IF/AGC

As shown in the Block Diagrams of Figures 2 and 3 and the partial Schematic of Figure 5, the AM and FM no longer share common IF circuitry. The AM has one NPN transistor used in a common emitter TRF circuit (Q101) and a second NPN transistor used as Converter (Q102). This is followed by a conventional, two NPN transistor, AM IF circuit (Q202, Q203). A voltage divider consisting of R219, R220, etc., connected between AM B+ and ground, establishes a reference bias for the RF and IF transistors under no signal conditions. In addition to being AM Detector, Diode CR205 also provides AM AGC voltage for the base of the 1st AM IF transistor (Q202). Voltage developed at the emitter of Q202 is fed via R106 providing reverse AGC to the base of AM RF transistor Q101.

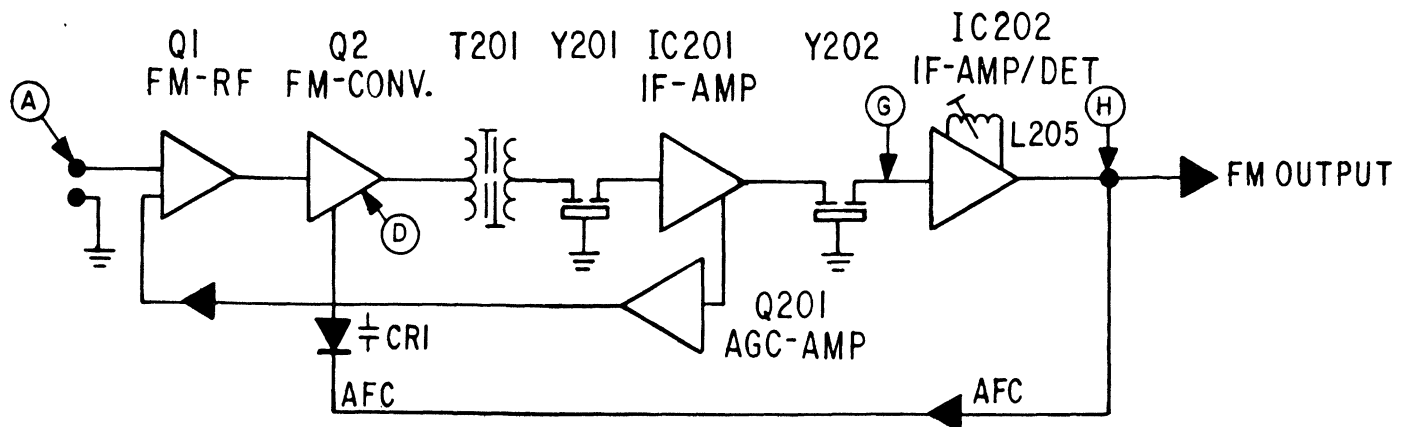


FIGURE 2 – CHASSIS 12WGR59 – FM RF/IF BLOCK DIAGRAM

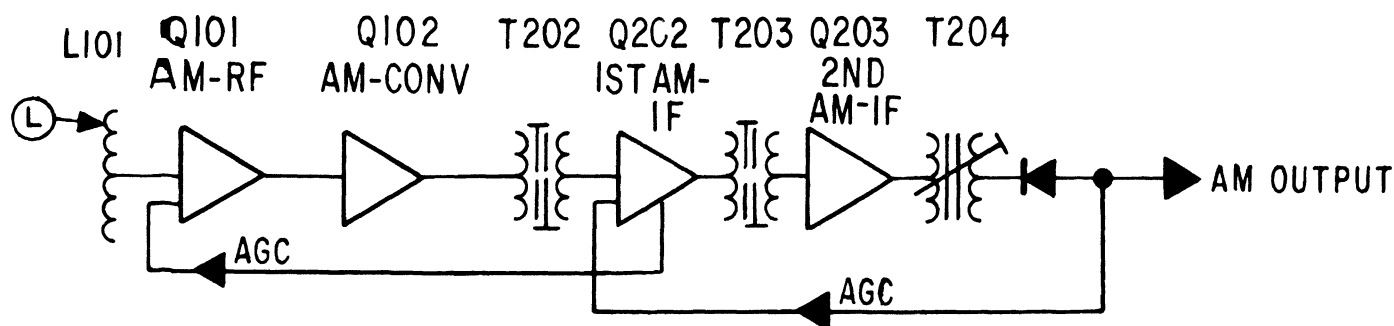


FIGURE 3 – CHASSIS 12WGR59 AM RF/IF BLOCK DIAGRAM

When B+ is applied to the AM RF / IF, a portion of that voltage is applied via R107 and R318 to forward bias CR303, placing a positive voltage on pin 14 of IC301. This will turn off the oscillator in the FM Multiplex Chip IC301, thereby preventing possible "birdies" when turned to AM.

FM - RF

Q1, the RF amplifier, is a Dual Insulated Gate MOS Field Effect Transistor (See Figure 5). FM Antenna coil (L1), FM RF coil (L2), and Oscillator coil (L4) are all precisely tuned to insure that the tuner will reject unwanted and undesired combinations of RF signals present in many areas due to today's complex communication systems. Coil L3 is part of a 10.7 Megahertz trap in the emitter lead to the Converter transistor (Q2).

Under no signal conditions voltages are applied as follows to the MOSFET elements. Resistors R3 and R6 form a voltage divider across the B+ line providing a fixed bias to Gate 1 (G1). The FM RF signal from L1 is also applied to G1. A second voltage divider consisting of R15, R201, and R202 associated with the voltage doubler circuit of CR202 and CR203 provides fixed bias of 5.6 volts, via R203 and R2 to Gate 2 (G2) under no signal conditions. Drain voltage is applied, from B+ via the RF coil L2.

At this point lets recap the existing voltage conditions:

- Gate 1 to Source - approx. -0.3 volts
- Gate 2 to Source - approx. $+3.6$ volts
- Drain to Source - approx. $+7.8$ volts
- Drain current - approx. 10 milliamp.

(A variation can be expected due to circuit component tolerances.)

As the gain of the IF stages increases, reverse AGC voltage will be developed at diodes CR202 and CR203, and applied to the Gate terminal (G2) of the FET. This increasing AGC voltage, when added to the gate bias voltage, will cause the gate voltages to be more negative, driving the FET toward cut-off. When this occurs, the current flow is reduced, thereby reducing the FET's gain. This stage is designed for optimum circuit performance and minimum noise. In this application, the drain current is at approximately one-half of the saturation current ($IDSS$).

MOSFET PROTECTION

When these devices are being handled out of circuit, it is possible for static charges to build up between gate and source. This charge could reach a value which would exceed the gate breakdown voltage. To reduce this condition, MOSFET'S of early design would be shipped with all leads twisted together, or with a wire wrapped around all leads. Since all leads were shorted together, there should be no impedance across which a voltage could develop.

While the above method was effective, it could be eliminated if protection were included within the FET package. A schematic of the internal configuration of such a package is shown in Figure 4. You will note back-to-back zener diodes connected from each gate to the source. These back-to-back diodes are diffused into the FET while it is being constructed. When a voltage of sufficient value is developed across the zeners, they will conduct, bypassing voltage transients which approach the gate breakdown voltage. This protects the gate structure, while allowing the FET to retain the wide dynamic signal range capability.

Even though gate protection has been included in the design of these devices, certain precautions should be observed while handling either MOSFETS or MOS Integrated Circuits:

- A. Do not generate static.
- B. Keep relative humidity above 60%.

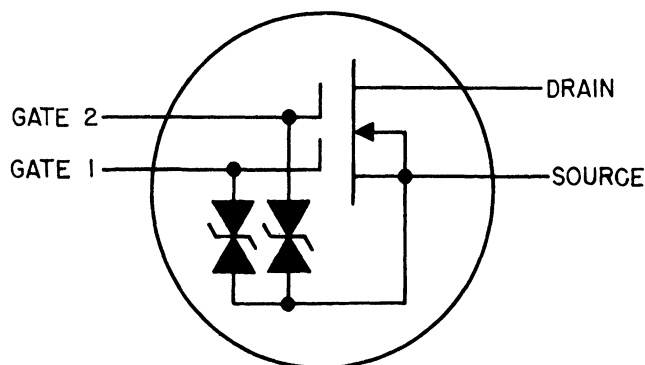


FIGURE 4 – MOSFET GATE PROTECTION

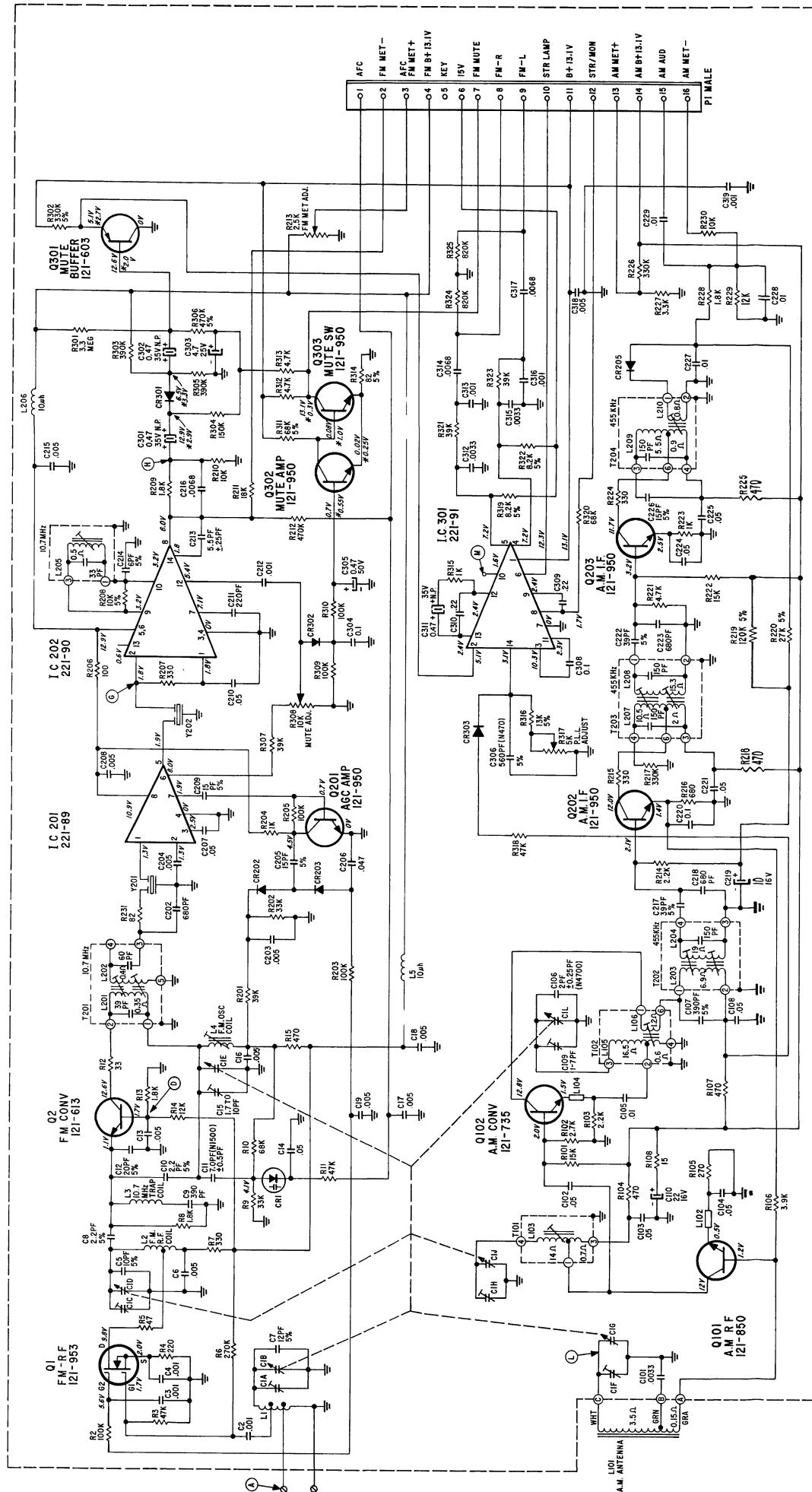


FIGURE 5 — CHASSIS 12WGR59 RF/IF/MPX SCHEMATIC

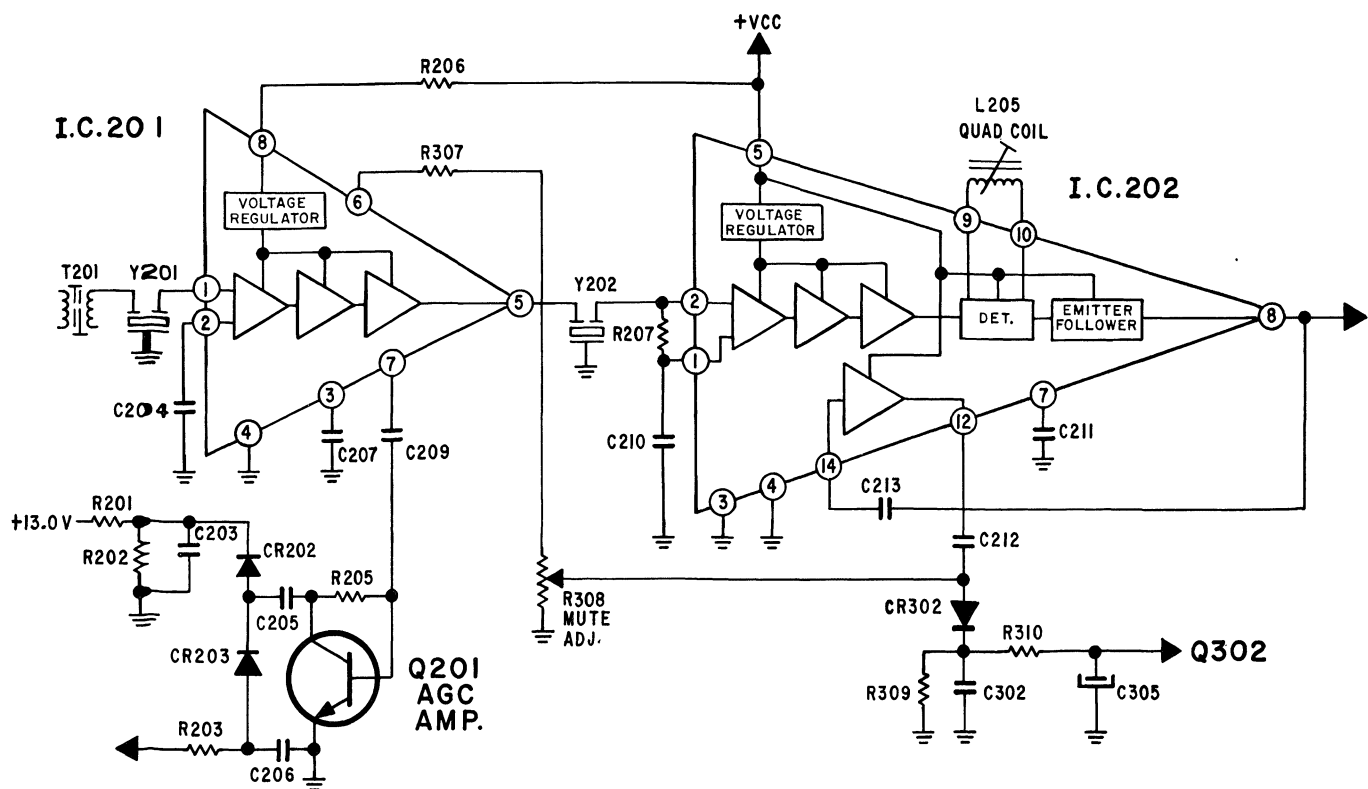
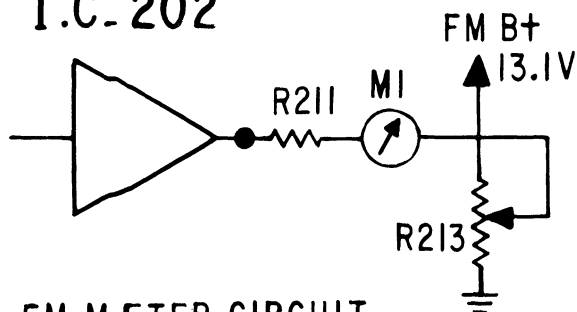


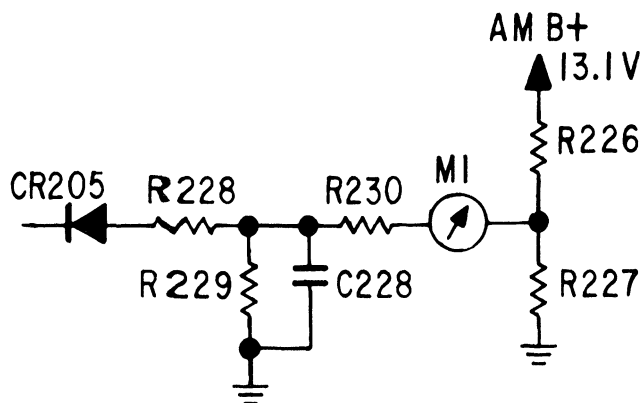
FIGURE 6 – CHASSIS 12WGR59 FM-IF

- C. Do not have rugs (especially nylon) in the service area.
- D. Do not use nylon or polyester pants, shirts or jackets.
- E. Do not wear rubber gloves. Cotton is recommended.
- F. Do not insert MOS devices in foam plastic holders.
- G. Leave MOS devices in their protective carriers (if supplied) until used in a circuit

I.C.-202



FM METER CIRCUIT



AM METER CIRCUIT

FIGURE 9 – TUNING METER

A front panel control is available, should it be desired to override the mute circuit. When the Mute Control is in the OFF position, the collector of Q303 is at ground, permitting Q303 to conduct.

TUNING METER

Tuning meter (M1) reads maximum on AM and zero center on FM. Meter Adjustment R213 is adjusted for zero center as part of the FM IF alignment. As mentioned previously when we discussed ceramic filters, alignment of this chassis requires that you set your generator to the frequency of the ceramic filters, then align the IF transformer (T201), the Quad Detector (L205), then Meter Adjustment R213 (See Figure 9).

FM – B+ SWITCHING

To reduce the possibility of "pop" in the speaker when switching to FM, two transistors (Q501, Q502) have been included (See Figure 10). When the selector switch is placed in FM, the +13.1 volts B+ is connected, via switch contacts SW1-R2 and 4 to the base of Q502. Electrolytic C512 begins to charge, causing Q502 to gradually conduct. As Q502 conducts, its collector voltage will begin to drop. This voltage drop will appear at the base of Q501, via R512, causing Q501 to conduct, resulting in B+ being fed from the +13.1 volt source via the emitter and collector of Q501 to pin 4 of connector P1 and then to the RF/IF/MPX circuit board.

FM-MULTIPLEX

For years we have used a multiplex decoder (either discrete components or an integrated circuit) which would amplify the incoming 19kHz pilot signal, then multiply it to 38kHz,

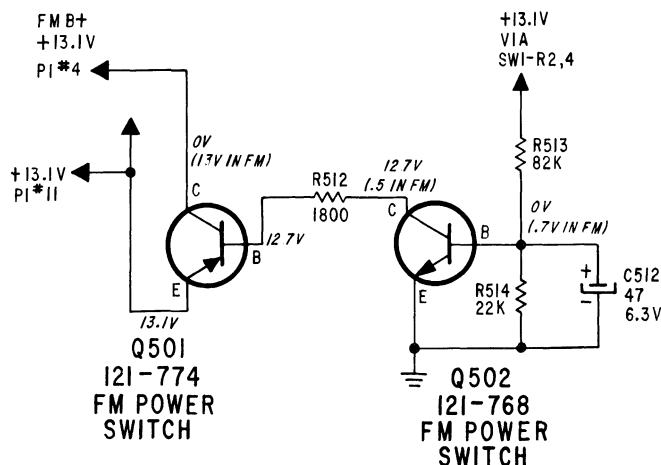


FIGURE 10 – FM B+ SWITCHING

reinsert the 38kHz into the difference (L-R) signal and matrix that signal with the sum (L+R) signal to recover the L and R audio signals.

Chassis 12WGR59 makes use of a circuit called a Phase Locked Loop (PLL), which can be compared to a thermostat controlled heating system. Figure 11A illustrates a basic heating system in which the furnace will generate heat. The thermostat will sense the temperature and compare it with the thermostat's manual setting. The thermostat will turn the fuel supply valve on or off, connecting or disconnecting the fuel source to the furnace, controlling heat generation from the furnace. This system functions in a closed loop.

Figure 11B illustrates the basic concept of a Phase Locked Loop (PLL). A Voltage Controlled Oscillator (VCO) is tuned to a given free running frequency. A portion of the VCO output is fed back to a phase detector, which also receives an external signal (19kHz in this case). These signals are compared for frequency and phase. Any difference is fed to a filter, the output of which will be a correction voltage applied to the VCO. This voltage keeps the VCO output on frequency and in phase with the input signal.

Figure 12 is a block diagram of the multiplex decoder (IC301). The three basic functions of IC301 include:

1. Regeneration of the 38kHz subcarrier frequency.
2. Stereo indicator switch.
3. Decoding (matrixing the L+R, and L-R/38kHz to provide the L and R outputs).

At the left in the upper row of Figure 12 is the input amplifier connected between pins 2 and 3. There are three outputs of this amplifier: The first output is to the Demodulator which we will discuss later. At pin 3 the signal is coupled via C308 to pin 11 at which point the signal goes to both the Phase Detector and the Amplitude Detector. Let's move three stages to the right of the Phase Detector where we find the 76kHz VCO whose free running frequency is controlled by C306, R316 and R317. Output of the VCO

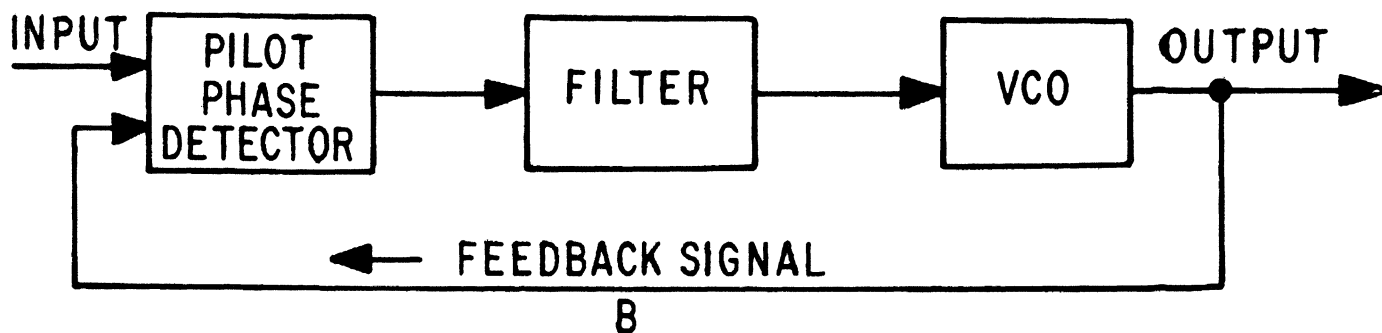
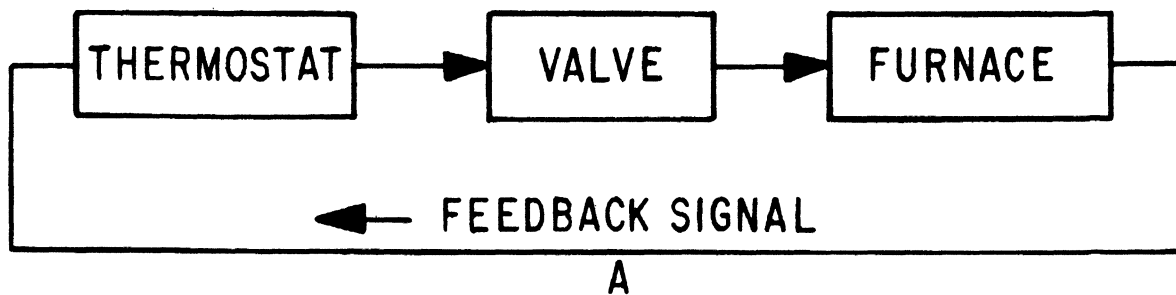


FIGURE 11 – PHASE LOCKED LOOP CONCEPT

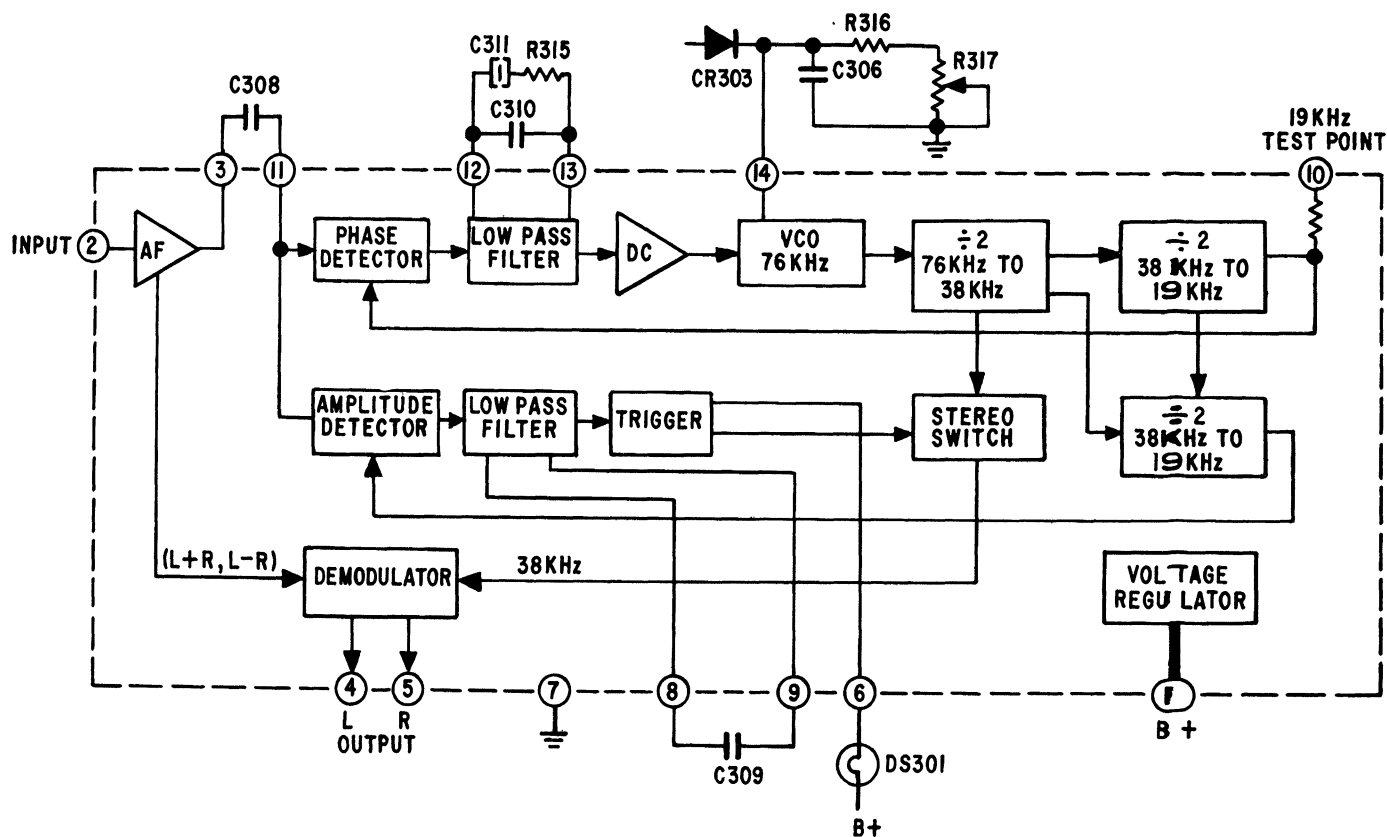
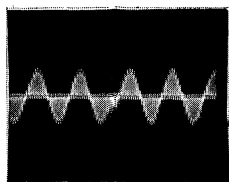
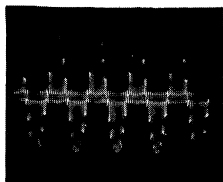


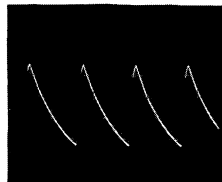
FIGURE 12 – MULTIPLEX DECODER BLOCK DIAGRAM



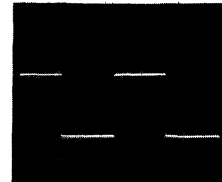
PIN 2-COMPOSITE INPUT
L+R, L-R (1 KHZ LEFT ONLY),
19 KHZ PILOT 10%
0.5V P/P (0.5 MILLISEC.)



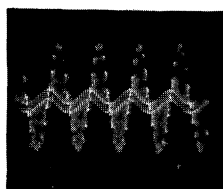
PINS 3 AND 11-COMPOSITE AMPLIFIED
L+R, L-R (1 KHZ LEFT ONLY),
19 KHZ PILOT 10%
1.4V P/P (0.5 MILLISEC.)



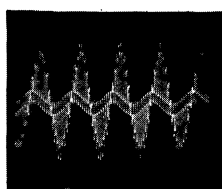
PIN 14-VOLTAGE CONTROLLED
OSCILLATOR ADJUSTMENT
3.5V P/P (5.0 MICROSEC.)



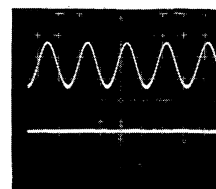
PIN 10-19 KHZ TEST POINT
2.7V P/P (10.0 MICROSEC.)



PINS 12 AND 13-FILTER-PHASE DETECTOR
0.14V P/P (0.5 MILLISEC.)



PINS 8 AND 9-FILTER-AMPLITUDE DETECTOR
0.47V P/P (0.5 MILLISEC.)



AT PLUG P1
P1, #9-(UPPER) LEFT OUTPUT
0.57V P/P (0.5 MILLISEC.)
P1, #8-(LOWER) RIGHT OUTPUT
0.05V P/P (0.5 MILLISEC.)

FIGURE 13 – MULTIPLEX DECODER WAVEFORMS

goes to two divide by two stages, resulting in outputs of 38kHz and 19kHz respectively. This 19kHz is available for external measurement at pin 10, as well as being fed back to the Phase Detector, where the phase and frequency of this 19kHz is compared with the input 19kHz. Any difference is fed to the low pass filter, and converted to a DC correction voltage, to be applied to the VCO if the VCO changes frequency.

Also at pin 11 is the Amplitude Detector which receives the input 19kHz and also the 19kHz output from a third divide by two stage. The Amplitude Detector will sense the level of the incoming 19kHz pilot level. If the level exceeds minimum, it will have an output which will be applied to the low pass filter and to the trigger stage. The trigger stage will activate the Stereo Indicator Light and also permits the Stereo Switch to pass 38kHz to the Demodulator.

In the demodulator the Sum (L+R), difference (L-R) and 38kHz are combined to derive the L and R outputs.

A regulator located in IC301 is connected to pin 1 (the +13.1 volt supply) and supplies most stages, while the unregulated +13.1 volts powers certain circuits.

Diode CR303 is connected to the AM B+ point at pin 14. When AM is turned on a positive voltage forward biases CR303, applies a positive voltage to pin 14, turning off the VCO. This prevents "birdies" from appearing on the AM band.

Proper adjustment of the VCO should be made by connecting a frequency counter to pin 10 and adjust R317 for 19kHz. In an emergency, if a frequency counter is not available, you might try the following: Tune in a station broadcasting stereo and adjust R317 until the stereo indicator turns on, then adjust control R317 to the center of the turn-on range.

"G" LINE AUDIO CIRCUITRY

Circuitry in the "G" line chassis families, while similar to "F" line chassis, contain circuit changes designed to reduce distortion. Current "G" line chassis families include the following:

1. 3WGR50, 3WGR52, 3WGR54.
2. 6WGR55, 6WGR56, 6WGR57.
3. 12WGR58
4. 12WGR59

COMPLEMENTARY SYMMETRY

As a review, in the past most output stages contained two transistors which were connected in a class "B" amplifier circuit. Both were normally a matched pair consisting of either two NPN or two PNP types. The class "B" circuit provides greater efficiency in the use of current supplied to the output stage than would be true in the use of current supplied to the output stage of class "A" amplifiers.

Normal class "B" circuits have some limitations of frequency response due to the driver and output transformer. A further limitation is cross-over distortion caused by one output transistor going into cut-off before the other output transistor has started to conduct. Cross-over distortion and the point of conduction are determined by the bias on the output stage.

Many bias circuits consisted only of a resistance divider network and when supply voltage varies so would bias voltage. This supply voltage change became critical in battery operated amplifiers but must still be considered when operating on AC power lines. Another factor that adds to the problem of controlling bias is temperature change, which will cause reduced base-emitter junction voltage and an increase in collector current. This bias voltage variation results in a change of operating voltages accompanied by a change in distortion.

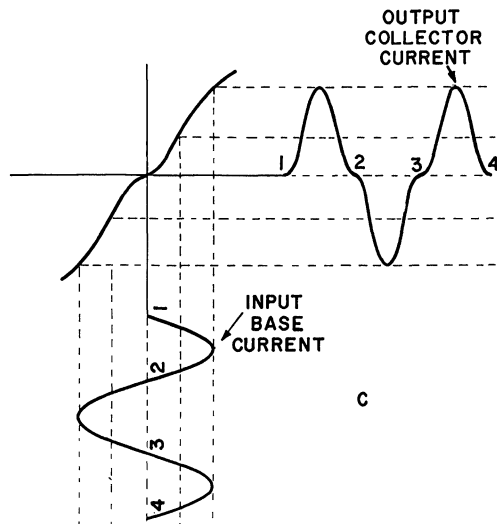
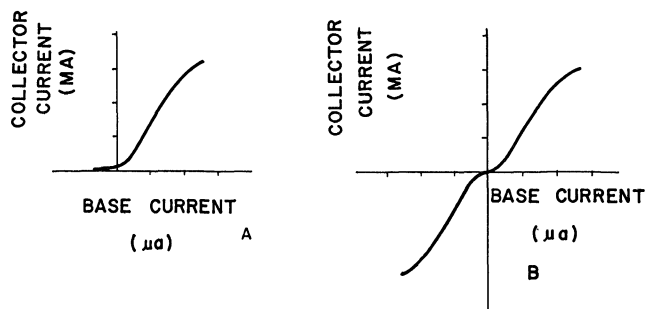


FIGURE 14 – CROSSOVER DISTORTION

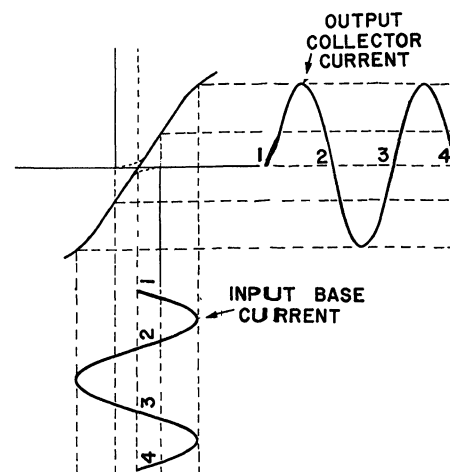
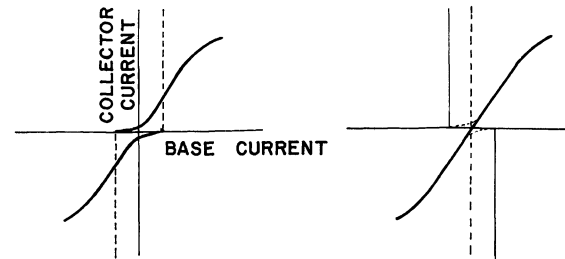


FIGURE 15 – DISTORTION REMOVED

Cross-over distortion is heard due to high order harmonics and may be recognized as a discordant sound. When viewed on a scope, the waveform may appear as a sine wave with straight sides or with a step between positive and negative half cycles. The latter is most common. (See Figure 14). This distortion can be greatly reduced or eliminated by applying forward bias to the output stage. Forward bias will cause a small current to flow in the base circuit of each transistor and the bias voltage causes a shift in the zero base current points (of each transistor), resulting in a smooth crossover between conduction of each output transistor (See Figure 15).

With the development of complementary symmetry circuits, we have eliminated the driver and output transformers. This improves the frequency response of the amplifier. These transformers have provided the phase relationship required to permit the class "B" push-pull output circuit to operate correctly. Proper signal phase relationship will be developed by the output transistors. Since one output transistor is NPN and the other is PNP, they will conduct on alternate half cycles, much the same as if a center tapped transformer were used to provide identical transistors with signals 180 degrees out of phase.

COMPLEMENTARY SYMMETRY - CHASSIS 3WGR50

A brief look at the complementary symmetry circuit of Chassis 3WGR50 (See Figure 16) will reveal direct coupling between the collector of the driver transistor (Q453) and the base of the output transistor nearest ground (Q455). Direct coupling will decrease distortion and provide consistent output measurements. The output circuit design is such that there is a center point between the emitters of Q454 and Q455. This point has a DC voltage which, under no-signal conditions, is equal to approximately one-half of the voltage on the collector of the transistor (Q454) nearest the high side of the supply voltage. Connected to this center point are:

1. A feedback loop (via resistors R463 and R473) to the emitter of the pre-driver (Q452).
2. A feedback loop via resistor R466 to the base of the driver transistor.
3. An output coupling capacitor (C472) to the speaker.

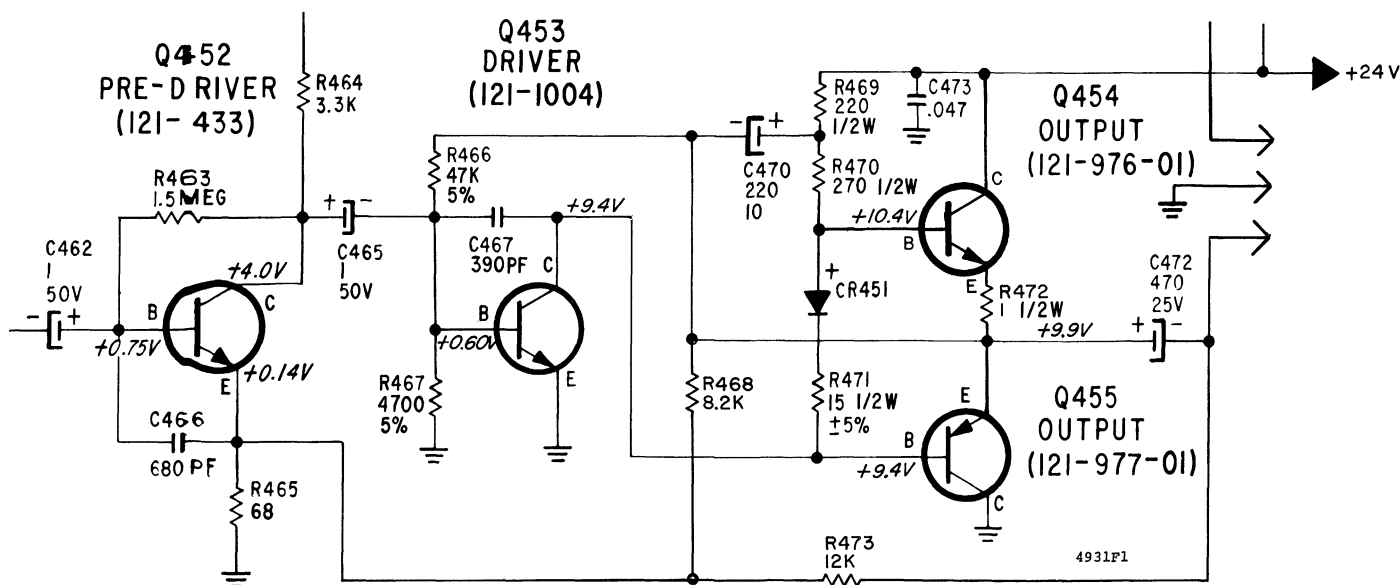


FIGURE 16 – CHASSIS 3WGR50 AUDIO OUTPUT CIRCUIT

Between the base of each output transistor there is a series connected resistor-diode circuit (R471, CR451). Bias voltage is developed across this resistor-diode combination and controls idling current in the output stage. Under no signal conditions voltage drops across the resistor-diode are equal to base-emitter voltages of the output transistors, plus the voltage drop across emitter resistor R472. Due to the very low value of the emitter resistor, and the voltage drop across it, voltage on the emitter can be considered to be same as the center point voltage. While many refer to this as a class "B" circuit, it should be called class "AB" due to the idling current. Bias diode CR451 has non-linear voltage/current relationships resulting in the following characteristics:

1. Voltage across the diode changes more slowly than current flowing through it.
2. Current is approximately proportional to supply voltage.
3. Voltage across the diode will decrease with rising temperature.

This non-linear diode voltage/current curve is similar to that of the output transistors allowing a near linear temperature relationship to exist between diode and transistors. Under no-signal conditions, both the diode and transistors will show similar effects due to any temperature change. If there is an increase in temperature, both the diode and transistors will show increased current flow. The added current flow in the diode will offset increased flow in the transistor and stabilize bias voltage. Since this diode has a low AC resistance, any changes in current of the driver stage results in less effect on the output stage than would be true with only biasing resistors.

Operating conditions for the driver transistor are determined by base-emitter voltage and driver transistor beta. Also affecting the operating point are values of the driver base resistor, feedback resistor to driver base, and two resistors in the driver's collector circuit. All these factors will effect voltage at the previously mentioned center point.

When a negative going signal is applied to the driver base, current gain of the driver is reduced. At the same time, however, the charge on the electrolytic (C470) will maintain a near constant current through resistor R470 connected in the base circuit of the upper output transistor (Q454). This will cause voltage across the resistor to maintain an almost constant value, which in turn determines base-emitter bias of transistor Q454. Notice that current flow from this bias resistor not only goes through the diode and collector circuit of the driver transistor but also goes to base of transistor Q454. Current in this base circuit will determine the amount of transistor gain. When transistor Q454 is conducting, Q455 is cut-off since it is reverse biased.

When a positive going signal is applied to the base of the driver (Q453), its collector current will increase. The electrolytic (C470) will still maintain a near constant voltage across the bias resistor of the upper transistor. Under these conditions the upper transistor (Q454) is now reverse biased to cut-off, and the lower transistor (Q455) is conducting.

Since each output transistor conducts on alternating halves of each cycle, voltage change at the center point will result in an output signal that will duplicate input. Use of complementary symmetry circuitry results in lower distortion and better frequency response.

QUASI COMPLEMENTARY SYMMETRY - CHASSIS 12WGR58

Transistors Q453, Q454 and Q455 of Figure 16, (complementary symmetry as used in Chassis 3WGR50) can be compared with Q453, Q455, and Q456 respectively of Figure 17 (quasi complementary symmetry as used in Chassis 12WGR58). Voltage changes on the collector of Q453 of Figure 17 appear on the base of Q456 (directly) and via Q454 to the base of Q455. AC signals will see Q454 as a short circuit.

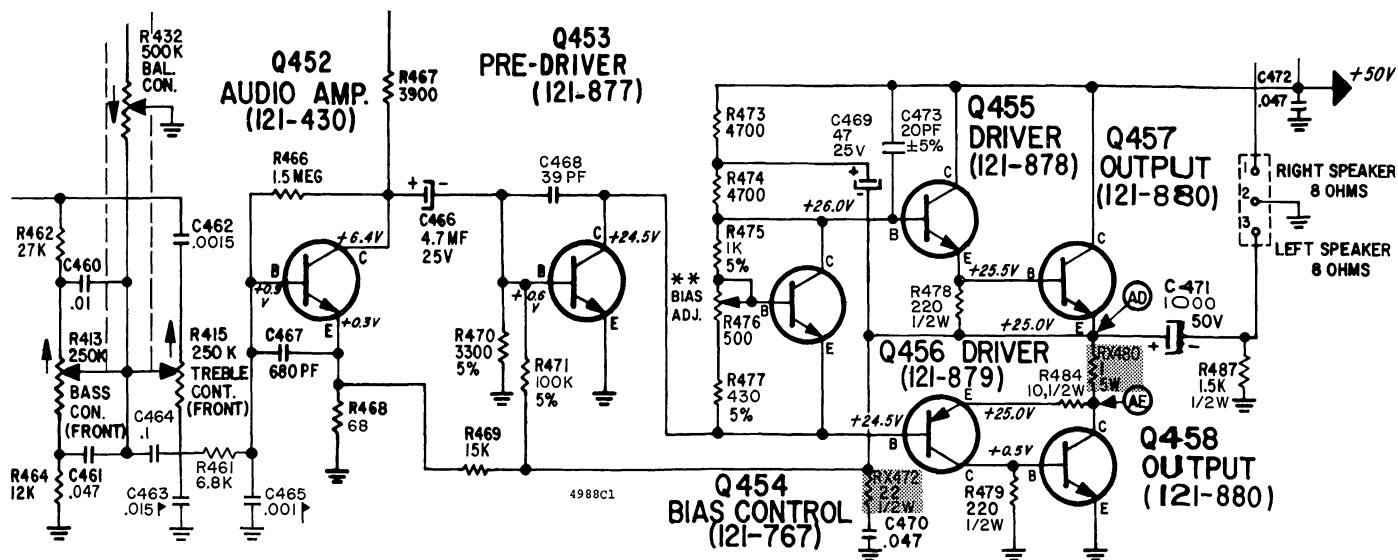


FIGURE 17 – CHASSIS 12WGR58 AUDIO OUTPUT CIRCUIT

When a positive going voltage appears on the base of Q455, a similar change occurs on its emitter, and also on the base of Q457 which is then forward biased into conduction. During this time, the positive going voltage will bias Q456 to cut off, and neither Q456 nor Q458 will conduct. When the base voltage on Q455 goes in a negative direction, Q455 will be biased towards cut off, while Q456 will be forward biased and in turn causes Q458 to conduct.

Operation of Chassis 12WGR58 in Figure 17 is similar to Chassis 3WGR50 in Figure 16 plus the addition of power output transistors Q457 and Q458. It should also be noted that Q456 provides phase inversion while Q455 is an emitter follower with no inversion.

Bias on output transistors Q454 and Q455 (Figure 16) is determined by diode CR451 connected between their bases. CR451 has temperature characteristics similar to the output transistors. When an increase in temperature causes an increase in transistor current, a similar voltage decrease occurs across the diode providing compensation by changing the base to base bias voltage of Q454 and Q455.

Quasi complementary symmetry circuit of Figure 17 uses a transistor (Q454) for bias control, instead of a diode. Q454 not only serves to stabilize base voltage, but also has the advantage of allowing manual presetting of the bias. Bias control (R476) is part of the voltage divider network (R475, R477) between collector and emitter of Q454. Setting R476 determines the bias on Q454, which in turn sets the bias and idling current of the output transistors. Q454 is subject to the same temperature changes as the output transistors. Any increase in temperature that causes increased current flow in Q454 will offset the increased current flow in the other transistors and will stabilize bias voltages.

Proper idling current in the output circuit of Chassis 12WGR58 is obtained when Bias Control (R476) is set to provide 0.010 to 0.015 volts across the 1 ohm resistor (R480).

Only one bias adjustment is required in each output channel of Chassis 12WGR58. Basic adjustment procedure consists of monitoring a DC voltage between two test points and adjusting the bias control for the correct voltage. Since voltage is in the millivolt range, it has been found that a digital voltmeter provides the best reading.

Recommended bias adjustment procedure for Chassis 12WGR58 includes the following considerations:

1. The set should be at room temperature prior to adjustment.
2. Bias adjustment should be made after the set has been on, permitting B+ voltages to stabilize.

Proceed as follows for Chassis 12WGR58:

1. With the set turned off, be certain that the power supply that belongs with the chassis is properly connected.
2. Turn both bias adjustment controls thru the full range and set to minimum (counterclockwise).
3. Turn loudness control to minimum (counterclockwise) and short input to ground.
4. Connect meter to the set of test points in one channel.
5. Turn set on.
6. After B+ has stabilized adjust bias control for channel to obtain a reading of 10 to 15 millivolt on your meter.
7. Turn set off.
8. Repeat steps 4 through 7.

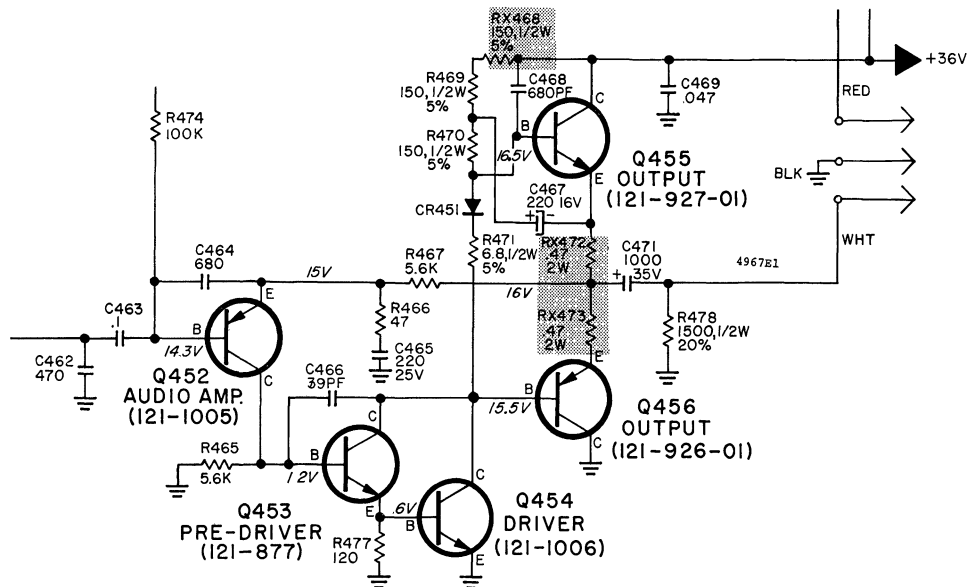


FIGURE 18 – CHASSIS 6WGR55 AUDIO OUTPUT CIRCUIT

AUDIO CIRCUITRY – CHASSIS 6WGR55 FAMILY

Figure 18 illustrates most of the audio circuitry used in Chassis 6WGR55, 6WGR56, and 6WGR57. This circuit is somewhat similar to the basic complementary symmetry circuit shown in Figure 16 for Chassis 3WGR50. Amplifier transistor Q452 is now direct coupled to the pre-driver Q453. Q453 and Q454 are effectively a class A Darlington circuit which will be explained shortly. Resistors R465 and R477 serve as collector loads for Q452 and Q453 respectively. Collectors of Q453 and Q454 are dc coupled to the base of Q456 (directly) and also to the base of Q455 (via resistor R471 and bias diode CR451). AC signals will see CR451 as a short circuit. Boot strap capacitor C467 is now connected directly to the emitter of Q455, instead of at the center point (junction of RX472 and RX473). At the center point are:

1. Output coupling capacitor C471 and bleeder resistor R478. The bleeder resistor provides protection should the set accidentally be operated without any load.
2. A feedback circuit to the emitter of Q452, consisting of voltage divider R466 and R467, determines the AC feedback to Q452. Capacitor C465 is included for dc insulation because the circuit is direct coupled.

R474, at the base of Q452, determines the center point dc voltage. C468 provides added high frequency stability. Operation of this circuit is the same as explained for Chassis 3WGR50 shown in Figure 16.

DARLINGTON CIRCUIT

Lets briefly review the operation of a Darlington type transistor. Examination of the schematic symbol in Figure 19 shows that, as used on Chassis 12WGR59 which follows, it is really two NPN transistors existing within one package. The 12WGR59 also uses a PNP Darlington in the output.

Operation of this device is the same as two transistors in separate packages but has such added advantages as reduced size, fewer external circuit components required and extremely high input impedance. Briefly the operation is as follows. Assume separate NPN transistors which we refer to as Q1 and Q2 (Figure 19). Since there are three external terminals identified with the conventional terms (emitter, base, and collector) voltages are applied as normal for NPN transistor (in this example), that is, the base is positive with respect to the emitter. The base and collector voltages are consecutively more in the positive direction. With DC bias voltages established the AC signal voltage is applied to the base of Q1. A positive going signal will increase the forward bias causing an increase in current flow in the collector-emitter circuit. This increased current flow also goes through the base-emitter junction of Q2 in series with Q1's base-emitter junction. Current in the Q2 collector-emitter circuit will also increase. A negative signal to the base of Q1 will cause current reduction in the output of Q2. For a common emitter amplifier circuit there will also be a phase reversal between input (base of Q1) and output (collector of Q2) terminals. The Darlington circuit has been seen at Q453 and Q454 in Figure 18 (Chassis 6WGR55) where separate transistors were used, and in Figure 20 (Chassis 12WGR59) where the Output transistors are internally a Darlington.

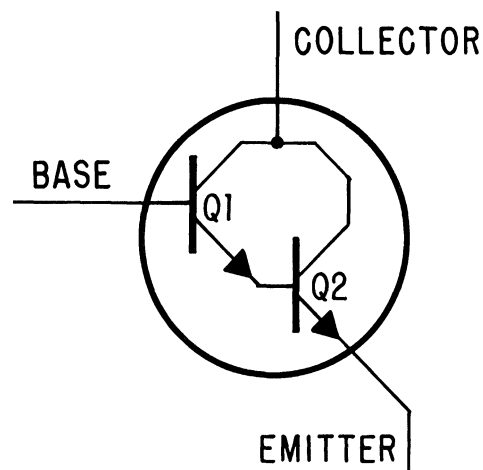


FIGURE 19 – DARLINGTON TRANSISTOR

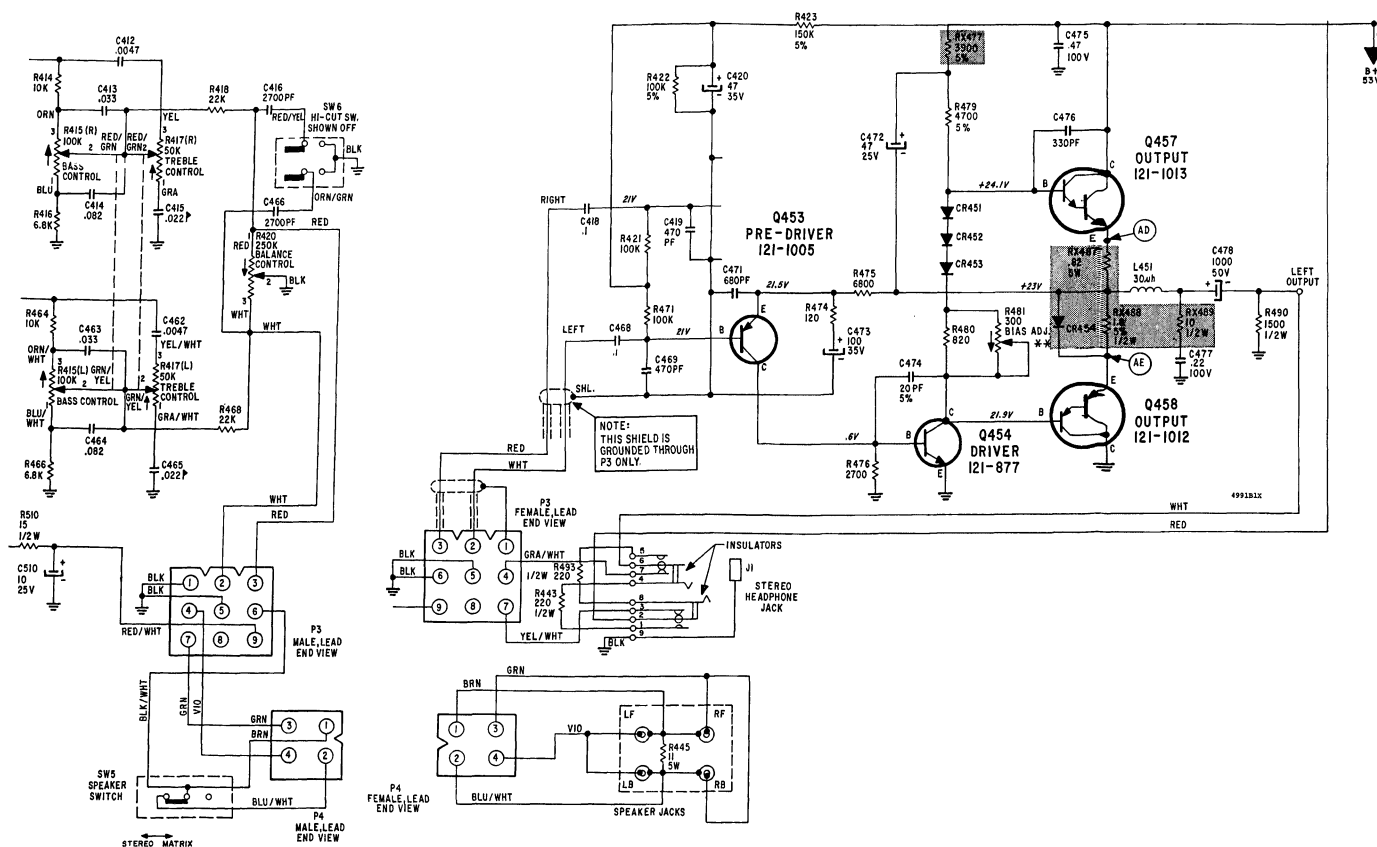


FIGURE 20 - CHASSIS 12WGR59 AUDIO OUTPUT CIRCUIT

AUDIO CIRCUITRY - CHASSIS 12WGR59

Figure 20 shows most of one channels audio circuitry for chassis 12WGR59 (except for Q451 and Q452). Q451 is an emitter follower stage followed by the Loudness Control, then a common emitter stage (Q452), the Bass, Treble and Balance controls. Connected at this point is a new control - the Hi Cut Switch (SW6). When this switch is in the "on" position a small value capacitor (C416 and C466) shunt the higher frequencies to ground.

Pre-driver transistor (Q453) is direct coupled to the driver (Q454), with R476 connected to ground from the junction of the collector of Q453 and the base of Q454. The collector of Q454 is connected directly to the base of output transistor Q455 (a Darlington). Q454 is also connected to the base of output transistor Q457, via the resistor-diode circuit of R480, R481, CR451, CR452 and CR453 (R481 being a variable Bias Adjustment control across R480). Bias voltage is developed across this combination and controls idling current in the output stage. If the bias is too low, crossover distortion will occur, and if the bias is too high there will be excess current and overheating. Under no signal conditions, the sum of the voltage drops across the resistors and diodes are equal to the base - emitter voltages of the output transistors, plus the voltage drops across the emitter resistors (RX487, RX488). Because of the low values of these resistors the emitter voltage may be considered to be the same as the centerpoint voltage. As you will note, resistors R480 and Bias Control R481 are paralleled, permitting smoother adjustment of the bias voltage.

Operating conditions for the driver transistor are determined by base-emitter voltage and driver transistor beta. Also effecting the operating point are values of the driver base resistor (R476-collector load for Q453), feedback resistor (R475) to the pre-driver base, four resistors in the output bias circuit (RX477, R479, R480, R481) and R471 connected to B+. All these factors effect voltage at the center point.

Connected at the center point are the following:

1. A feedback loop (via R475) to the emitter of the pre-driver Q453. R474 and R475 determine the AC feedback to Q453, while C473 provides DC isolation.
2. Output circuit consisting of:
 - A. L451, RX489 and C477 comprise a high frequency roll-off circuit.
 - B. Output coupling capacitor C478.
 - C. Load resistor R490 will drain any charge off of C478, providing protection if the output does not have the proper load.
3. Between center point and emitter of Q458 are the parallel combination of CR454 and RX488. When the circuit is operating at low output power the diode is not forward biased, therefore it is in effect open, and RX488 is in the circuit limiting the output stage current. When the output power reaches a given value, the diode is forward biased, effectively shorting the resistor, permitting higher output power.

When a negative going signal is applied to the driver base, current gain of the driver is reduced. At the same time, the charge on electrolytic C472 will maintain a near constant current through resistor R479 connected in the base circuit of the upper output transistor (Q457). This will cause voltage across resistor R479 to maintain an almost constant value, which in turn determines base-emitter bias of transistor Q457. Notice that current flow through bias resistor R479 goes not only through the resistor - diode circuit and the collector of driver transistor Q454 but also to the base of transistor Q457. Current in this base circuit will determine the amount of transistor gain. As transistor Q457 is conducting, Q458 is cut-off because it is reversed biased.

When a positive going signal is applied to the base of the driver (Q454), collector current of the driver will increase. The electrolytic (C472) will still maintain a near constant voltage across the bias resistor of Q457. Under these conditions, the upper transistor (Q457) is now reverse biased to cut-off, but the lower transistor (Q458) is conducting. Since each output transistor conducts on alternating halves of each cycle, voltage change at the center point will result in an output signal duplicating the input.

Proper idling current in the output circuit of Chassis 12WGR59 is obtained when Bias Control R481 is set to provide 0.025 to 0.030 volts across resistors (RX487, RX488).

Only one bias adjustment is required in each output channel of Chassis 12WGR59. Bias adjustment procedure consists of monitoring a DC voltage between two test points and adjusting the control for the correct voltage. Since voltage is in the millivolt range, it has been found that a digital voltmeter provides the best reading.

Recommended bias adjustment procedure for Chassis 12WGR59 includes the following considerations:

1. The set should be at room temperature prior to adjustment.
2. Bias adjustment should be made after the set has been on, permitting B+ to stabilize.

Proceed as follows for Chassis 12WGR59:

1. Turn both bias adjustment controls thru the full range and set to minimum (counterclockwise).
2. Turn loudness control to minimum (counterclockwise).
3. Connect meter to the set of the test points in one channel.
4. Turn set on. Line should be at 120 VAC \pm 2%.
5. After B+ has stabilized, adjust bias control for channel to obtain a reading of 25 to 30 millivolts on your meter.
6. Turn set off.
7. Repeat steps 3 through 6.

TWO ON TWO SPEAKER MATRIX

All "G" line stereo modular and console models incorporate a speaker matrix decoder system called "Two On Two". This system is classified as a high level (at speaker level) decoder as compared with the low level electronic decoding used in certain chassis. Models having the "Two On Two" feature incorporate a switch identified "MATRIX-STEREO" (See Figure 21).

When speaker systems are connected to both rear or external speaker jacks, it is possible to connect those speakers in parallel with the front speakers (switch in "STEREO" position). This will allow better sound distribution in a large room, or the external speakers can distribute the same sound to another room.

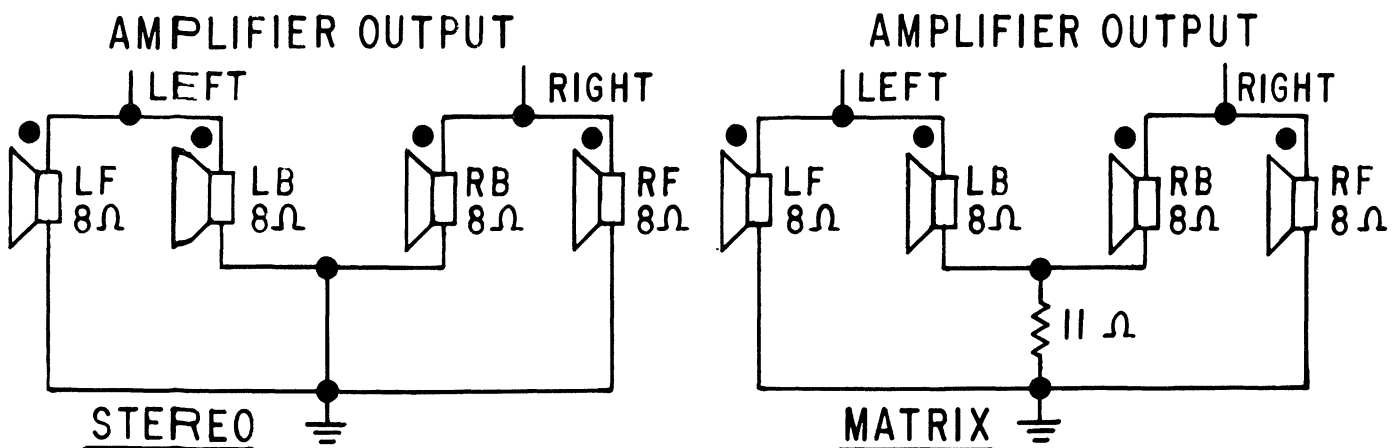


FIGURE 21 — TWO ON TWO SPEAKER MATRIX

In the "MATRIX" position a resistor is connected in the circuit resulting in a matrixing action. This results in reproduction of simulated four channel sound from records encoded in the various matrix concepts, or from many standard stereo records. The latter is possible because many stereo records contain ambient information having a phase difference between the left and right channels.

Some models also include a third position, "EXT", on the "STEREO-MATRIX" switch. In the "EXT" (external) position speakers connected to the rear or external jacks will play, but the front or internal speakers will be disconnected. It is therefore possible to play the stereo through speakers in another room without operating the "front" speakers.

ALLEGRO SPEAKER SYSTEMS

Speaker systems in the "G" line fall into three basic groups:

1. Allegro in Model G9019W and all consoles except G904P.
2. Allegro 1000 (Model G1000W), Allegro 2000 (Model G2000W) and Allegro 3000 (Model G3000W) which are the speaker systems designed as the main units for the "G" line modular models as well as external speaker systems for use with the modular and console models having the "Two On Two" speaker matrix feature.
3. Non-Allegro system in Model G904P.

Allegro speaker system, Model G9019W, is of the bass reflex type. Figure 22 is the schematic, while Figure 23 illustrates the cabinet design. As you will note, the enclosure has two openings in the front, one for each speaker. In the past, most bass reflex enclosures had a port on the front, with the remaining walls being solid. Model G9019W, as illustrated in Figure 23, has a port in the rear panel of the enclosure, instead of the front.

It is interesting to note that a bass reflex speaker enclosure can be described as a tuned enclosure in which the air in the port will resonate with the air in the main area of the cabinet, at a given frequency. This frequency determines the effective low frequency cutoff of the system (cabinet and enclosure combined). Below the selected frequency (45 Hz in the G9019W) the response drops very rapidly (approximately 18 db/octave).

It could also be described as an acoustical phase inverter. That is, at some frequency, within its normal operating range, the air in the port is moving in an outward direction (to the back), while the speaker cone is also moving in an outward direction (to the front). These two movements would occur at the same instant.

A basic advantage of the bass reflex system, as compared to a closed box enclosure, is that in a bass reflex system the designer can either extend the frequency response, while maintaining the same level of efficiency; or retain the frequency response while raising the efficiency approximately 3 - 4 db. In designing the Allegro system, it was decided to improve the frequency response beyond that of an earlier model (S9017).

Sound level of signals radiated thru the port (in the 40-70 Hz range) is comparable to the sound level radiated by the woofer (in the range of 70 Hz to 1 kHz). This requires that the 2-5/8" diameter port (in Model G9019W) must "pulsate" air at a much higher velocity than the woofer, which is approximately 8" in diameter. Several factors must be considered in order to maintain the required port velocity.

- A. The woofer uses a highly efficient magnetic structure making it comparable to a powerful electrical motor. This forces air, in the port, to move at high velocities, even though the air in the box is attempting to stop motion of the speaker cone.

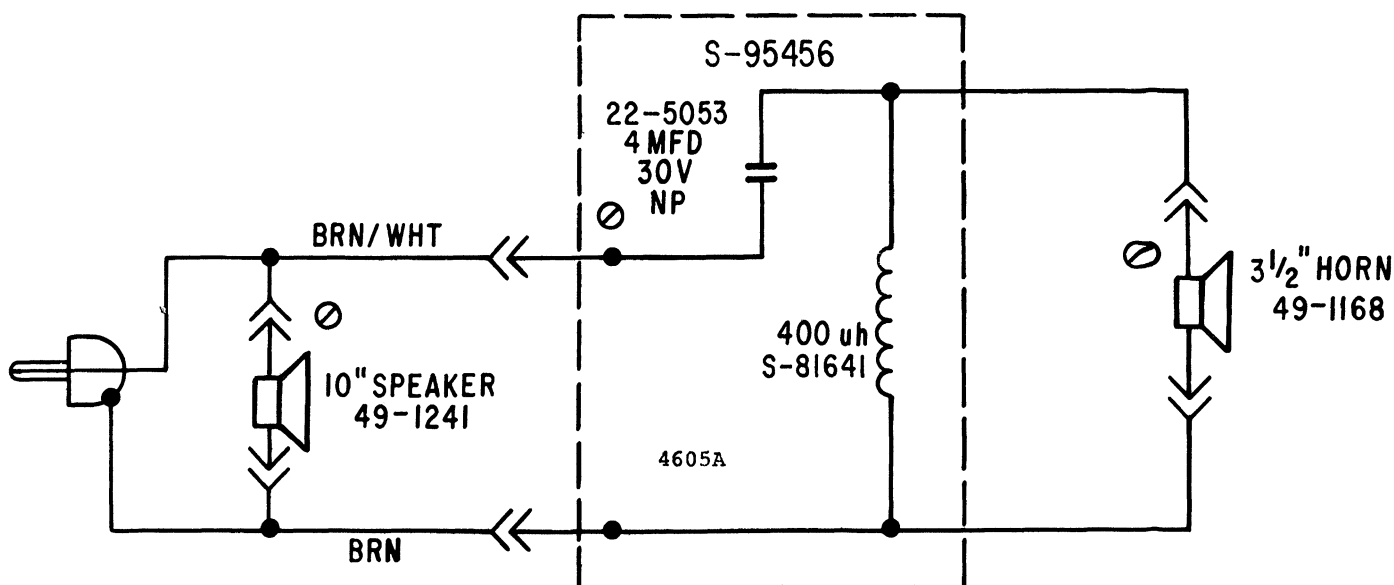


FIGURE 22 — MODEL G9019W SCHEMATIC

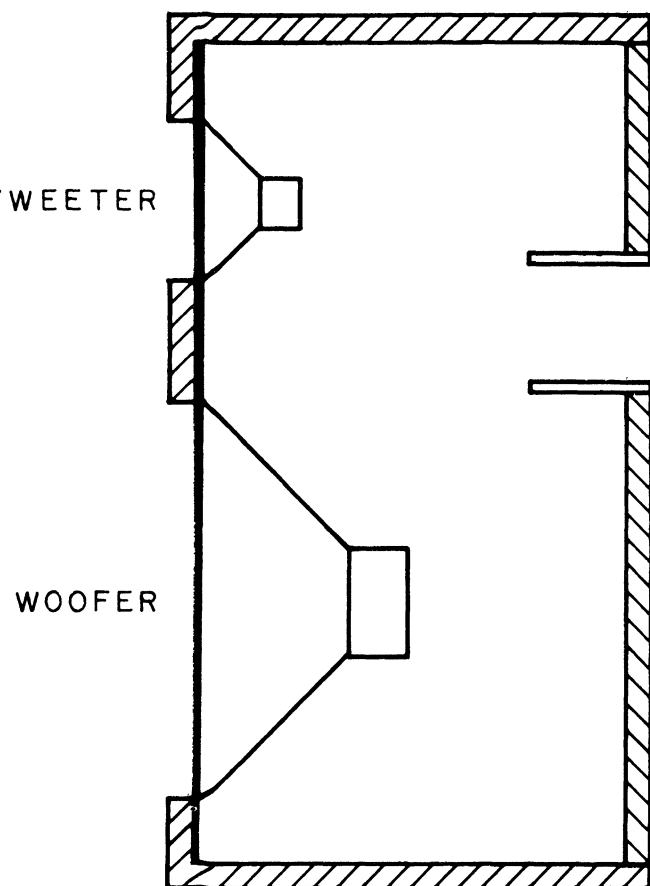


FIGURE 23 – MODEL G9019W
SPEAKER ENCLOSURE

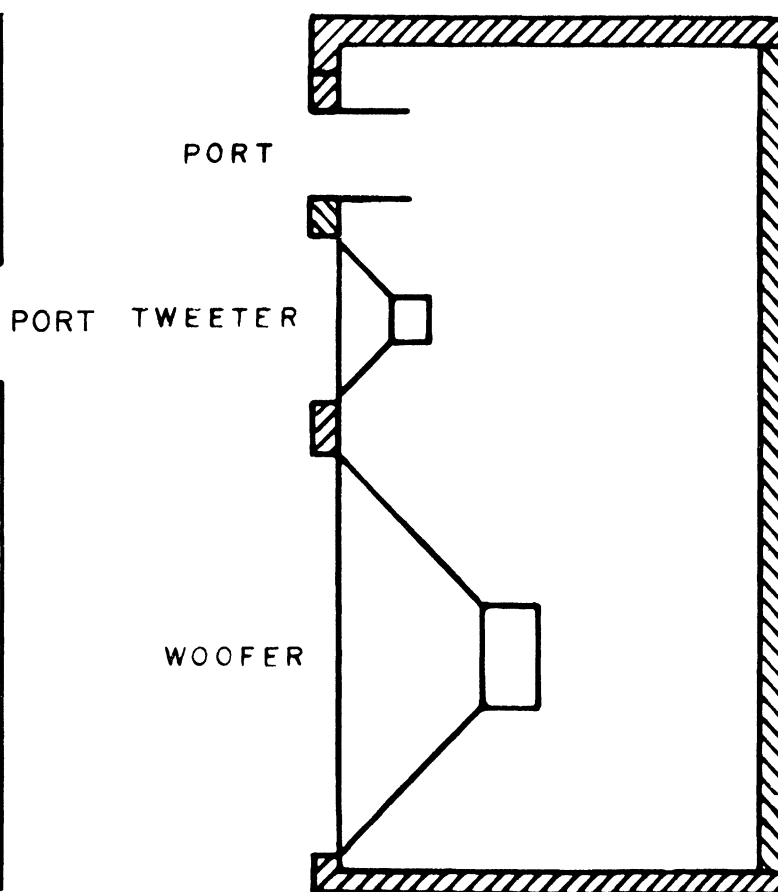


FIGURE 24 – MODEL G1000W
SPEAKER ENCLOSURE

- B. The internal air pressure in a bass reflex enclosure is much higher than that found in a conventional closed-box enclosure, therefore mechanical construction of a bass reflex enclosure must be more substantial than that of an air suspension type. All panels, walls and joints must be extremely rigid to withstand these air pressures.
- C. Speakers (and other components) must be securely fastened to prevent air leaks. Leaks or loose components can result in losses which cause a deterioration of performance.

In order to effectively increase cabinet volume, and also to dampen internal resonances of the enclosure, three acoustic pads of variable density are placed adjacent to the internal walls. The area of each pad that has the highest density is adjacent to the wall surface. These pads must not obstruct the port.

When servicing these units (or for that matter most speaker enclosures) several precautions must be taken:

- A. When removing the back, be careful when handling the acoustic pads (they may tear easily).
- B. All speakers must be securely fastened to prevent leaks and rattles.
- C. If the front grille is removed, be certain that the baffle is tightly captivated by the mounting screws when reinstalled.

- D. When replacing the back, be certain that the acoustic pads don't interfere with the port.
- E. The screws holding the back must be secured by using a sufficient amount of torque in order to prevent air leaks.

Normal positioning of this enclosure in a listening room would be near a wall. While this would be normal, in fact desirable, caution must be taken to avoid placing this enclosure in any position that would obstruct the port, as this would result in degraded bass response. The desired positioning would be one which allows at least 1½ inches between the back of the enclosure and the wall of the room (or similar obstruction).

Speaker enclosures for Models G1000W, G2000W and G3000W are also of the bass reflex type and are similar in design to the model described above except for the forward facing part. Figure 24 is a cross section view of this latter group.

DISASSEMBLY PROCEDURE MODELS G596W and GR596W

Basic disassembly procedure for the above models, using Chassis 12WGR59, is simplified due to modular construction techniques with the use of convenient cable connectors. This is illustrated by the accompanying photos, in Figures 25 through 28.

CABINET BOTTOM REMOVAL

1. With power disconnected, place main unit on right side (as viewed from front) on top of a soft clean surface.

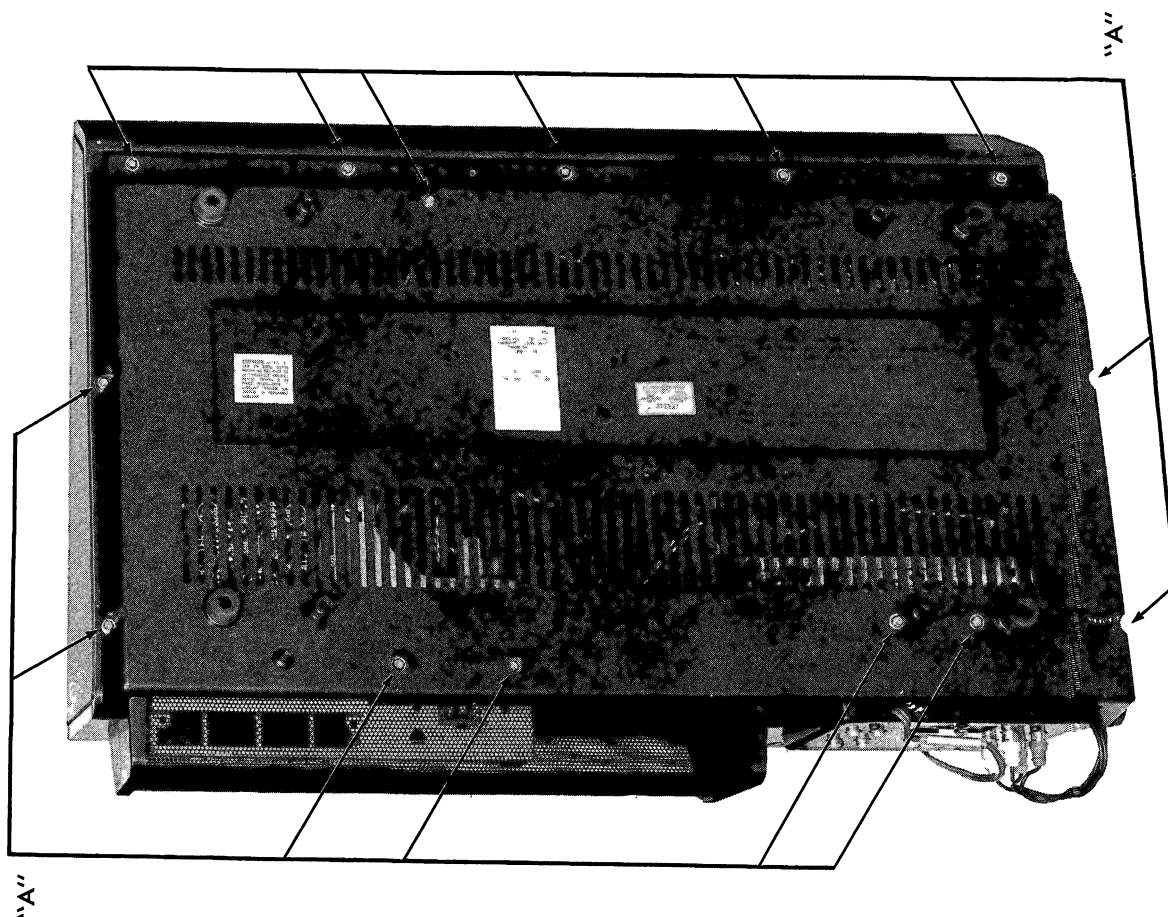


FIGURE 25 - MODELS G596W AND GR596W
CABINET BOTTOM SCREW LOCATIONS

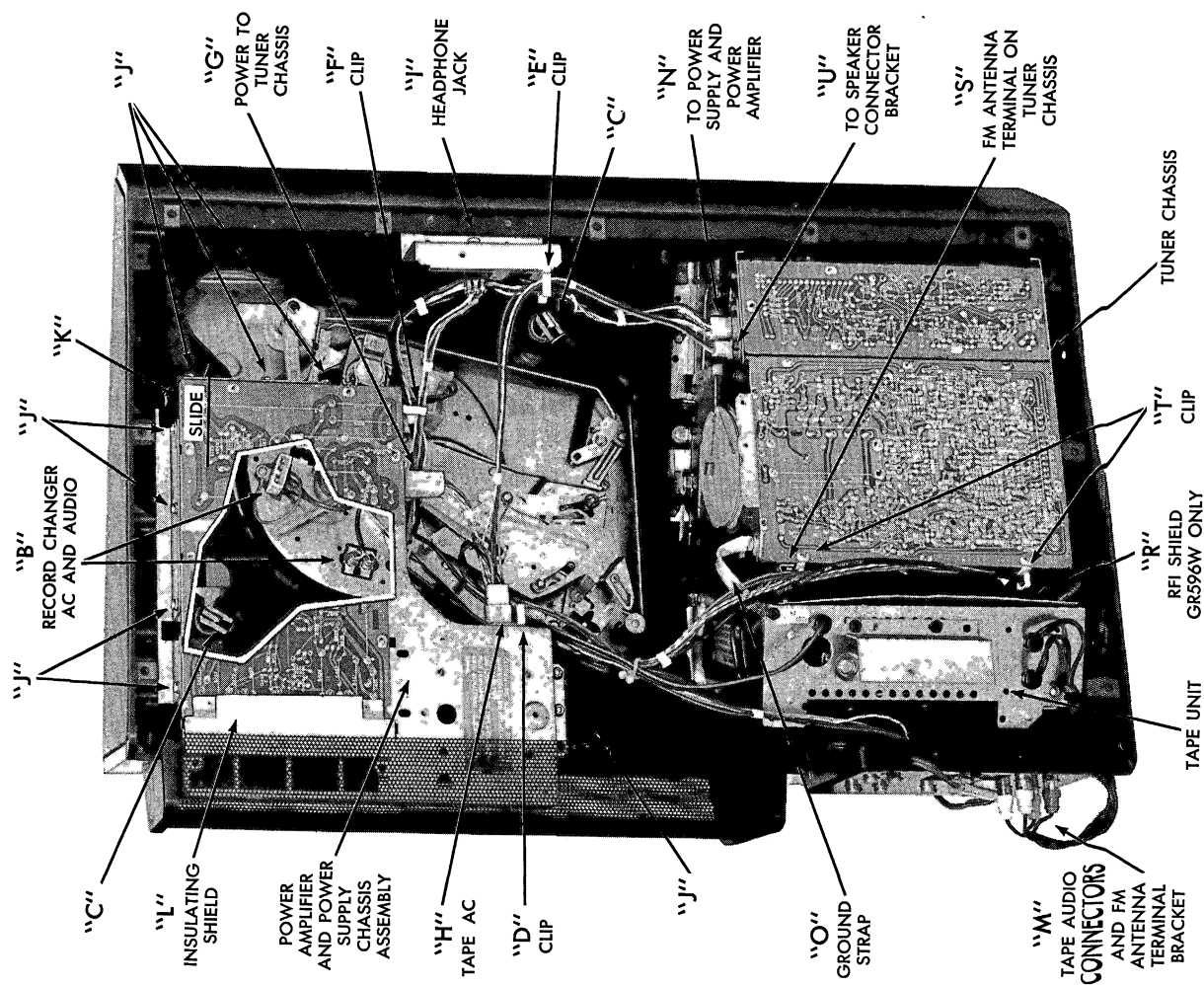


FIGURE 26 - MODELS G596W AND GR596W
CABINET BOTTOM REMOVED

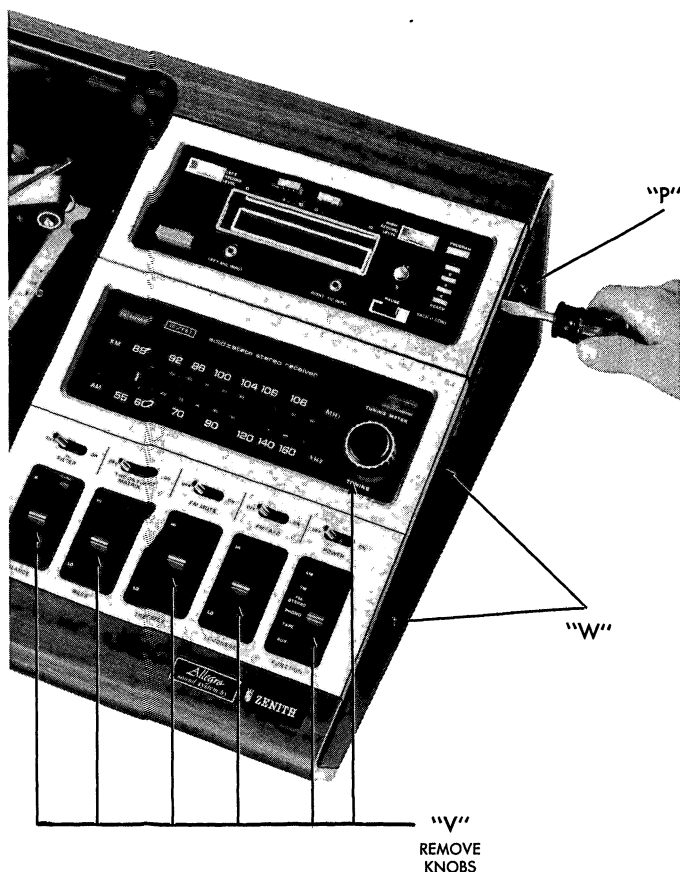


FIGURE 27 — MODELS G596W AND GR596W
ESCUTCHEON REMOVAL

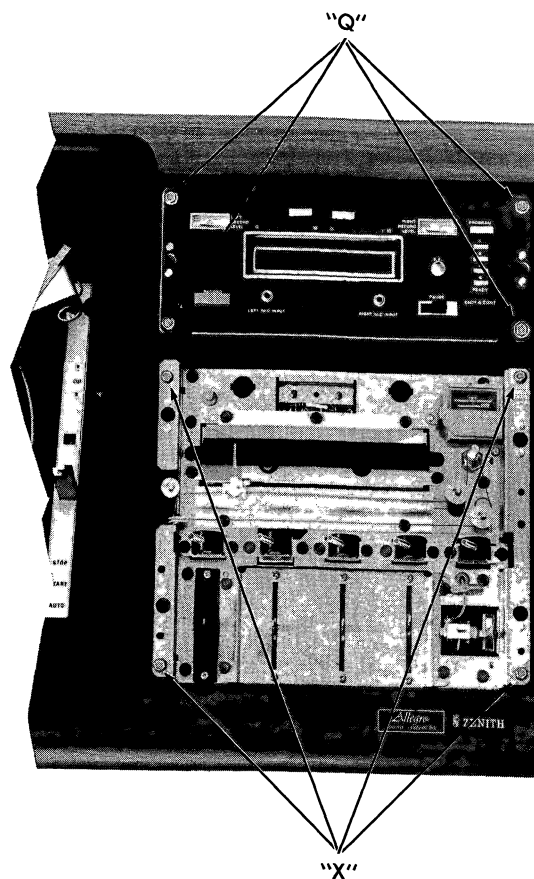


FIGURE 28 — MODELS G596W AND GR596W
TAPE UNIT AND TUNER CHASSIS
MOUNTING SCREWS

2. Remove fourteen (14) screws holding bottom cover ("A" in Figure 25).

RECORD CHANGER REMOVAL

1. Proceed as for "Cabinet Bottom Removal".
2. Release one (1) record changer mounting clip (located above headphone jack — "C" in Figure 26).
3. Lift record changer upward and disconnect AC and audio cables at record changer (visible above amplifier chassis — "B" in Figure 26).
4. Using caution, slide record changer forward while lifting outward to remove.

POWER SUPPLY/AMPLIFIER REMOVAL

1. Proceed as for "Cabinet Bottom Removal".
2. Release interconnecting cables from retainers ("D" and "E" in Figure 26).
3. Unplug record changer AC cable at record changer ("B" in Figure 26).
4. Unplug two connectors on this chassis ("G" and "H" in Figure 26).
5. Unplug connector on tuner chassis ("N" in Figure 26).

6. Disconnect FM antenna connector ("M" in Figure 26).
7. Dismount headphone jack ("I" in Figure 26) from bracket.
8. Remove nine (9) screws holding chassis assembly and mounting brackets ("J" in Figure 26).
9. Remove chassis by sliding in direction of arrow ("K" in Figure 26).

10. When replacing chassis be certain that insulating shield ("L" in Figure 26) is between chassis and rear grille.

TAPE UNIT REMOVAL

1. Proceed as for "Cabinet Bottom Removal".
2. Unclip and disconnect tape unit audio cables at rear panel connectors ("M" in Figure 26).
3. Unclip and disconnect tape unit AC cables at power supply chassis ("D" and "H" in Figure 26).
4. Disconnect group strap between tape unit and tuner chassis ("O" in Figure 26).
5. The tape unit mounting screws are covered by a "snap off" escutcheon. A notch will be found on the center of the outer edge of the escutcheon ("P" in Figure 27). Insert a thin blade screwdriver into this notch between the escutcheon and the cabinet proper being careful not to mar the surface. Force the escutcheon upward, causing it to disen-

gage the first stud. Grasp the escutcheon along the top, lifting to disengage second stud. Remove escutcheon.

6. Remove (4) screws holding tape unit to front panel ("Q" in Figure 28).

7. Slide tape unit out through front panel (noting location of RFI shield on Model GR596W — "R" in Figure 26).

CAUTION: When replacing tape unit in Model GR596W be certain RFI shield is in proper location.

NOTE: Main unit should be in horizontal position when reinstalling tape unit.

TUNER CHASSIS REMOVAL

1. Proceed as for "Cabinet Bottom Removal".
2. Remove four (4) screws holding FM Antenna and Tape Bracket ("M" in Figure 26).
3. Unclip and disconnect cables ("D", "G", "N", and "U" in Figure 26).
4. Disconnect ground strap between tape and tuner chassis ("O" in Figure 26).
5. Remove six (6) knobs ("V" in Figure 27).
6. The tuner chassis mounting screws are covered by a "snap-off" escutcheon. Two notches will be found on the bottom of the outer edge of the escutcheon ("W" in Figure 27). Insert a thin blade screwdriver into these notches between the escutcheon and the cabinet proper being careful not to mar any surface. Force the escutcheon upward, causing it to disengage first two studs. Grasp the escutcheon along the top, lifting to disengage second two studs.
7. Remove four (4) screws holding tuner chassis to front panel ("X" in Figure 28).
8. Slide tuner chassis out through front panel (noting location of RFI shield on Model GR596W — "R" in Figure 26).

CAUTION: When replacing tuner chassis in Model GR596W be certain RFI shield is in proper location.

NOTE: Main unit should be in horizontal position when reinstalling tuner chassis.

ADDITIONAL DISASSEMBLY PROCEDURES

In addition to the disassembly procedure for Models G596W and GR596W outlined above, there are two other procedures (Groups "B" and "C" below) which apply to various "G" line models that also use the snap-off escutcheon and the out-front chassis removal concepts of the "E" and "F" line. On such models the escutcheon is held in place by three (or more depending on model) studs and clips. This method facilitates access for cleaning the back side of the escutcheon lens and also for access to chassis mounting screws. The chassis (and/or some tape units) may be removed thru the front of modular models, or thru the top mounting panel of console models.

GROUP "B" models include:

CHASSIS	3WGR50	CHASSIS	3WGR54
MODELS	G914P G915AE G916M	MODEL	G680W2
CHASSIS	3WGR52	CHASSIS	5WFR50
MODELS	G584W1 G587W2 GR587W1	MODEL	G904P
		CHASSIS	6WGR55
		MODEL	G920AE G922M

NOTE: In addition, the following "E" and "F" chassis and models follow the Group "B" procedure with one exception. Some models in Group "B" have screws holding the escutcheon from the inside. It would be necessary to remove such screws before attempting to remove the escutcheon. The use of these additional screws can be determined by viewing the escutcheon from the rear.

CHASSIS	5WER50	CHASSIS	15WER55
MODELS	E902W ET902W E903M, M2 ET903M, M2 E904DE ET904DE, DE2	MODELS	E911W E912M, M1 E913DE, DE1 E913P, P1 ET914W, W1 ET915DE ET915P, P1, P21 E921DE E921P E922M
CHASSIS	5WER51	CHASSIS	15WER56
MODELS	E584W, W1 E587W, W1 E588W	MODELS	E585J, J1 E586W, X E589W, W1 E594W, W1
CHASSIS	5WER53	CHASSIS	15WFR55
MODELS	E445W E680W E685W	MODELS	ET914W3 F914W ET915DE3 ET915P3 F915DE F915P F915DE1 F915P1 F916M F916PN
CHASSIS	5WFR50	CHASSIS	15WFR57
MODELS	F902W, W1 F903M F904DE F904P	MODELS	F585W F586X F589W F589X F594W
CHASSIS	5WFR51		
MODELS	F584W F587W F588W		
CHASSIS	5WFR53		
MODELS	F445W, W1 F680W F685W		
CHASSIS	15WFR51		
MODELS	F941DE F941P F942M F946AE F947P		

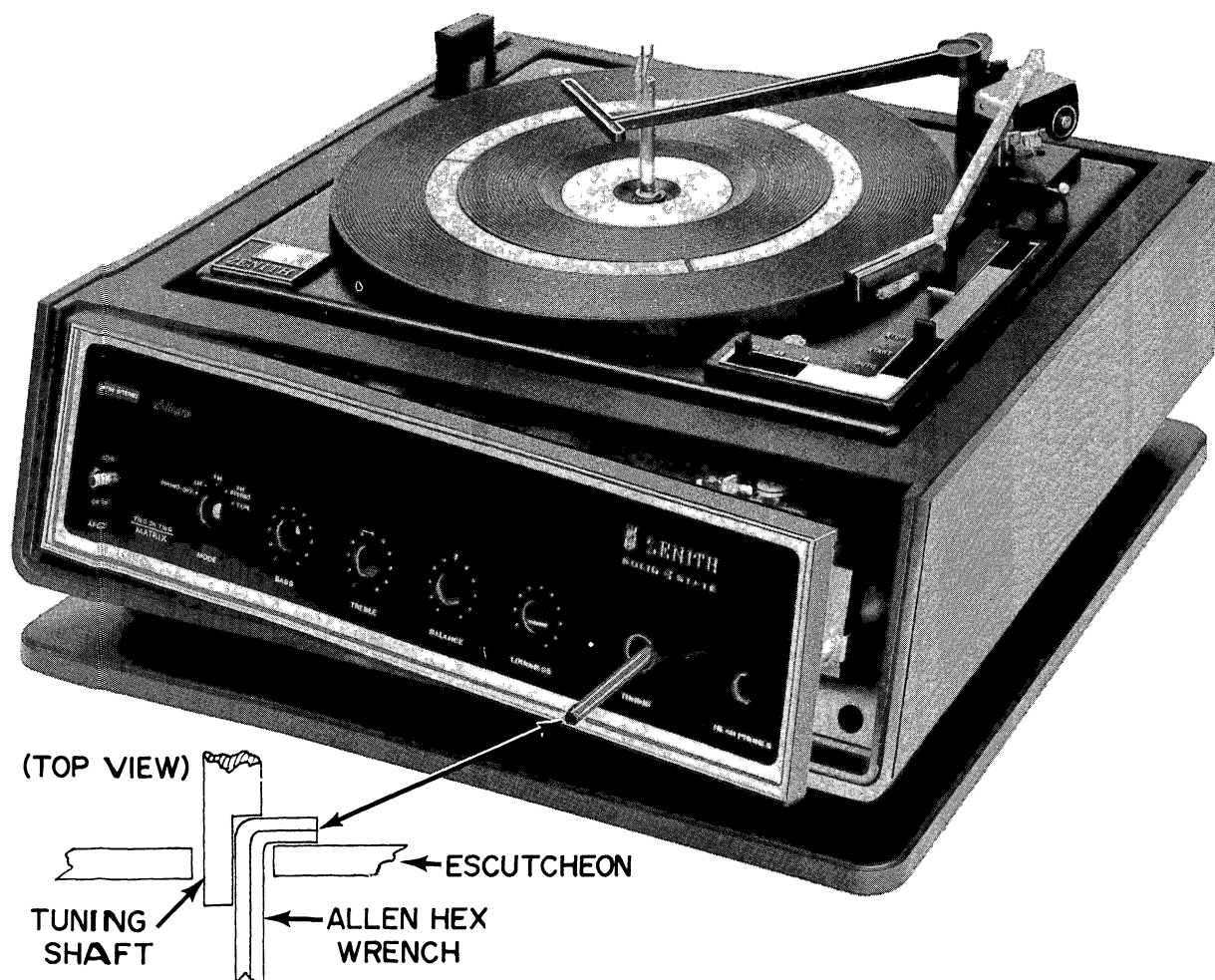


FIGURE 29 -- ESCUTCHEON REMOVAL -- GROUP "B"

Model G584W1 is representative of those models which have the above features, and will be used in the following explanation.

ESCUTCHEON REMOVAL -- GROUP "B"

Figure 29 illustrates the technique used:

1. Remove all knobs (except AFC) from the control panel.
2. Rotate tuning shaft so that the "flat" is vertical, and the cut-away portion is facing the headphone jack.
3. Referring to the top view in Figure 29, insert the short end of a 1/8" (size may vary) "L" shaped Allen hex wrench between the shaft and the escutcheon.
4. Position the short end of the wrench behind the escutcheon, with the wrench against the step of the shaft.
5. Moving wrench to left will apply pressure to the back of the escutcheon, causing the nearest stud and clip to disengage.
6. Remove wrench.
7. Grasp loosened end of escutcheon, and firmly pull escutcheon outward until all studs and clips are disengaged.

CAUTION -- Refer to Figure 30. On some models the Stereo Indicator and Digilite Indicator lamps are mounted in grommets on the chassis, while on other models these lamps (in grommets) are fitted into the escutcheon.

8. Escutcheon is now removed.

OUT FRONT CHASSIS REMOVAL -- GROUP "B"

Figure 30 identifies the location of certain components involved. While Model G584W1 is representative of the disassembly procedure for the above models, there are some minor variations that must be noted. These variations will be denoted with the model number and variation shown in ().

1. Remove escutcheon as explained above.
2. Remove screws holding cabinet back and remove back (E584W, E585J, J1, E586W, X, F584W, F585W, F586X, G584W1 -- Remove screws holding cabinet bottom, and remove bottom).
3. Unmount both the Speaker Jack Assembly Bracket and the Antenna/Tape/Phono Connector Assembly Bracket from the cabinet back.

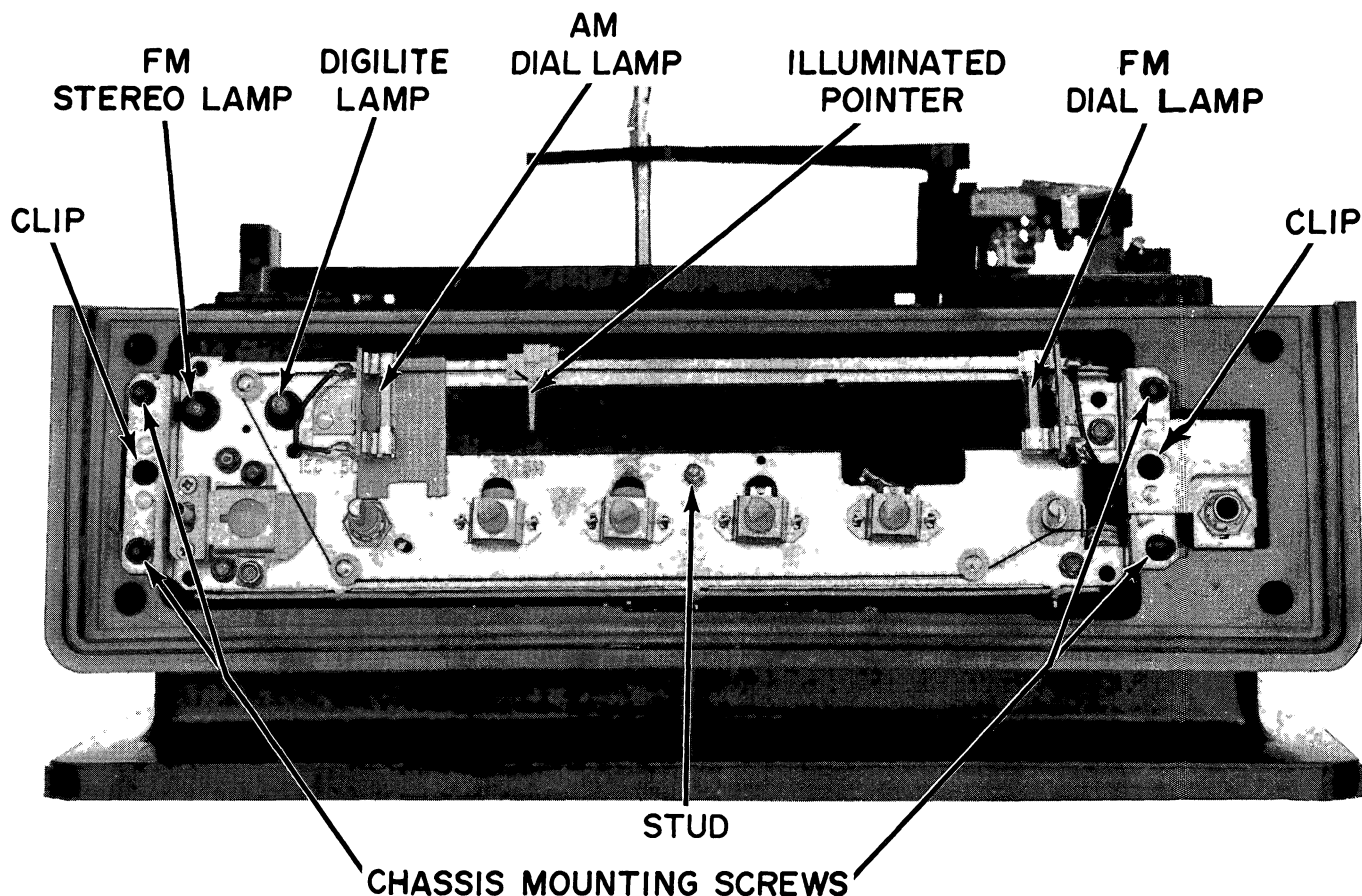


FIGURE 30 — OUT FRONT CHASSIS REMOVAL — GROUP "B"

4. Untie cable retainers. (Disconnect record changer and tape unit cables when used.)
5. Remove one screw from bottom of cabinet under center of chassis (E584W, — Two screws.) (E585J, J1, E586W, X, F584W, F585W, F586W, G584W1 — Four screws to remove bottom base, then two screws under chassis.) (E587W, W1, E680W, F587W, F680W, G587W2, GR587W1, G680W2 — Also four screws under tape assembly.)
6. Remove four screws from front of chassis. (E587W, W1, E680W, F587W, F680W, G587W2, GR587W1, G680W2 — Tape unit is secured to radio chassis with a bracket. There are two additional screws to the left of the tape unit.)
7. Slide radio chassis (E587W, W1, E680W, F587W, F680W, G680W, G587W2, GR587W1, G680W2 — Tape unit is mounted to radio chassis with a bracket), with attached brackets and cables, out thru front of cabinet.

This completes chassis removal.

When reinstalling chassis, be certain to reconnect cables, retie cable retainers, etc.

ESCUTCHEON REMOVAL — GROUP "C"

CHASSIS	6WGR56	CHASSIS	6WGR57
MODEL	GR684W	MODE LS	G590W
			GR590W
			GR591W

Models identified in Group "C" have access provisions similar to those in Group "B" above, with the significant difference being in the method of escutcheon removal.

Figure 31 illustrates the technique used :

1. Remove all knobs (except Power, AFC and Matrix). Also remove the nut on the headphone jack.
2. Group "C" models have three notches formed into the under side of the escutcheon (visible from the bottom).
3. Insert screwdriver blade into this notch, between the escutcheon and the cabinet proper, being careful not to mar the surface. Force the escutcheon outward, causing it to disengage each stud.
4. Remove the escutcheon.

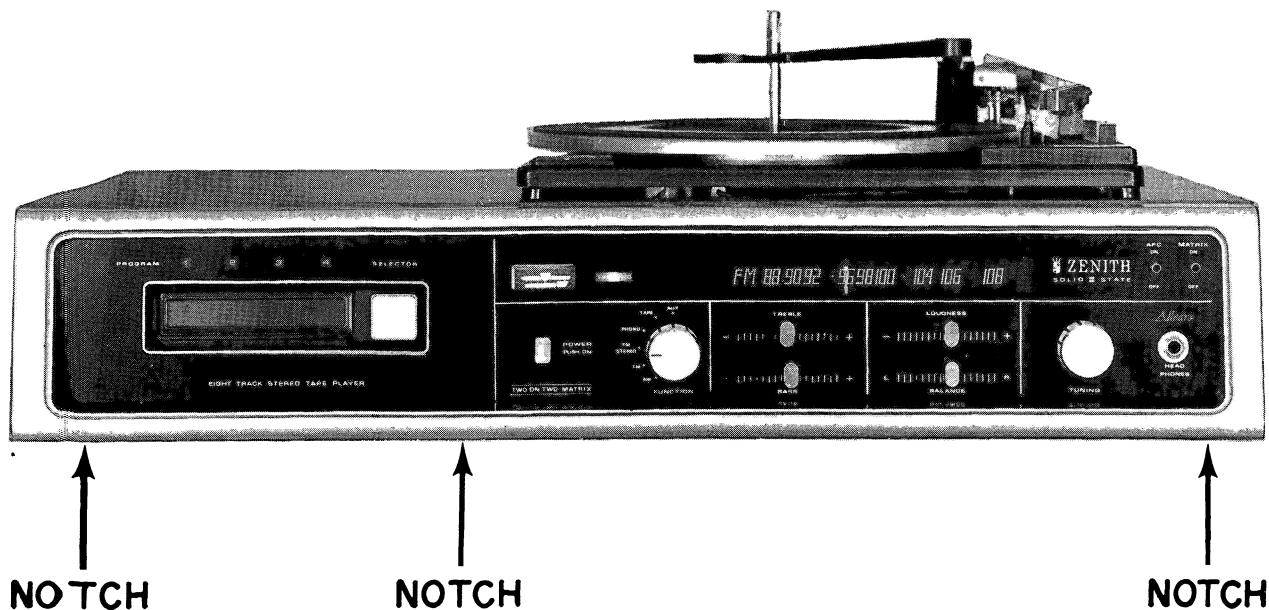


FIGURE 31 – ESCUTCHEON REMOVAL – GROUP “C”

OUT FRONT CHASSIS REMOVAL – GROUP “C”

1. Remove escutcheon as explained above.
2. Remove screws holding cabinet back, and remove back.
3. Unmount both the Speaker Jack Assembly Bracket and the Antenna/Tape/Phone Connector Assembly Bracket from the cabinet back.
4. Untie cable retainers. (Disconnect record changer and tape unit cables when used.)
5. Remove three screws from bottom of cabinet under tuner chassis, then four screws under tape assembly.

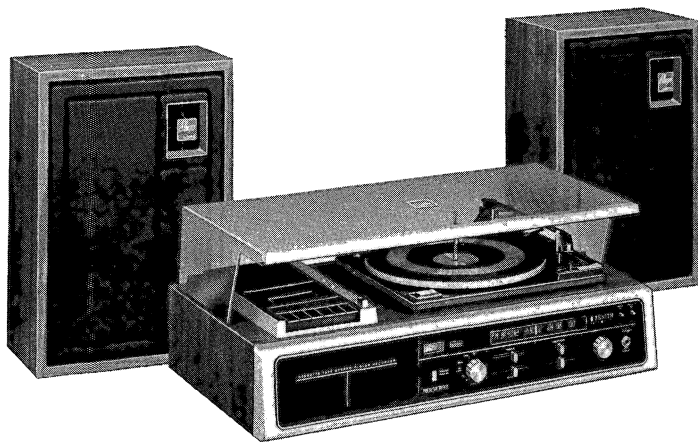
6. Remove three screws from front of chassis. Tape unit is secured to radio chassis with a bracket (G590W, GR590W, GR684W).

7. Slide radio chassis (Tape unit is mounted to radio chassis with a bracket), with attached brackets and cables, out thru front of cabinet.

This completes chassis removal.

When reinstalling chassis, be certain to reconnect cables, retie cable retainers, etc.

7. This comple



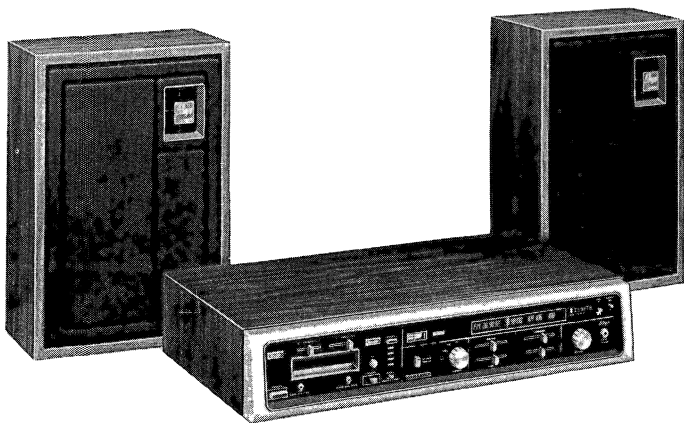
GR591W



GR590W



G680W



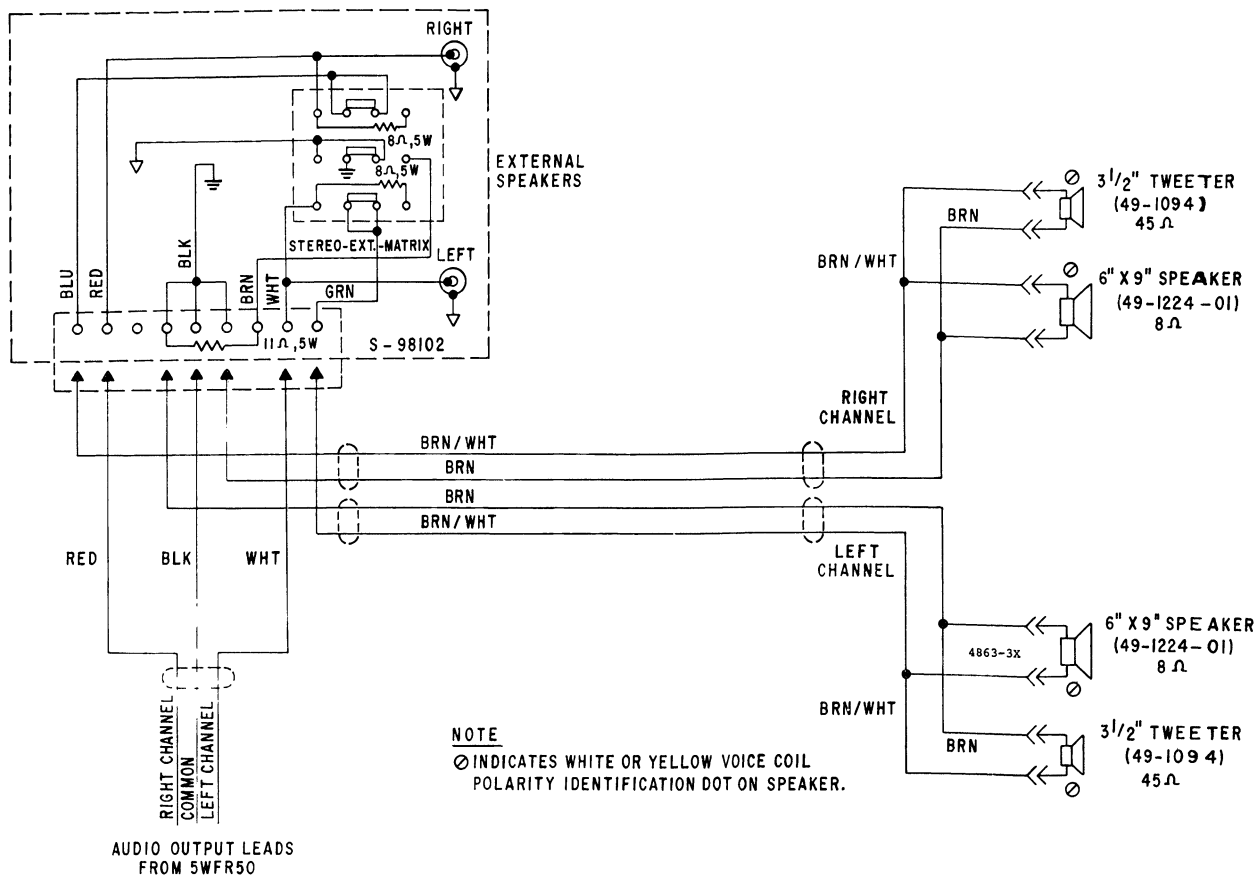
GR684W



G9026W

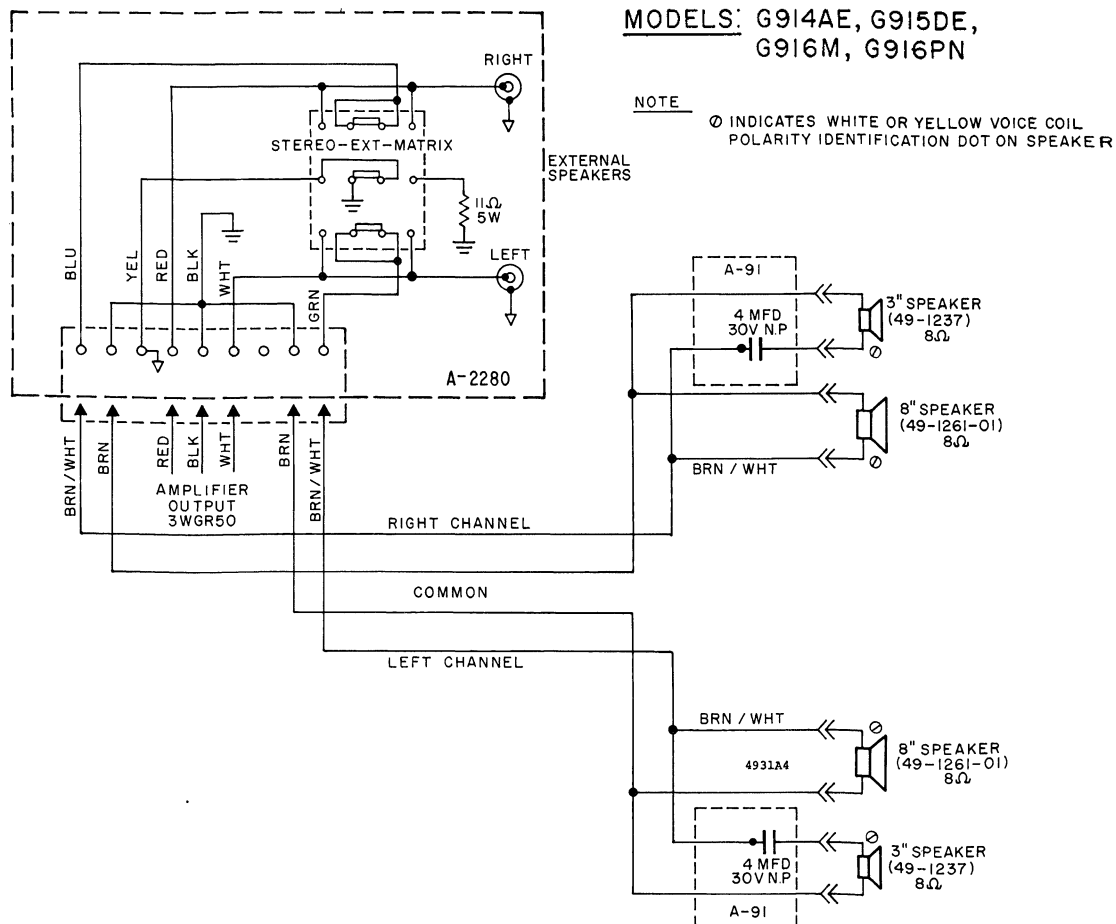
NOTE - MODULAR MODELS
ARE SHOWN WITH OPTIONAL
ALLEGRO SPEAKER SYSTEMS.

REPRESENTATIVE MODEL ILLUSTRATIONS

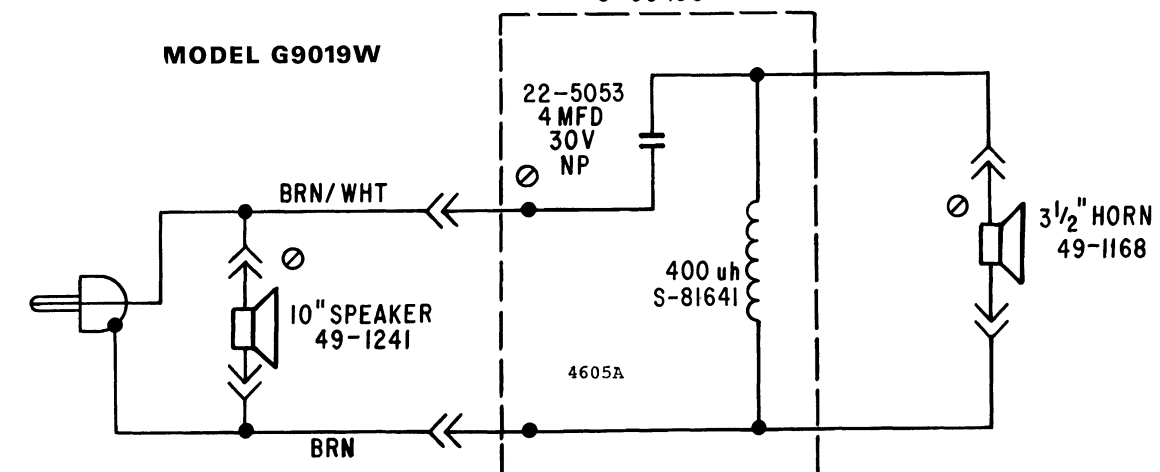
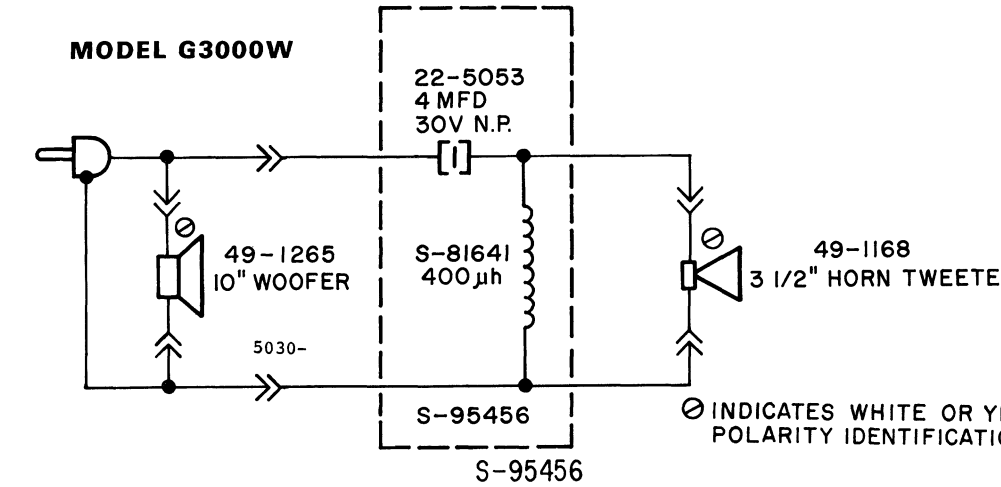
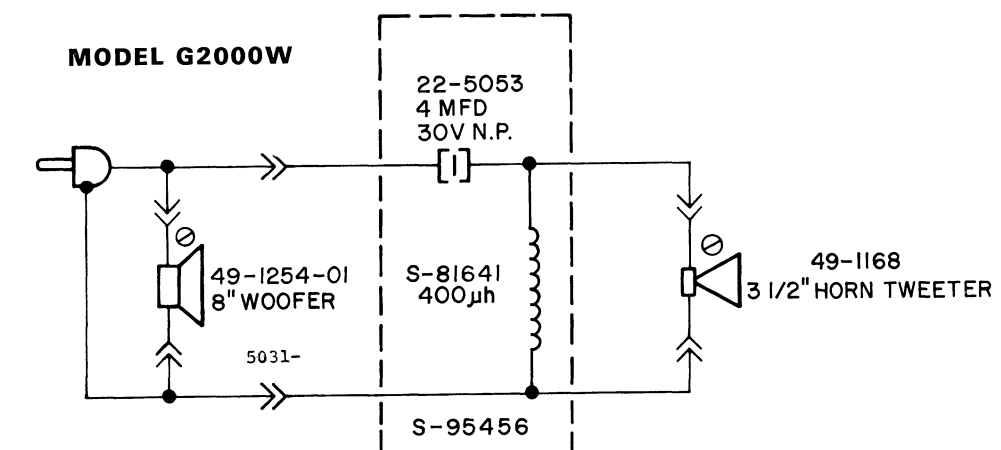
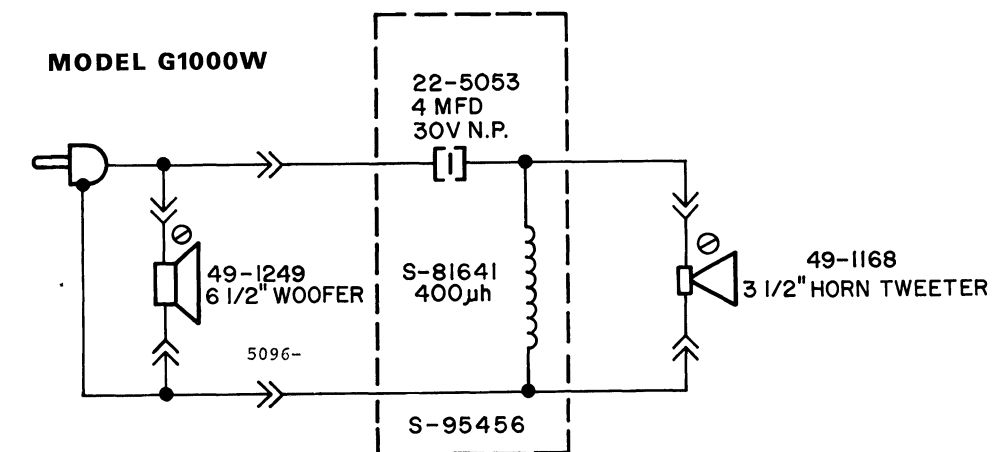
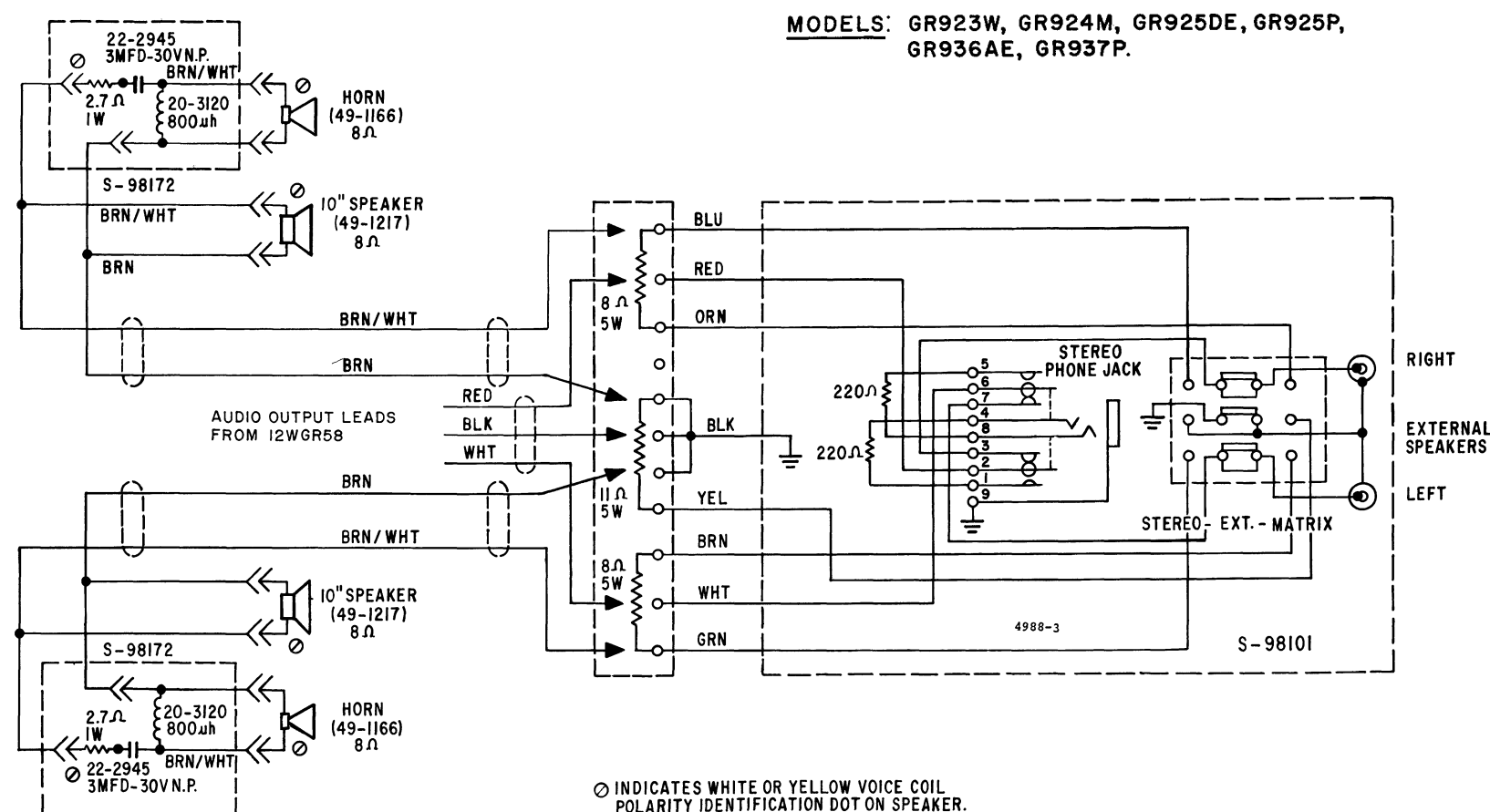
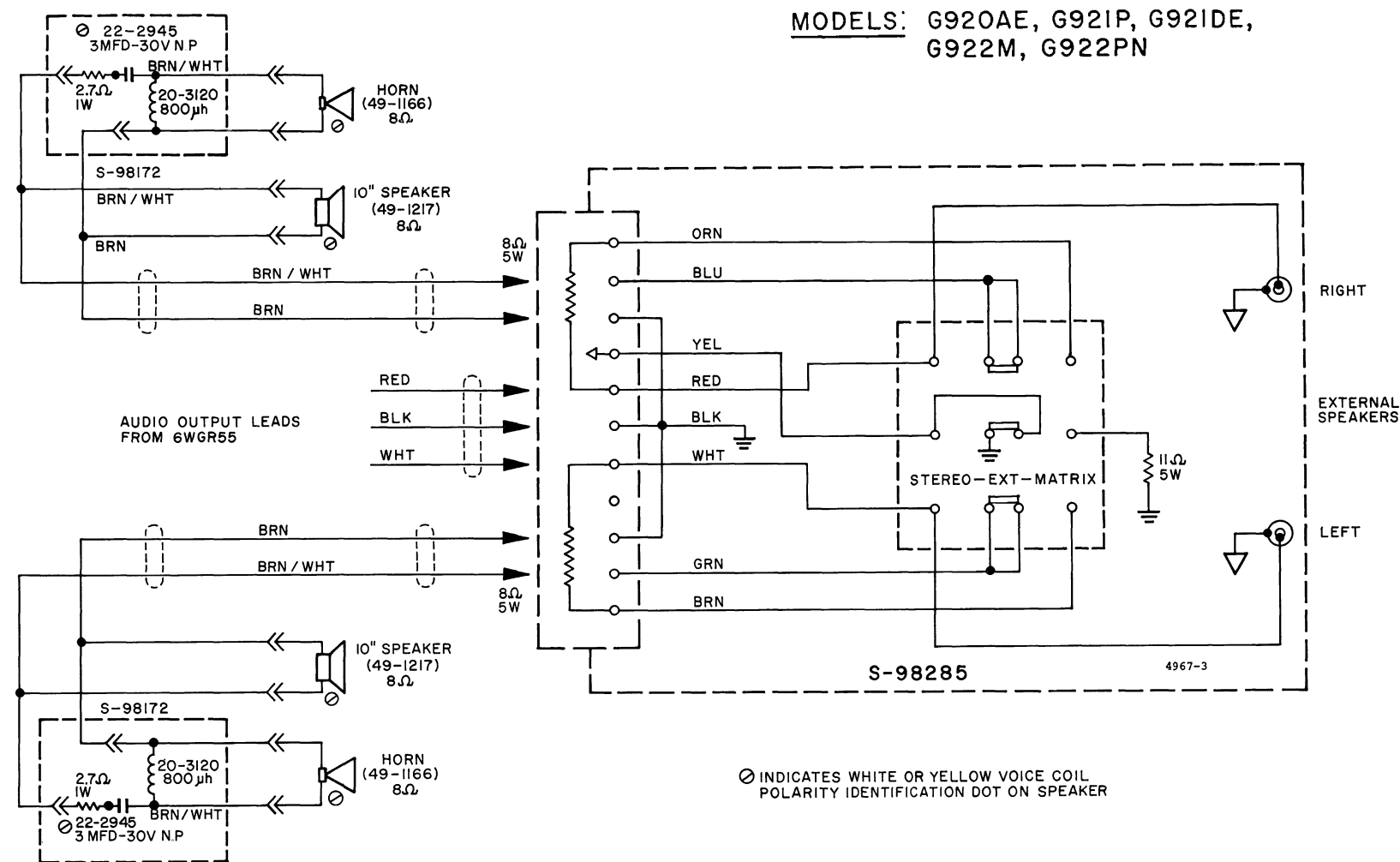


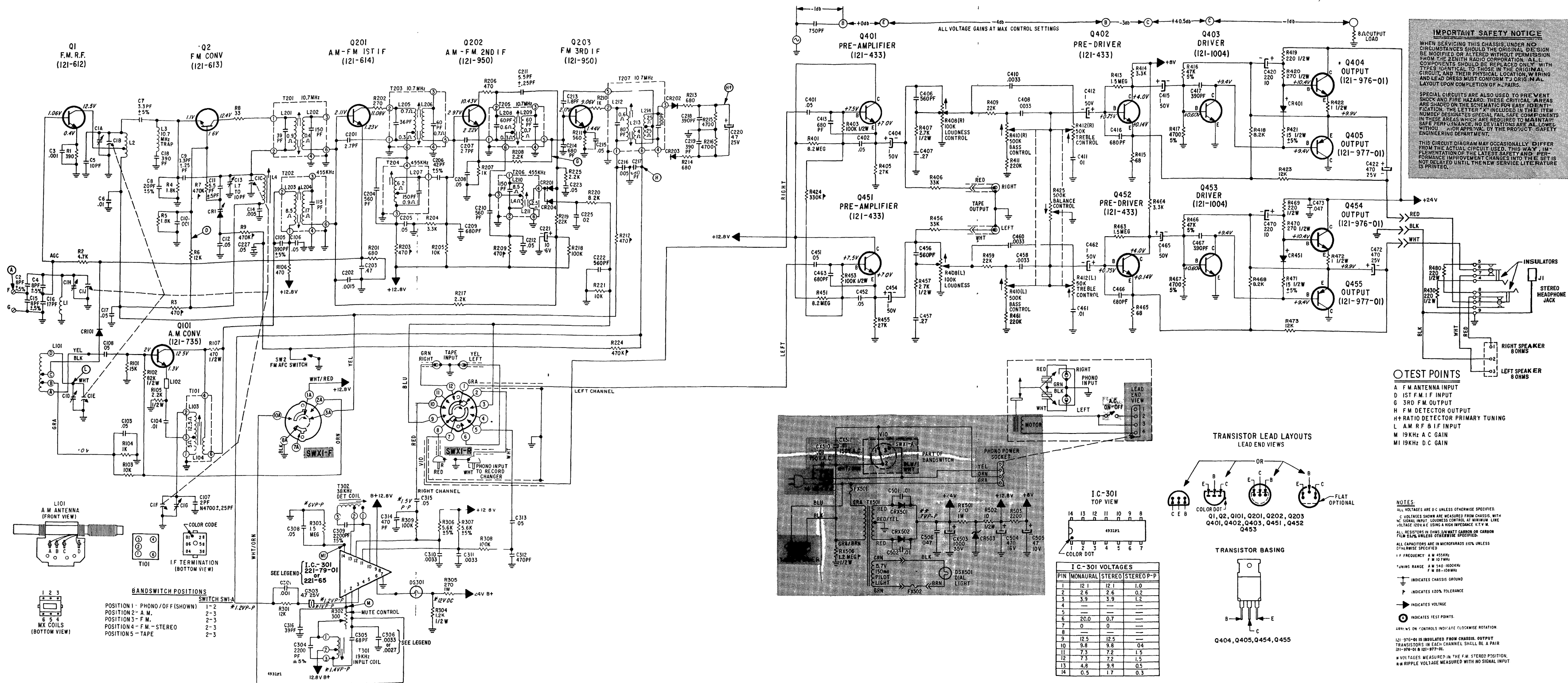
AUDIO OUTPUT LEADS FROM 5WFR50

MODELS: G914AE, G915DE, G916M, G916PN

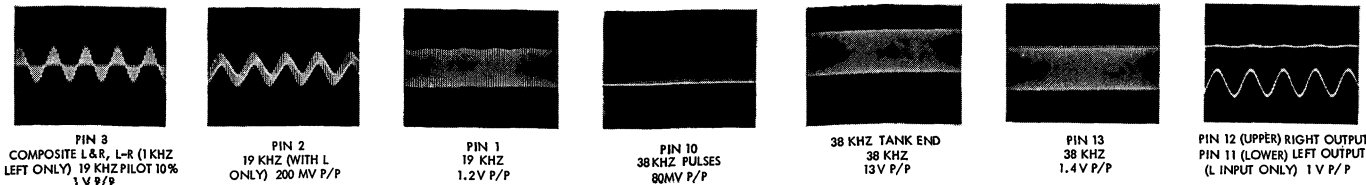


SPEAKER WIRING SCHEMATICS





IC 301 WAVE FORMS

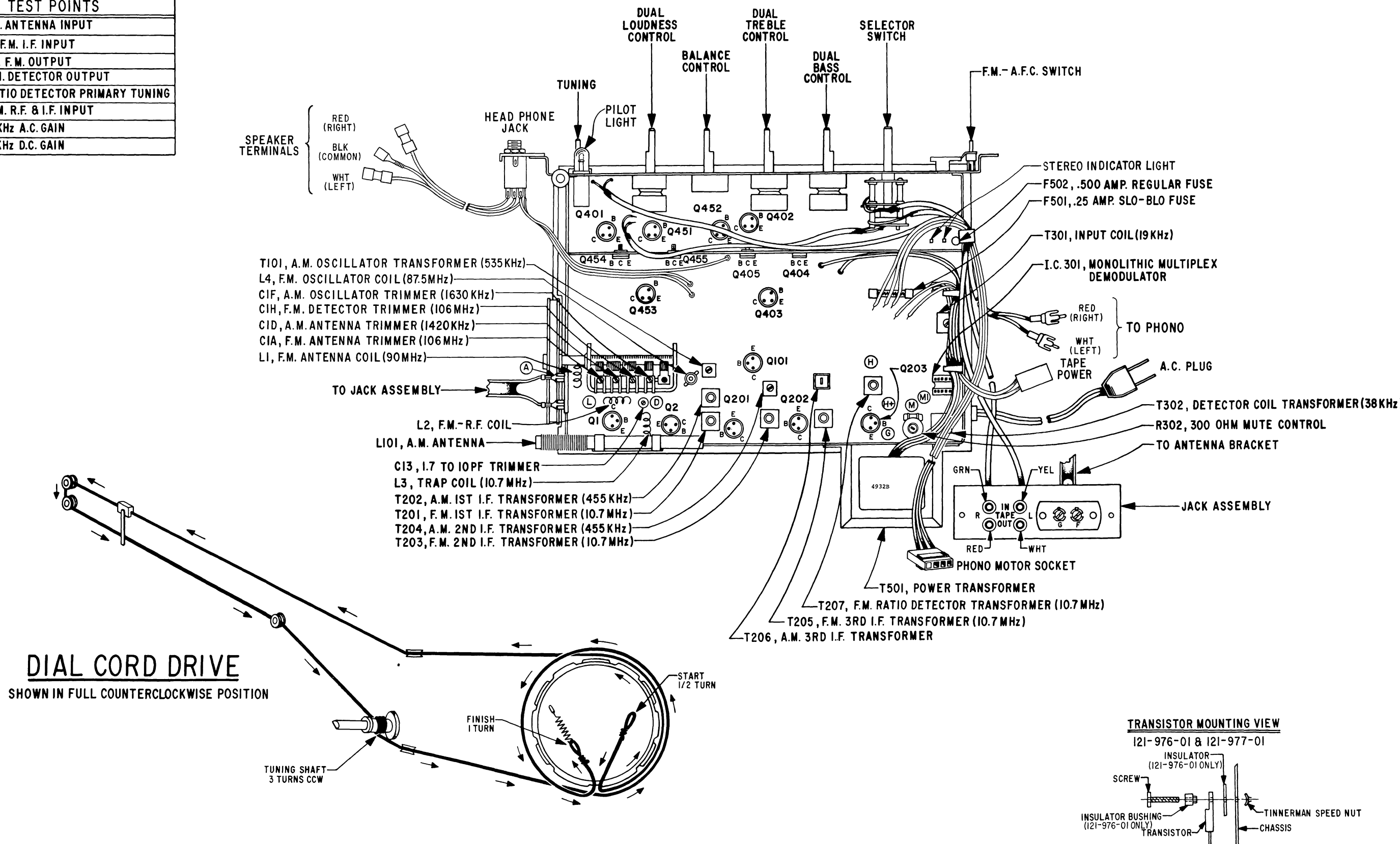


ITEM NO	PART NUMBER	DESCRIPTION	ITEM NO	PART NUMBER	DESCRIPTION
C1A	22-7-134	FM DETECTOR TRIMMER	R218	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C1B		FM OSCILLATOR TUNING	R219	83-9922-04	10K OHM 5% (ALT. 63-7862 1/2W 10%)
C1C		AM ANTENNA TRIMMER	R220	83-9921-90	8.2K OHM 5% (ALT. 63-7788 1/2W 10%)
C1D		FM ANTENNA TRIMMER	R221	83-9922-36	10K OHM 5% (ALT. 63-7788 1/2W 10%)
C1E		AM OSCILLATOR TUNING	R222	83-9922-36	10K OHM 5% (ALT. 63-7788 1/2W 10%)
C1F		AM OSCILLATOR TRIMMER	R225	83-9921-90	2.2K OHM 5% (ALT. 63-7792 1/2W 10%)
C1G		FM ANTENNA TRIMMER	R301	83-9921-98	12K OHM 5% (ALT. 63-7831 1/2W 10%)
C1H	22-2-2481	FM ANTENNA TRIMMER	R302	83-9922-04	300 OHM MUTE CONTROL
C1I	22-2-2481	FM ANTENNA TRIMMER	R303	83-9922-48	10K OHM 5% (ALT. 63-7915 1/2W 10%)
C2	22-2-2728	0.01 MFD DISC 25V	R304	63-1789	1.2K OHM 1/2W 10%
C3	22-2-2728	0.01 MFD DISC 25V	R306	63-1789	1.2K OHM 1/2W 10%
C4	22-2-2728	8 PF DISC 1.05V 500V	R307	63-1789	1.2K OHM 1/2W 10%
C5	22-2-2728	10 PF DISC 1.05V 500V	R308	63-1789	1.2K OHM 1/2W 10%
C6	22-3-3303	0.1 MFD DISC 25V	R309	83-9921-90	5.6K OHM 5% (ALT. 63-7816 1/2W 5%)
C7	22-3-3303	0.1 MFD DISC 25V	R310	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C8	22-3-3303	0.1 MFD DISC 25V	R311	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C9	22-3-3303	0.1 MFD DISC 25V	R312	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C10	22-3-3303	0.1 MFD DISC 25V	R313	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C11	22-3-3303	0.1 MFD DISC 25V	R314	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C12	22-3-3303	0.1 MFD DISC 25V	R315	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C13	22-3-3303	0.1 MFD DISC 25V	R316	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C14	22-3-3303	0.1 MFD DISC 25V	R317	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C15	22-3-3303	0.1 MFD DISC 25V	R318	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C16	22-3-3303	0.1 MFD DISC 25V	R319	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C17	22-3-3303	0.1 MFD DISC 25V	R320	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C18	22-3-3303	0.1 MFD DISC 25V	R321	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C19	22-3-3303	0.1 MFD DISC 25V	R322	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C20	22-3-3303	0.1 MFD DISC 25V	R323	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C21	22-3-3303	0.1 MFD DISC 25V	R324	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C22	22-3-3303	0.1 MFD DISC 25V	R325	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C23	22-3-3303	0.1 MFD DISC 25V	R326	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C24	22-3-3303	0.1 MFD DISC 25V	R327	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C25	22-3-3303	0.1 MFD DISC 25V	R328	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C26	22-3-3303	0.1 MFD DISC 25V	R329	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C27	22-3-3303	0.1 MFD DISC 25V	R330	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C28	22-3-3303	0.1 MFD DISC 25V	R331	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C29	22-3-3303	0.1 MFD DISC 25V	R332	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C30	22-3-3303	0.1 MFD DISC 25V	R333	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C31	22-3-3303	0.1 MFD DISC 25V	R334	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C32	22-3-3303	0.1 MFD DISC 25V	R335	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C33	22-3-3303	0.1 MFD DISC 25V	R336	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C34	22-3-3303	0.1 MFD DISC 25V	R337	83-9922-20	100K OHM 5% (ALT. 63-7862 1/2W 10%)
C35	22-3-3303	0.			

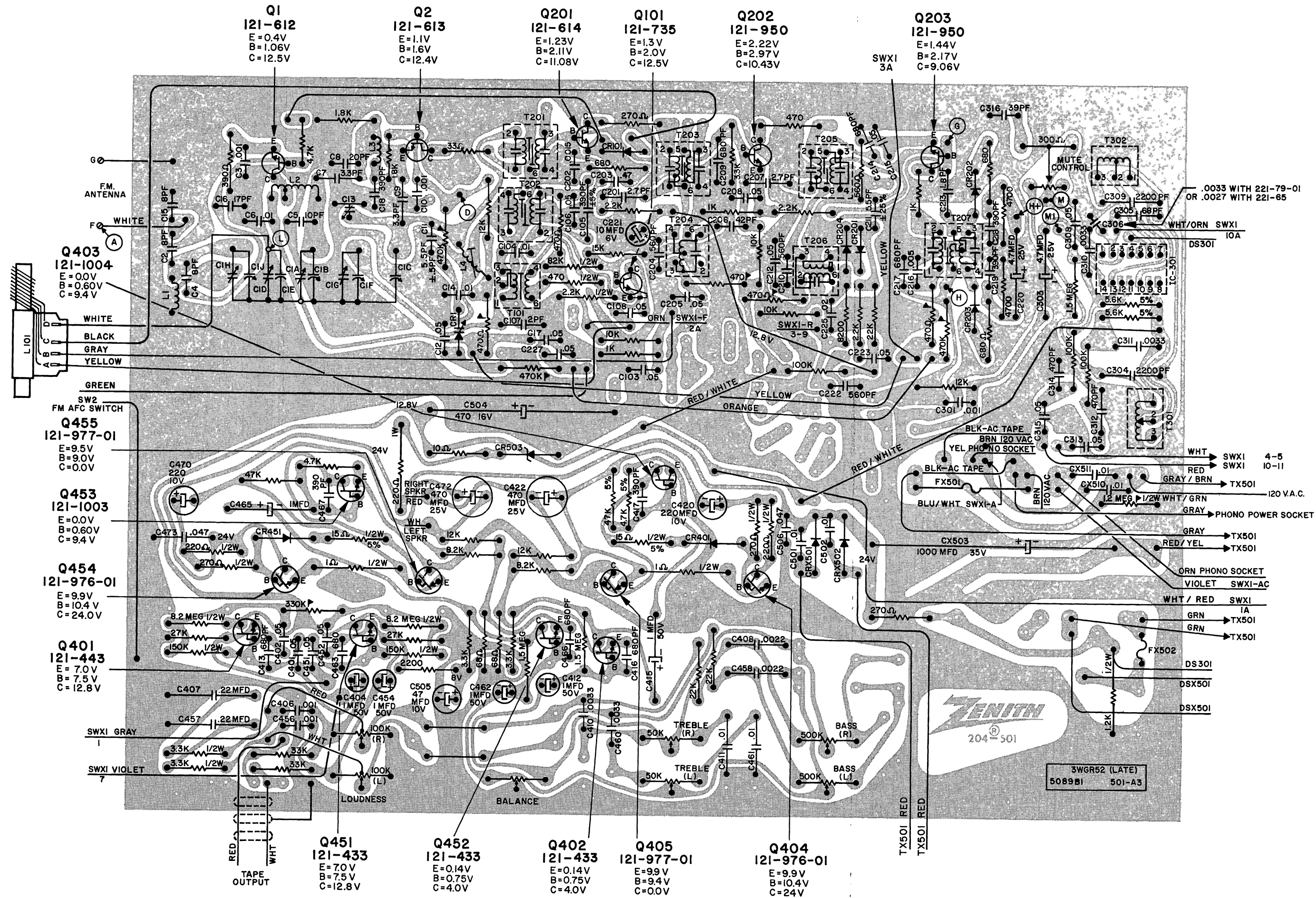


TRANSISTORS		
No.	PART No.	DESCRIPTION
Q1	121-612	F.M.-R.F.
Q2	121-613	F.M. CONVERTER
Q101	121-735	A.M. CONVERTER
Q201	121-614	A.M.-F.M. 1st I.F.
Q202	121-950	A.M.-F.M. 2nd I.F.
Q203		F.M. 3rd I.F.
Q401	121-433	PRE-AMPLIFIER
Q402		PRE-DRIVER
Q403	121-1004	DRIVER
Q404	121-976-01	OUTPUT
Q405	121-977-01	
Q451	121-433	PRE-AMPLIFIER
Q452		PRE-DRIVER
Q453	121-1004	DRIVER
Q454	121-976-01	OUTPUT
Q455	121-977-01	
IC3 01	221-79-01 or 221-65	MULTIPLEX DEMODULATOR

TEST POINTS	
A	F.M. ANTENNA INPUT
D	1st F.M. I.F. INPUT
G	3rd F.M. OUTPUT
H	F.M. DETECTOR OUTPUT
H+	RATIO DETECTOR PRIMARY TUNING
L	A.M. R.F. & I.F. INPUT
M	19KHz A.C. GAIN
MI	19KHz D.C. GAIN



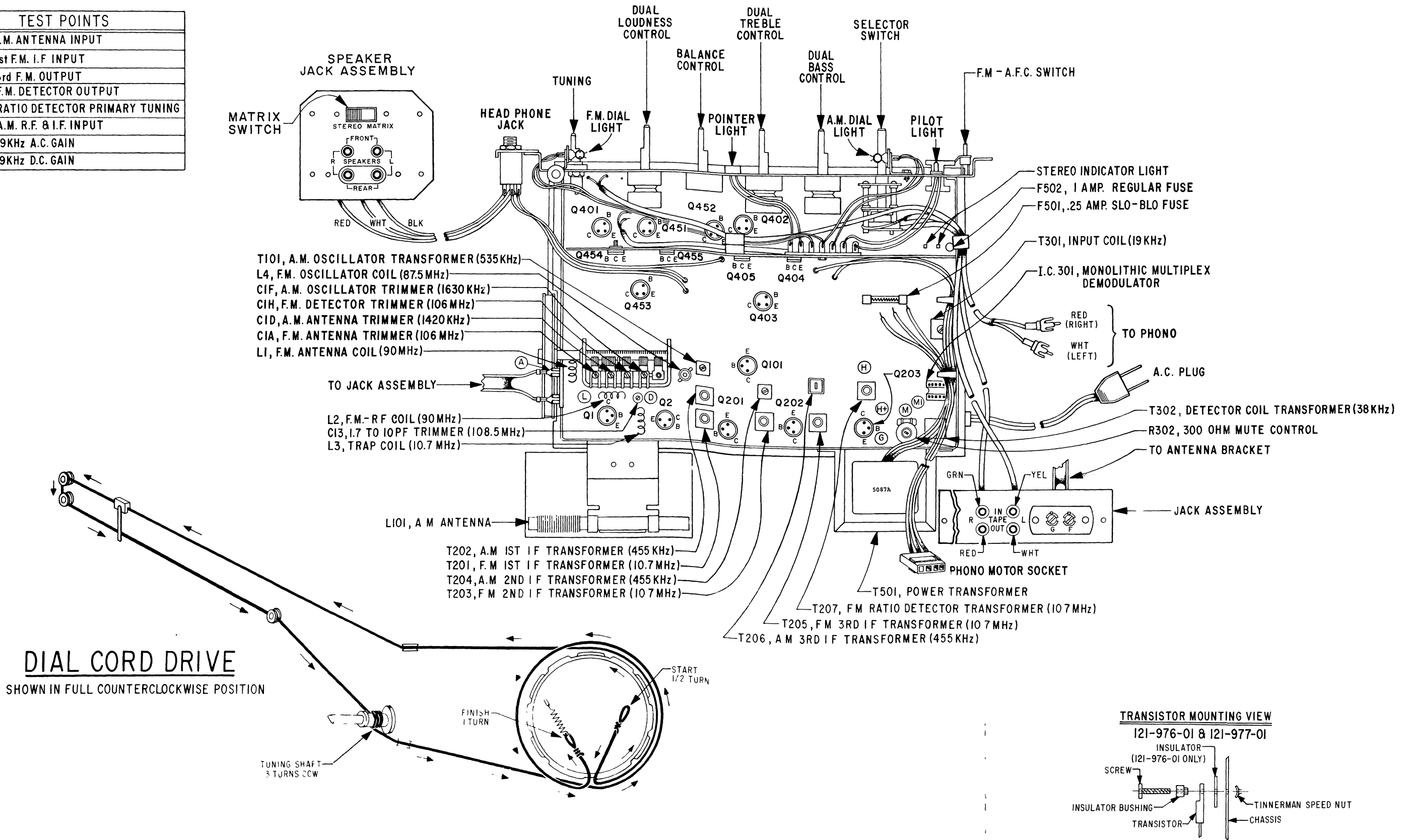
[illegible]



CHASSIS 3WGR52 - CHASSIS WIRING AND COMPONENTS VIEWED FROM FOIL SIDE - LATE PRODUCTION

TRANSISTORS		
No.-	PART No.	DESCRIPTION
Q1	121-612	F.M. - R.F.
Q2	121-613	F.M. CONVERTER
Q101	121-735	A.M. CONVERTER
Q201	121-614	A.M.-F.M. 1st I.F.
Q202	121-950	A.M.-F.M. 2nd I.F.
Q203		F.M. 3rd I.F.
Q401	121-433	PRE-AMPLIFIER
Q402		PRE-DRIVER
Q403	121-1004	DRIVER
Q404	121-976	OUTPUT
Q405	121-977	PRE-AMPLIFIER
Q451	121-433	PRE-AMPLIFIER
Q452		PRE-DRIVER
Q453	121-1004	DRIVER
Q454	121-976-01	OUTPUT
Q455	121-977-01	OUTPUT
IC3 01	221-79-01 or 221-65	MULTIPLEX DEMODULATOR

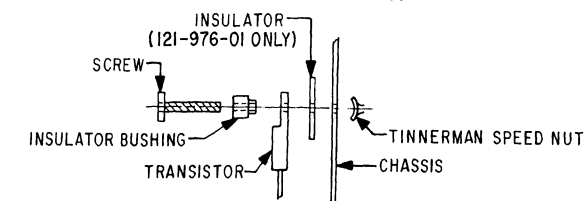
TEST POINTS	
A	F.M. ANTENNA INPUT
D	1st F.M. I.F. INPUT
G	3rd F.M. OUTPUT
H	F.M. DETECTOR OUTPUT
H+	RATIO DETECTOR PRIMARY TUNING
L	A.M. R.F. & I.F. INPUT
M	19KHz A.C. GAIN
MI	19KHz D.C. GAIN



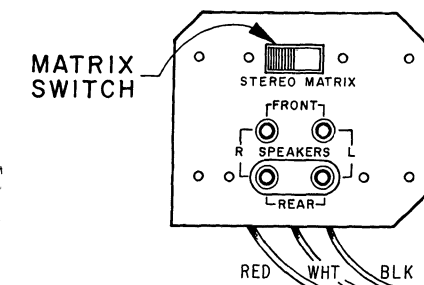
TRANSISTORS		
No.	PART No.	DESCRIPTION
Q1	121-612	F.M.-R.F.
Q2	121-613	F.M. CONVERTER
Q101	121-735	A.M. CONVERTER
Q201	121-614	A.M.-F.M. 1st I.F.
Q202	121-950	A.M.-F.M. 2nd I.F.
Q203		F.M. 3rd I.F.
Q401	121-433	PRE-AMPLIFIER
Q402		PRE-DRIVER
Q403	121-1004	DRIVER
Q404	121-976-01	OUTPUT
Q405	121-977-01	OUTPUT
Q451	121-433	PRE-AMPLIFIER
Q452		PRE-DRIVER
Q453	121-1004	DRIVER
Q454	121-976-01	OUTPUT
Q455	121-977-01	OUTPUT
IC301	221-79-01 or 221-65	MULTIPLEX DEMODULATOR

TEST POINTS	
A	F.M. ANTENNA INPUT
D	1st F.M. I.F. INPUT
G	3rd F.M. OUTPUT
H	F.M. DETECTOR OUTPUT
H+	RATIO DETECTOR PRIMARY TUNING
L	A.M. R.F. & I.F. INPUT
M	19KHz A.C. GAIN
MI	19KHz D.C. GAIN

TRANSISTOR MOUNTING VIEW
121-976-01 & 121-977-01



SPEAKER JACK ASSEMBLY



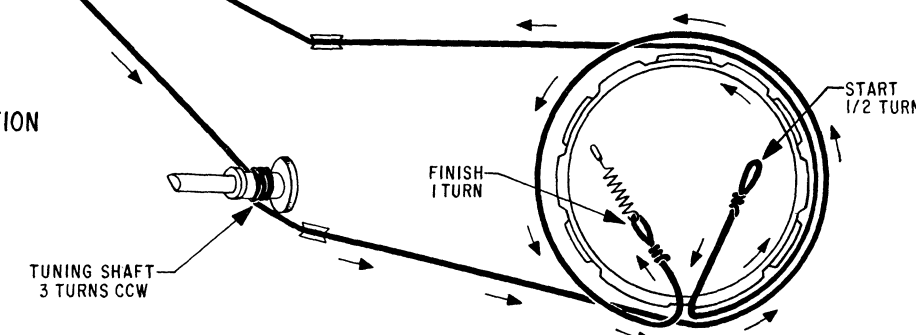
- T101, A.M. OSCILLATOR TRANSFORMER (535 KHz)
- L4, F.M. OSCILLATOR COIL (87.5 MHz)
- C1F, A.M. OSCILLATOR TRIMMER (1630 KHz)
- C1H, F.M. DETECTOR TRIMMER (106 MHz)
- C1D, A.M. ANTENNA TRIMMER (1420 KHz)
- C1A, F.M. ANTENNA TRIMMER (106 MHz)
- L1, F.M. ANTENNA COIL (90 MHz)

TO JACK ASSEMBLY

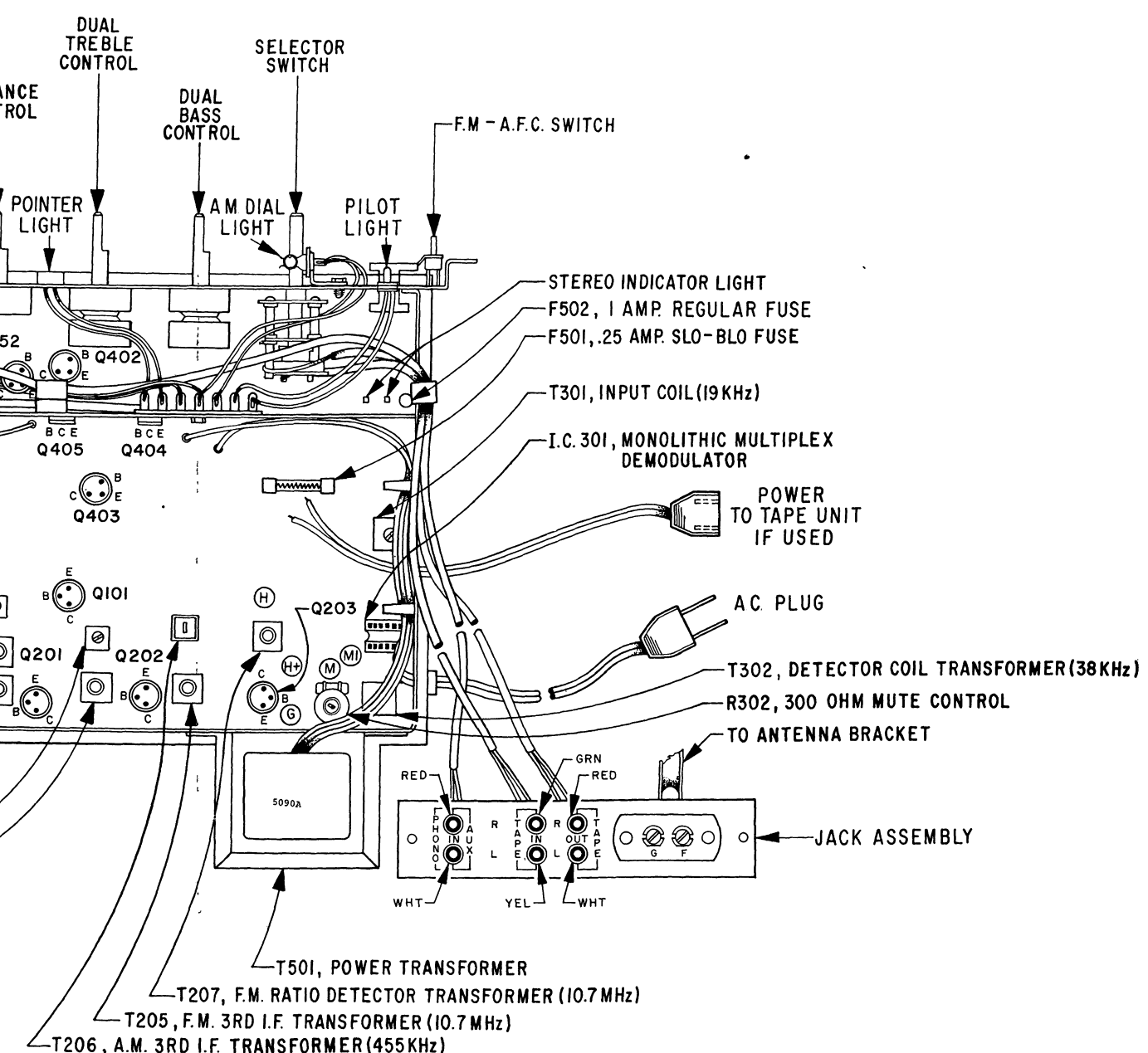
- L2, F.M.-R.F. COIL (90 MHz)
- L101, A.M. ANTENNA

- C13, 1.7 TO 10PF TRIMMER (108.5 MHz)
- L3, TRAP COIL (10.7 MHz)
- T202, A.M. 1ST I.F. TRANSFORMER (455 KHz)
- T201, F.M. 1ST I.F. TRANSFORMER (10.7 MHz)
- T204, A.M. 2ND I.F. TRANSFORMER (455 KHz)
- T203, F.M. 2ND I.F. TRANSFORMER (10.7 MHz)

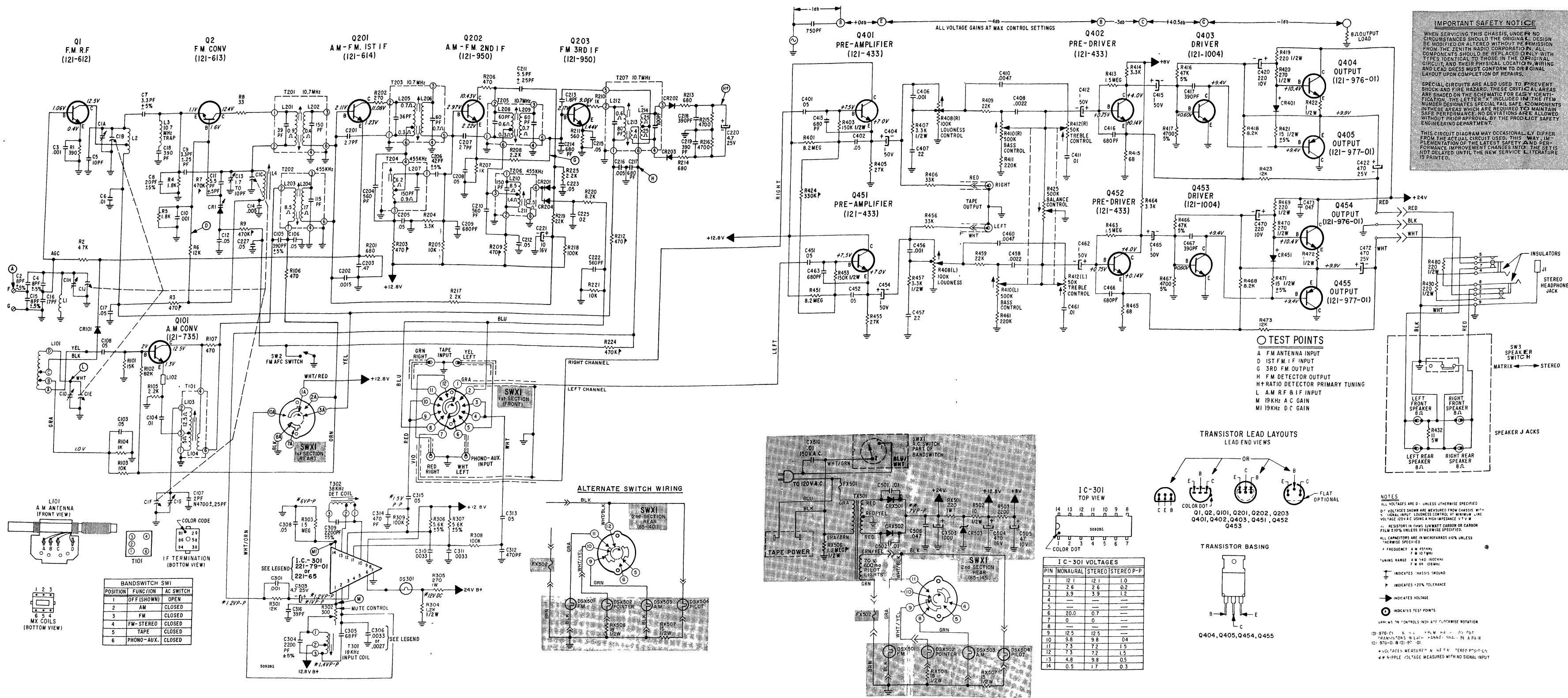
DIAL CORD DRIVE
SHOWN IN FULL COUNTERCLOCKWISE POSITION



CHASSIS 3WGR54 - CHASSIS LAYOUT







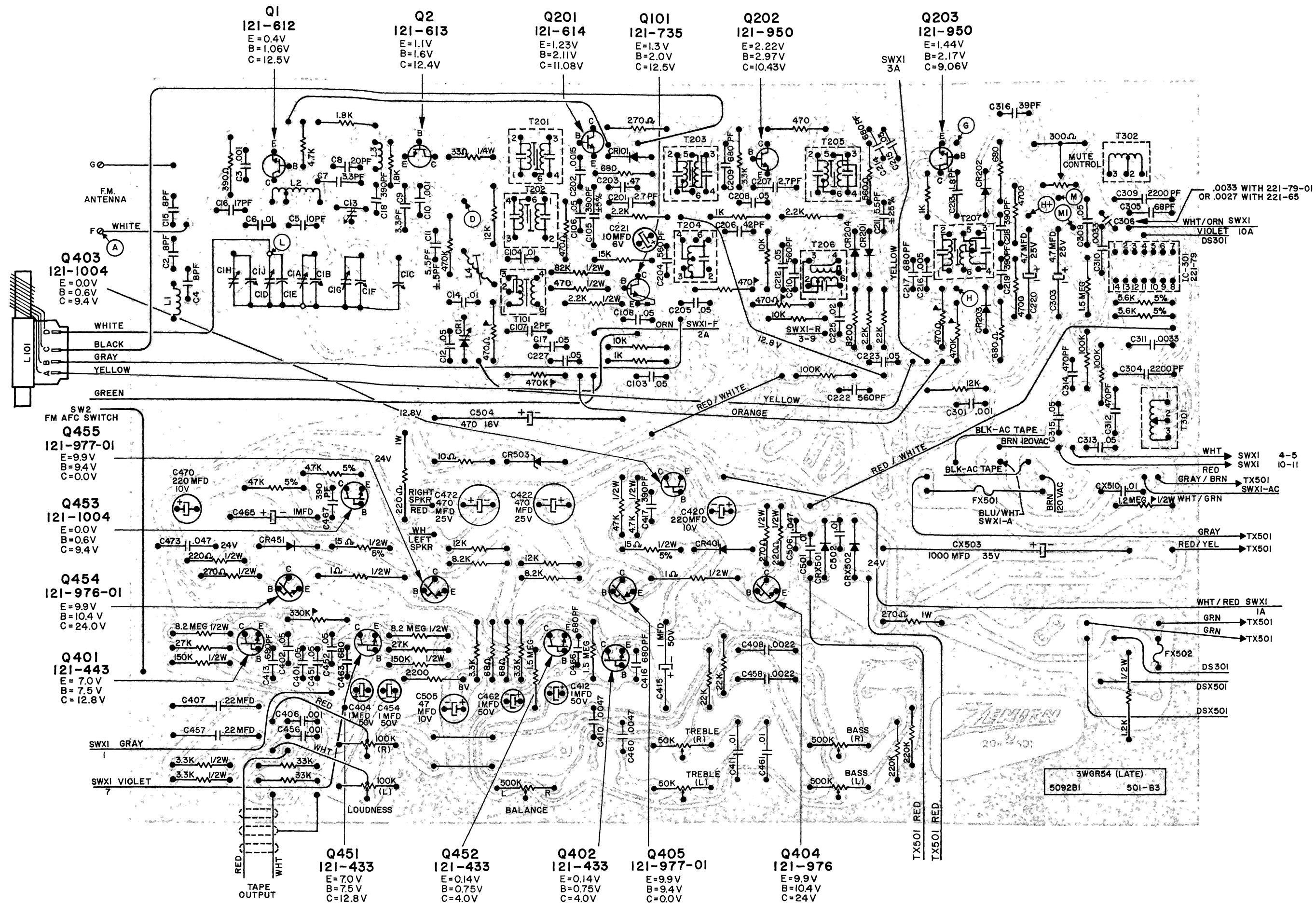
IMPORTANT SAFETY NOTICE

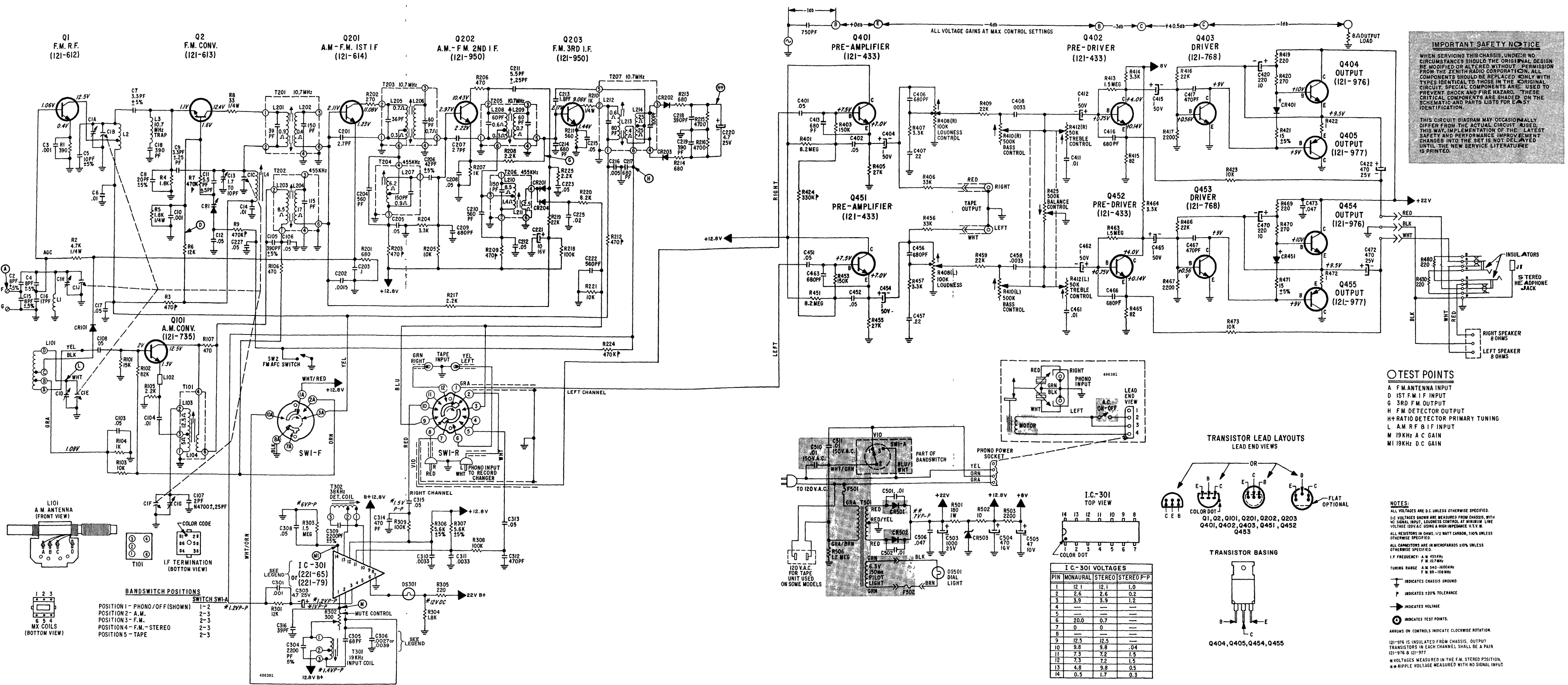
WHEN SERVICING THIS CHASSIS, UNDER NO CIRCUMSTANCES SHOULD THE ORIGINAL DESIGN BE MODIFIED OR ALTERED WITHOUT PERMISSION FROM THE ZENITH RADIO CORPORATION. ALL COMPONENTS SHOULD BE REPLACED ONLY WITH TYPES IDENTICAL TO THOSE IN THE ORIGINAL CIRCUIT, AND THEIR PHYSICAL LOCATION, WIRING AND LEAD DRESS MUST CONFORM TO ORIGINAL LAYOUT UPON COMPLETION OF REPAIRS.

SPECIAL CIRCUITS ARE ALSO USED TO PREVENT SHOCK AND FIRE HAZARD. THESE CRITICAL AREAS ARE SHOWN ON THE SCHEMATIC FOR EASY IDENTIFICATION. THE LETTER "X" INCLUDED IN THE ITEM NUMBER DESIGNATES SPECIAL FAULT-SAFE COMPONENTS IN THESE AREAS WHICH ARE REQUIRED TO MAINTAIN SAFE PERFORMANCE. NO DEVIATIONS ARE ALLOWED WITHOUT PRIOR APPROVAL BY THE PRODUCT SAFETY ENGINEERING DEPARTMENT.

THIS CIRCUIT DIAGRAM MAY OCCASIONALLY DIFFER FROM THE ACTUAL CIRCUIT USED. THIS WAY OF IMPLEMENTATION OF THE LATEST SAFETY AND PERFORMANCE IMPROVEMENT CHANGES INTO THE SET IS NOT DELAYED UNTIL THE NEW SERVICE LITERATURE IS PRINTED.

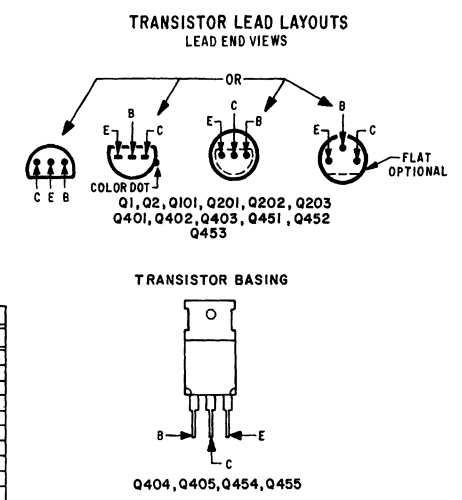
	ITEM NO.	PART NUMBER	DESCRIPTION	ITEM NO.	PART NUMBER	DESCRIPTION
C1A			F.M. DETECTOR TRIMMER	R301	63-9218-1	12K OHM 5%
C1B			F.M. DETECTOR TRIMMER	R302	63-9218-1	12K OHM 5%
C1C			F.M. DETECTOR TRIMMER	R303	63-9218-1	12K OHM 5%
C1D	27-2-34		F.M. DETECTOR TRIMMER	R304	63-9218-1	12K OHM 5%
C1E			F.M. DETECTOR TRIMMER	R305	63-9218-1	12K OHM 5%
C1F			F.M. DETECTOR TRIMMER	R306	63-9218-1	12K OHM 5%
C1G			F.M. DETECTOR TRIMMER	R307	63-9218-1	12K OHM 5%
C1H			F.M. DETECTOR TRIMMER	R308	63-9218-1	12K OHM 5%
C1I			F.M. DETECTOR TRIMMER	R309	63-9218-1	12K OHM 5%
C1J			F.M. DETECTOR TRIMMER	R310	63-9218-1	12K OHM 5%
C1K			F.M. DETECTOR TRIMMER	R311	63-9218-1	12K OHM 5%
C1L			F.M. DETECTOR TRIMMER	R312	63-9218-1	12K OHM 5%
C1M			F.M. DETECTOR TRIMMER	R313	63-9218-1	12K OHM 5%
C1N			F.M. DETECTOR TRIMMER	R314	63-9218-1	12K OHM 5%
C1O			F.M. DETECTOR TRIMMER	R315	63-9218-1	12K OHM 5%
C1P			F.M. DETECTOR TRIMMER	R316	63-9218-1	12K OHM 5%
C1Q			F.M. DETECTOR TRIMMER	R317	63-9218-1	12K OHM 5%
C1R			F.M. DETECTOR TRIMMER	R318	63-9218-1	12K OHM 5%
C1S			F.M. DETECTOR TRIMMER	R319	63-9218-1	12K OHM 5%
C1T			F.M. DETECTOR TRIMMER	R320	63-9218-1	12K OHM 5%
C1U			F.M. DETECTOR TRIMMER	R321	63-9218-1	12K OHM 5%
C1V			F.M. DETECTOR TRIMMER	R322	63-9218-1	12K OHM 5%
C1W			F.M. DETECTOR TRIMMER	R323	63-9218-1	12K OHM 5%
C1X			F.M. DETECTOR TRIMMER	R324	63-9218-1	12K OHM 5%
C1Y			F.M. DETECTOR TRIMMER	R325	63-9218-1	12K OHM 5%
C1Z			F.M. DETECTOR TRIMMER	R326	63-9218-1	12K OHM 5%
C2A			F.M. DETECTOR TRIMMER	R327	63-9218-1	12K OHM 5%
C2B			F.M. DETECTOR TRIMMER	R328	63-9218-1	12K OHM 5%
C2C			F.M. DETECTOR TRIMMER	R329	63-9218-1	12K OHM 5%
C2D			F.M. DETECTOR TRIMMER	R330	63-9218-1	12K OHM 5%
C2E			F.M. DETECTOR TRIMMER	R331	63-9218-1	12K OHM 5%
C2F			F.M. DETECTOR TRIMMER	R332	63-9218-1	12K OHM 5%
C2G			F.M. DETECTOR TRIMMER	R333	63-9218-1	12K OHM 5%
C2H			F.M. DETECTOR TRIMMER	R334	63-9218-1	12K OHM 5%
C2I			F.M. DETECTOR TRIMMER	R335	63-9218-1	12K OHM 5%
C2J			F.M. DETECTOR TRIMMER	R336	63-9218-1	12K OHM 5%
C2K			F.M. DETECTOR TRIMMER	R337	63-9218-1	12K OHM 5%
C2L			F.M. DETECTOR TRIMMER	R338	63-9218-1	12K OHM 5%
C2M			F.M. DETECTOR TRIMMER	R339	63-9218-1	12K OHM 5%
C2N			F.M. DETECTOR TRIMMER	R340	63-9218-1	12K OHM 5%
C2O			F.M. DETECTOR TRIMMER	R341	63-9218-1	12K OHM 5%
C2P			F.M. DETECTOR TRIMMER	R342	63-9218-1	12K OHM 5%
C2Q			F.M. DETECTOR TRIMMER	R343	63-9218-1	12K OHM 5%
C2R			F.M. DETECTOR TRIMMER	R344	63-9218-1	12K OHM 5%
C2S			F.M. DETECTOR TRIMMER	R345	63-9218-1	12K OHM 5%
C2T			F.M. DETECTOR TRIMMER	R346	63-9218-1	12K OHM 5%
C2U			F.M. DETECTOR TRIMMER	R347	63-9218-1	12K OHM 5%
C2V			F.M. DETECTOR TRIMMER	R348	63-9218-1	12K OHM 5%
C2W			F.M. DETECTOR TRIMMER	R349	63-9218-1	12K OHM 5%
C2X			F.M. DETECTOR TRIMMER	R350	63-9218-1	12K OHM 5%
C2Y			F.M. DETECTOR TRIMMER	R351	63-9218-1	12K OHM 5%
C2Z			F.M. DETECTOR TRIMMER	R352	63-9218-1	12K OHM 5%
C3A			F.M. DETECTOR TRIMMER	R353	63-9218-1	12K OHM 5%
C3B			F.M. DETECTOR TRIMMER	R354	63-9218-1	12K OHM 5%
C3C			F.M. DETECTOR TRIMMER	R355	63-9218-1	12K OHM 5%
C3D			F.M. DETECTOR TRIMMER	R356	63-9218-1	12K OHM 5%
C3E			F.M. DETECTOR TRIMMER	R357	63-9218-1	12K OHM 5%
C3F			F.M. DETECTOR TRIMMER	R358	63-9218-1	12K OHM 5%
C3G			F.M. DETECTOR TRIMMER	R359	63-9218-1	12K OHM 5%
C3H			F.M. DETECTOR TRIMMER	R360	63-9218-1	12K OHM 5%





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THIS CIRCUIT DIAGRAM MAY OCCASIONALLY DIFFER FROM THE ACTUAL CIRCUIT. LATEST SAFETY AND PERFORMANCE IMPROVEMENT CHANGES INTO THE SET IS NOT DELAYED UNTIL THE NEW SERVICE LITERATURE IS PRINTED.

- TEST POINTS**
- A F.M. ANTENNA INPUT
 - D 1ST F.M. I.F. INPUT
 - G 3RD F.M. OUTPUT
 - H F.M. DETECTOR OUTPUT
 - H+ RATIO DETECTOR PRIMARY TUNING
 - L A.M. R.F. I.F. INPUT
 - M 19KHz A.C. GAIN
 - M1 19KHz D.C. GAIN

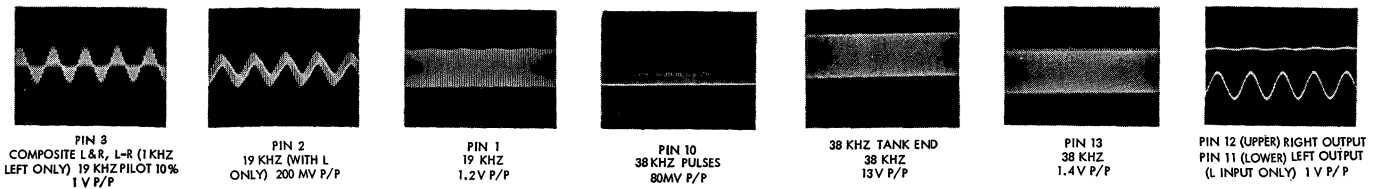


NOTES:
ALL VOLTAGES ARE D.C. UNLESS OTHERWISE SPECIFIED.
D.C. VOLTAGES SHOWN ARE MEASURED FROM CHASSIS, WITH NO SIGNAL INPUT, LOUDNESS CONTROL AT MINIMUM, LINE VOLTAGE 120V A.C. USING A HIGH IMPEDANCE V.T.V.M.
ALL RESISTORS IN OHMS, 1/2 WATT CARBON, ±10% UNLESS OTHERWISE SPECIFIED.
ALL CAPACITORS ARE IN MICROFARADS ±10% UNLESS OTHERWISE SPECIFIED.
I.F. FREQUENCY: A.M. 455KHz, F.M. 90.7MHz
TUNING RANGE: A.M. 540-1600KHz, F.M. 88-108MHz
⊥ INDICATES CHASSIS GROUND
P INDICATES ±20% TOLERANCE
⊕ INDICATES VOLTAGE
● INDICATES TEST POINTS
ARROWS ON CONTROLS INDICATE CLOCKWISE ROTATION.
121-976 IS INSULATED FROM CHASSIS. OUTPUT TRANSISTORS IN EACH CHANNEL SHALL BE A PAIR 121-976 B 121-977.
* VOLTAGES MEASURED IN THE F.M. STEREO POSITION.
** RIPPLE VOLTAGE MEASURED WITH NO SIGNAL INPUT.

I.C.-301 TOP VIEW

PIN	MONAURAL	STEREO	STEREO P-P
1	12.1	12.1	1.0
2	2.6	2.6	0.2
3	3.9	3.9	1.2
4	—	—	—
5	—	—	—
6	20.0	0.7	—
7	0	0	—
8	—	—	—
9	12.5	12.5	—
10	9.8	9.8	0.4
11	7.3	7.2	1.5
12	7.3	7.2	1.5
13	4.8	9.8	0.5
14	0.5	1.7	0.3

IC 301 WAVE FORMS



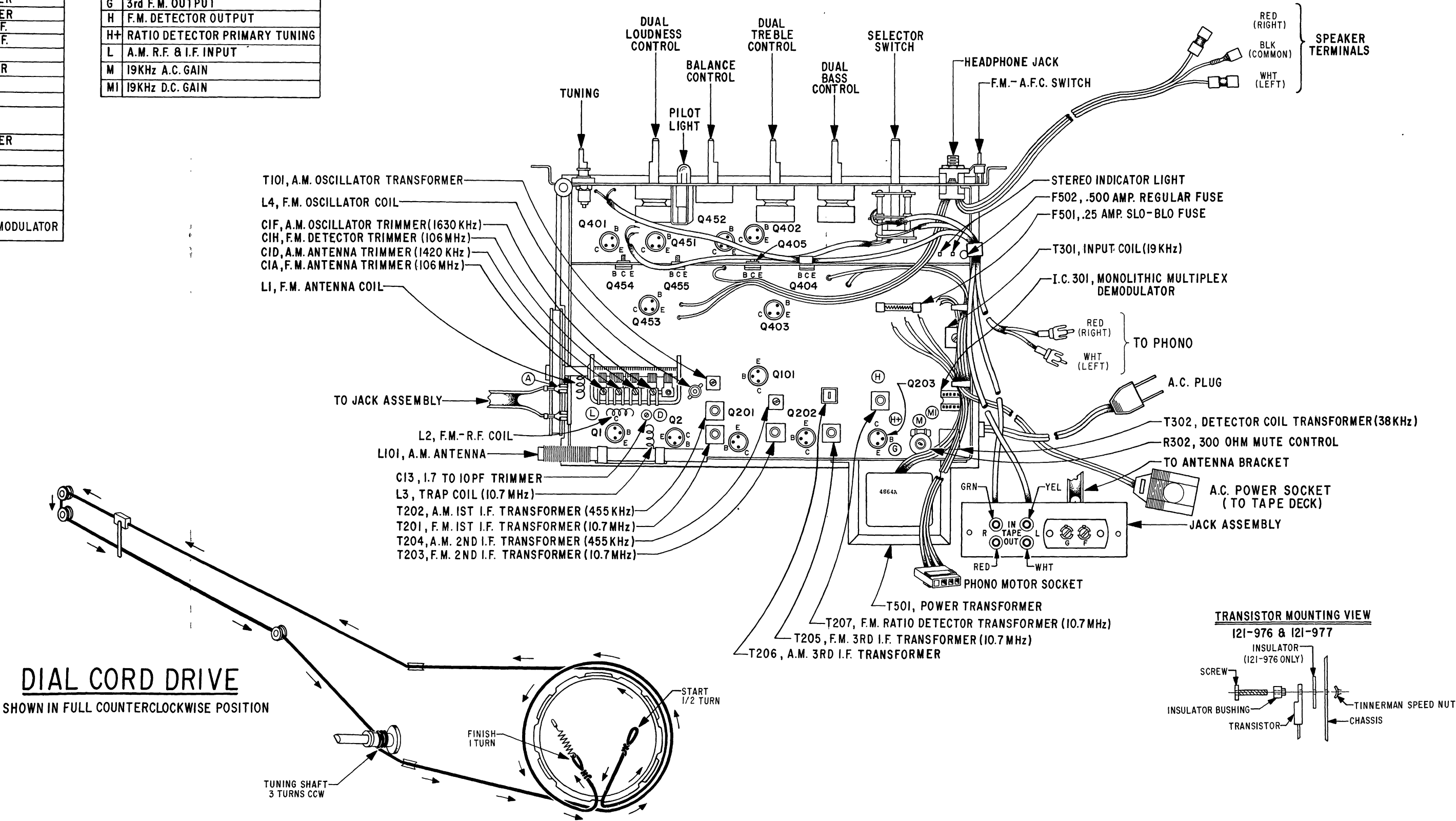
CHASSIS 5WFR50 — SCHEMATIC

ITEM NO.	PART NUMBER	DESCRIPTION	ITEM NO.	PART NUMBER	DESCRIPTION
C1A		FM DETECTOR TUNING	R213		880 OHM
C1B		FM DETECTOR TUNING	R214	63-1778	880 OHM
C1C		FM OSCILLATOR TRIMMER	R215	63-1813	470 OHM
C1D		AM ANTENNA TRIMMER	R216	63-1813	470 OHM
C1E		AM ANTENNA TUNING	R217	63-1779	2.2K OHM
C1F		AM OSCILLATOR TUNING	R218	63-1869	100K OHM
C1G		AM OSCILLATOR TRIMMER	R219	63-1941	100K OHM
C1H		FM ANTENNA TRIMMER	R220	63-1824	8500 OHM
C1J		FM ANTENNA TUNING	R221	63-1824	10K OHM
C21	22-2481	8 PF DISC ± .5% 500V	R224	63-1898	470 OHM 20%
C22	22-2729	.001 MFD DISC 25V	R225	63-1779	2.2K OHM
C23	22-2730	.01 MFD DISC .5% 500V	R301	63-1831	12K OHM
C24	22-3675	10 PF DISC ± .5% 500V	R302	63-8328	300 OHM MUTE CONTROL
C25	22-3360	.01 MFD DISC 25V	R303	63-1813	1.5 MEG OHM
C26	22-3841	3.3 PF GIMMICK ± .5% 500V	R304	63-1786	3.3K OHM
C27	20-3121	20 PF DISC ± .5% 500V	R305	63-1767	220 OHM
C28	22-3782	3.3 PF DISC ± .25 PF 50V	R306	63-1815	1.8K OHM 5%
C29	20-3120	.001 MFD DISC 25V	R307	63-1818	6.8K OHM 5%
C30	22-5878	5.5 PF DISC 1.05 PF 25V	R308	63-1869	100K OHM
C31	22-3034	20 MFD DISC 25V	R309	63-1909	100K OHM
C32	22-4856	1.7 TO 10 PF CERAMIC TRIMMER	R401	63-1959	8.2 MEG OHM
C33	22-3782	2 MFD DISC 25V	R403	63-1876	150K OHM
C34	22-4856	1.7 TO 10 PF CERAMIC TRIMMER	R405	63-1845	27K OHM
C35	22-3782	2 MFD DISC 25V	R406	63-1848	33K OHM
C36	22-4856	1.7 TO 10 PF CERAMIC TRIMMER	R407	63-1845	3.3K OHM
C37	22-3782	2 MFD DISC 25V	R408	63-1845	3.3K OHM
C38	22-3782	2 MFD DISC 25V	R409	63-1845	3.3K OHM
C39	22-3782	2 MFD DISC 25V	R410	63-1845	3.3K OHM
C40	22-3782	2 MFD DISC 25V	R411	63-1845	3.3K OHM
C41	22-3782	2 MFD DISC 25V	R412	63-1845	3.3K OHM
C42	22-3782	2 MFD DISC 25V	R413	63-1845	3.3K OHM
C43	22-3782	2 MFD DISC 25V	R414	63-1845	3.3K OHM
C44	22-3782	2 MFD DISC 25V	R415	63-1845	3.3K OHM
C45	22-3782	2 MFD DISC 25V	R416	63-1845	3.3K OHM
C46	22-3782	2 MFD DISC 25V	R417	63-1845	3.3K OHM
C47	22-3782	2 MFD DISC 25V	R418	63-1845	3.3K OHM
C48	22-3782	2 MFD DISC 25V	R419	63-1845	3.3K OHM
C49	22-3782	2 MFD DISC 25V	R420	63-1845	3.3K OHM
C50	22-3782	2 MFD DISC 25V	R421	63-1845	3.3K OHM
C51	22-3782	2 MFD DISC 25V	R422	63-1845	3.3K OHM
C52	22-3782	2 MFD DISC 25V	R423	63-1845	3.3K OHM
C53	22-3782	2 MFD DISC 25V	R424	63-1845	3.3K OHM
C54	22-3782	2 MFD DISC 25V	R425	63-1845	3.3K OHM
C55	22-3782	2 MFD DISC 25V	R426	63-1845	3.3K OHM
C56	22-3782	2 MFD DISC 25V	R427	63-1845	3.3K OHM
C57	22-3782	2 MFD DISC 25V	R428	63-1845	3.3K OHM
C58	22-3782	2 MFD DISC 25V	R429	63-1845	3.3K OHM
C59	22-3782	2 MFD DISC 25V	R430	63-1757	220 OHM
C60	22-3782	2 MFD DISC 25V	R431	63-1959	8.2 MEG OHM
C61	22-3782	2 MFD DISC 25V	R432	63-1876	150K OHM
C62	22-3782	2 MFD DISC 25V	R433	63-1845	27K OHM
C63	22-3782	2 MFD DISC 25V	R434	63-1848	33K OHM
C64	22-3782	2 MFD DISC 25V	R435	63-1845	3.3K OHM
C65	22-3782	2 MFD DISC 25V	R436	63-1845	3.3K OHM
C66	22-3782	2 MFD DISC 25V	R437	63-1845	3.3K OHM
C67	22-3782	2 MFD DISC 25V	R438	63-1845	3.3K OHM
C68	22-3782	2 MFD DISC 25V	R439	63-1845	3.3K OHM
C69	22-3782	2 MFD DISC 25V	R440	63-1845	3.3K OHM
C70	22				



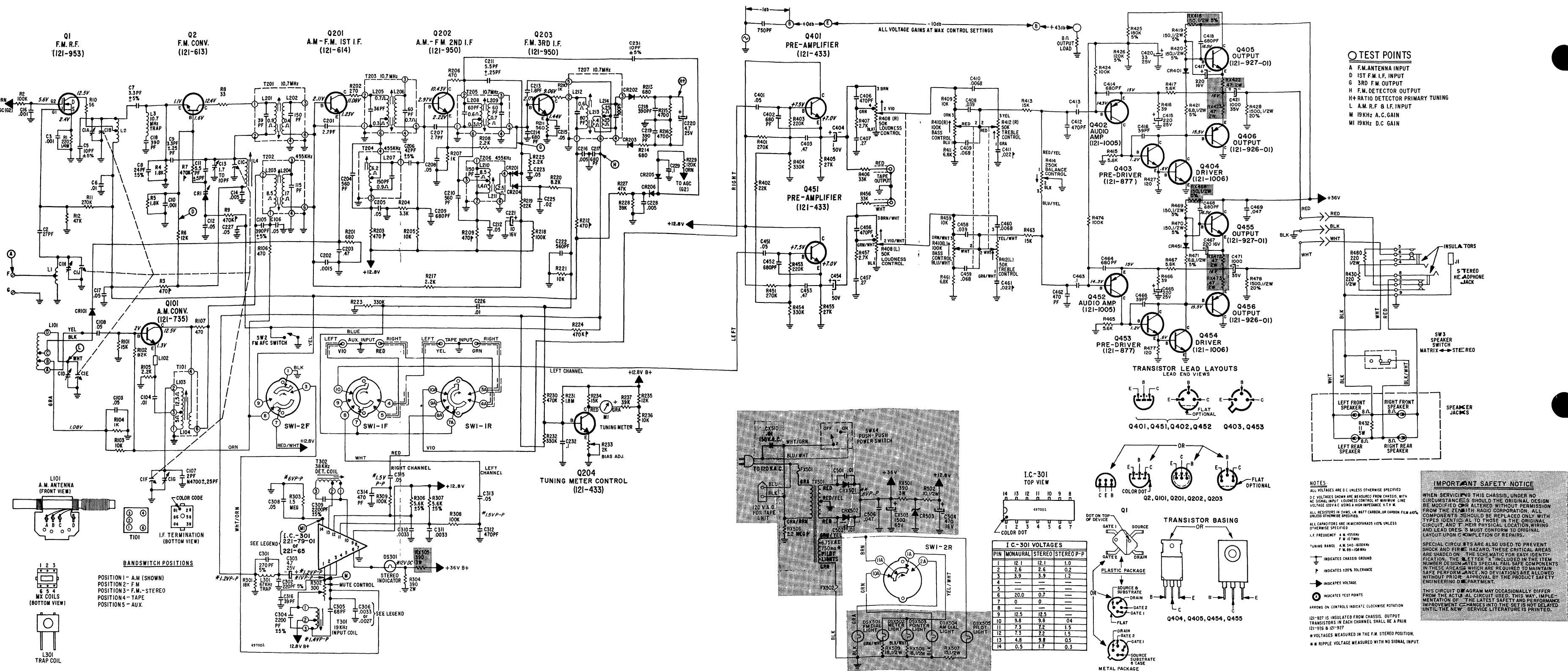
TRANSISTORS		
No.	PART No.	DESCRIPTION
Q1	I21-612	F.M.-R.F.
Q2	I21-613	F.M. CONVERTER
Q101	I21-735	A.M. CONVERTER
Q201	I21-614	A.M.-F.M. 1st I.F.
Q202	I21-950	A.M.-F.M. 2nd I.F.
Q203		F.M. 3rd I.F.
Q401	I21-433	PRE-AMPLIFIER
Q402		PRE-DRIVER
Q403	I21-768	DRIVER
Q404	I21-976	OUTPUT
Q405	I21-977	
Q451	I21-433	PRE-AMPLIFIER
Q452		PRE-DRIVER
Q453	I21-768	DRIVER
Q454	I21-976	OUTPUT
Q455	I21-977	
IC301	221-65	MULTIPLEX DEMODULATOR
	221-79	

TEST POINTS	
A	F.M. ANTENNA INPUT
D	1st F.M. I.F. INPUT
G	3rd F.M. OUTPUT
H	F.M. DETECTOR OUTPUT
H+	RATIO DETECTOR PRIMARY TUNING
L	A.M. R.F. & I.F. INPUT
M	19KHz A.C. GAIN
M1	19KHz D.C. GAIN

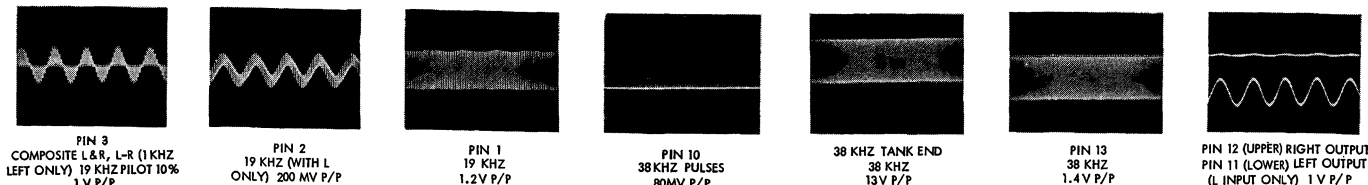


ITEM NO.	PART NUMBER	DESCRIPTION	ITEM NO.	PART NUMBER	DESCRIPTION
C1A	226-1387	FM DETECTOR TRIMMER	R229	83-9822-32	120K OHMS 5% (ALT. 63-7873 1/2W 10%)
C1B	226-1387	FM DETECTOR TRIMMER	R230	83-9822-33	470 OHM 1/2W
C1C	226-1387	FM OSCILLATOR TUNING	R231	90-9240-50	1.8 MEG OHM 1/2W
C1D	226-1387	FM ANTENNA TUNING	R232	83-9822-32	330K OHM 1/2W
C1E	226-1387	FM ANTENNA TUNING	R233	83-9822-33	ALT. 63-7860 1/2W 10%)
C1F	226-1387	FM ANTENNA TUNING	R234	83-9822-34	20K OHM METER CONTROL
C1G	226-1387	FM ANTENNA TUNING	R235	83-9822-35	15K OHM 1/2W (ALT. 63-7861 1/2W 10%)
C1H	226-1387	FM ANTENNA TUNING	R236	83-9822-36	120K OHM 5% (ALT. 63-7862 1/2W 10%)
C1I	226-1387	FM ANTENNA TUNING	R237	83-9822-37	10K OHM 5% (ALT. 63-7863 1/2W 10%)
C1J	226-1387	FM ANTENNA TUNING	R238	83-9822-38	39K OHM 5% (ALT. 63-7864 1/2W 10%)
C1K	226-1387	FM ANTENNA TUNING	R239	83-9822-39	15 OHM 5% (ALT. 63-7865 1/2W 10%)
C1L	226-1387	FM ANTENNA TUNING	R240	83-9822-40	8 1/2W 10%)
C1M	226-1387	FM ANTENNA TUNING	R241	83-9822-41	300 OHM MUTE CONTROL
C1N	226-1387	FM ANTENNA TUNING	R242	83-9822-42	15 OHM 5% (ALT. 63-7866 1/2W 10%)
C1O	226-1387	FM ANTENNA TUNING	R243	83-9822-43	330K OHM 5% (ALT. 63-7867 1/2W 10%)
C1P	226-1387	FM ANTENNA TUNING	R244	83-9822-44	27K OHM 5% (ALT. 63-7868 1/2W 10%)
C1Q	226-1387	FM ANTENNA TUNING	R245	83-9822-45	33K OHM 5% (ALT. 63-7869 1/2W 10%)
C1R	226-1387	FM ANTENNA TUNING	R246	83-9822-46	2.7K OHM 5% (ALT. 63-7870 1/2W 10%)
C1S	226-1387	FM ANTENNA TUNING	R247	83-9822-47	10K OHM 5% (ALT. 63-7871 1/2W 10%)
C1T	226-1387	FM ANTENNA TUNING	R248	83-9822-48	100K OHM 5% (ALT. 63-7872 1/2W 10%)
C1U	226-1387	FM ANTENNA TUNING	R249	83-9822-49	100K OHM 5% (ALT. 63-7873 1/2W 10%)
C1V	226-1387	FM ANTENNA TUNING	R250	83-9822-50	100K OHM 5% (ALT. 63-7874 1/2W 10%)
C1W	226-1387	FM ANTENNA TUNING	R251	83-9822-51	100K OHM 5% (ALT. 63-7875 1/2W 10%)
C1X	226-1387	FM ANTENNA TUNING	R252	83-9822-52	100K OHM 5% (ALT. 63-7876 1/2W 10%)
C1Y	226-1387	FM ANTENNA TUNING	R253	83-9822-53	100K OHM 5% (ALT. 63-7877 1/2W 10%)
C1Z	226-1387	FM ANTENNA TUNING	R254	83-9822-54	100K OHM 5% (ALT. 63-7878 1/2W 10%)
C201	226-3310	2.7P FM GIMMICK 1.50K 500V	R255	83-9822-55	100K OHM 5% (ALT. 63-7879 1/2W 10%)
C202	226-3310	2.7P FM GIMMICK 1.50K 500V	R256	83-9822-56	100K OHM 5% (ALT. 63-7880 1/2W 10%)
C203	226-3310	2.7P FM GIMMICK 1.50K 500V	R257	83-9822-57	100K OHM 5% (ALT. 63-7881 1/2W 10%)
C204	226-3310	2.7P FM GIMMICK 1.50K 500V	R258	83-9822-58	100K OHM 5% (ALT. 63-7882 1/2W 10%)
C205	226-3310	2.7P FM GIMMICK 1.50K 500V	R259	83-9822-59	100K OHM 5% (ALT. 63-7883 1/2W 10%)
C206	226-3310	2.7P FM GIMMICK 1.50K 500V	R260	83-9822-60	100K OHM 5% (ALT. 63-7884 1/2W 10%)
C207	226-3310	2.7P FM GIMMICK 1.50K 500V	R261	83-9822-61	100K OHM 5% (ALT. 63-7885 1/2W 10%)
C208	226-3310	2.7P FM GIMMICK 1.50K 500V	R262	83-9822-62	100K OHM 5% (ALT. 63-7886 1/2W 10%)
C209	226-3310	2.7P FM GIMMICK 1.50K 500V	R263	83-9822-63	100K OHM 5% (ALT. 63-7887 1/2W 10%)
C210	226-3310	2.7P FM GIMMICK 1.50K 500V	R264	83-9822-64	100K OHM 5% (ALT. 63-7888 1/2W 10%)
C211	226-3310	2.7P FM GIMMICK 1.50K 500V	R265	83-9822-65	100K OHM 5% (ALT. 63-7889 1/2W 10%)
C212	226-3310	2.7P FM GIMMICK 1.50K 500V	R266	83-9822-66	100K OHM 5% (ALT. 63-7890 1/2W 10%)
C213	226-3310	2.7P FM GIMMICK 1.50K 500V	R267	83-9822-67	100K OHM 5% (ALT. 63-7891 1/2W 10%)
C214	226-3310	2.7P FM GIMMICK 1.50K 500V	R268	83-9822-68	100K OHM 5% (ALT. 63-7892 1/2W 10%)
C215	226-3310	2.7P FM GIMMICK 1.50K 500V	R269	83-9822-69	100K OHM 5% (ALT. 63-7893 1/2W 10%)
C216	226-3310	2.7P FM GIMMICK 1.50K 500V	R270	83-98	



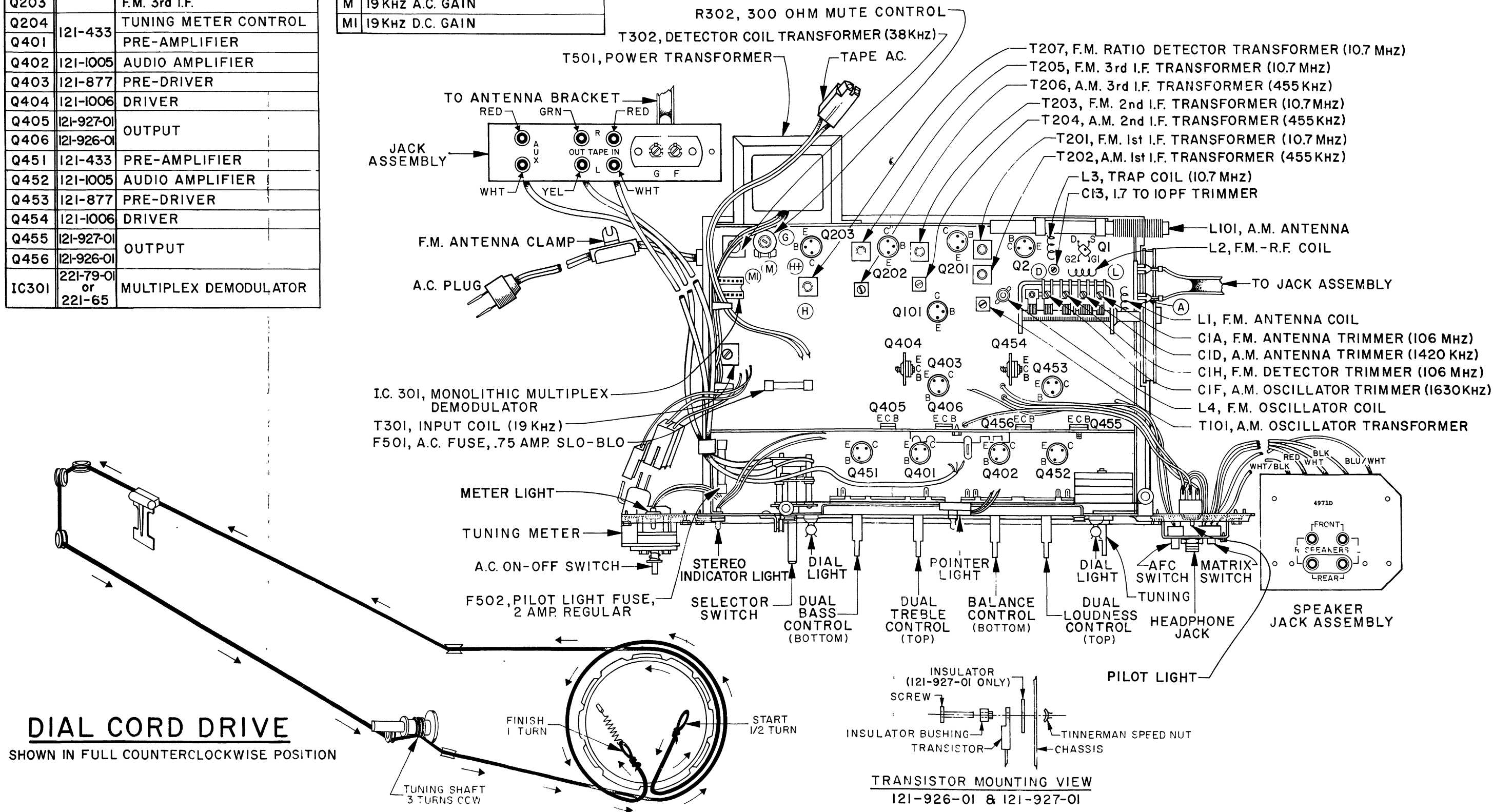


IC 301 WAVE FORMS



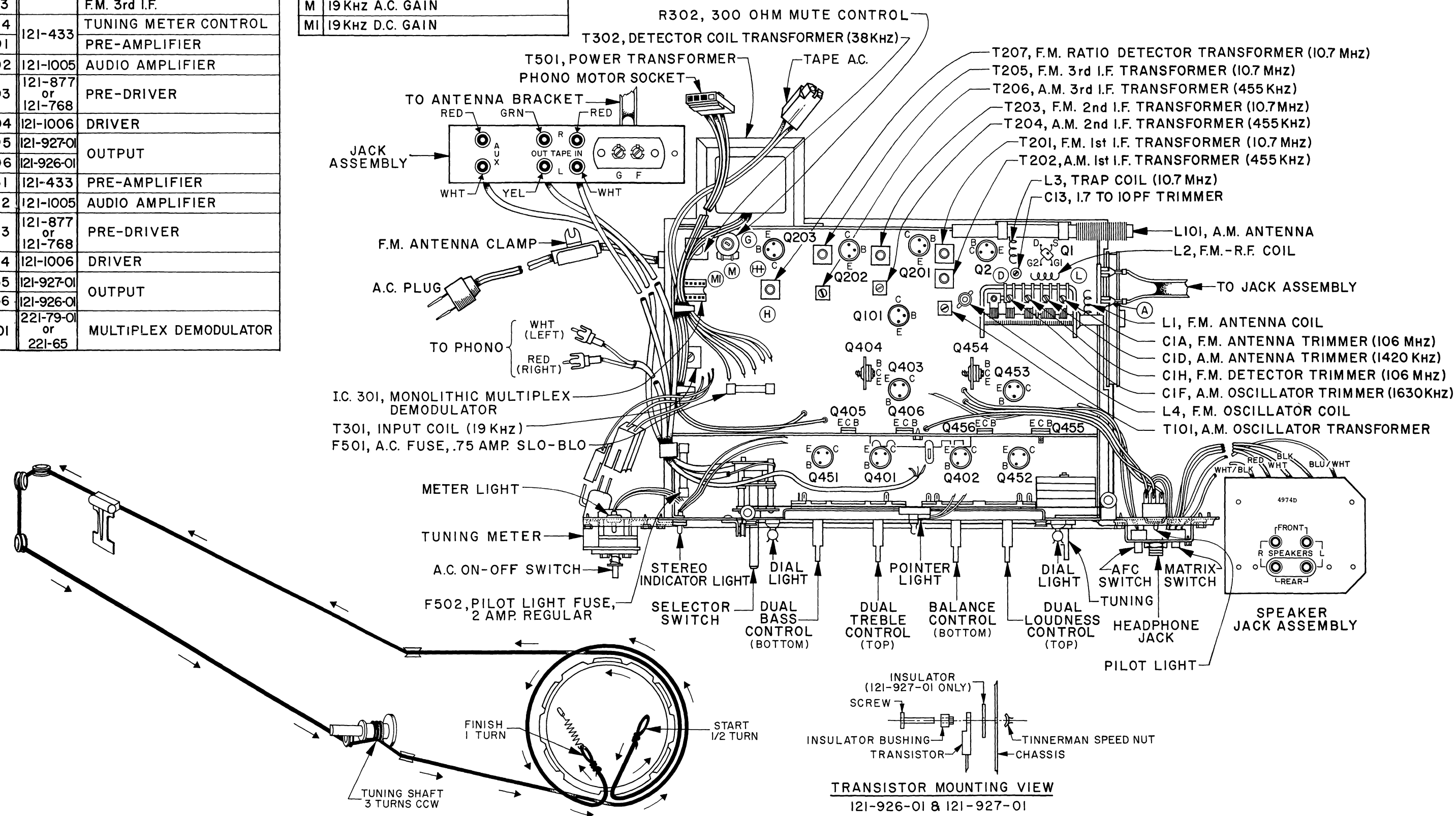
TRANSISTORS		
No.	PART No.	DESCRIPTION
Q1	121-953	F.M.-R.F.
Q2	121-613	F.M. CONVERTER
Q101	121-735	A.M. CONVERTER
Q201	121-614	A.M.-F.M. 1st I.F.
Q202	121-950	A.M.-F.M. 2nd I.F.
Q203		F.M. 3rd I.F.
Q204	121-433	TUNING METER CONTROL
Q401		PRE-AMPLIFIER
Q402	121-1005	AUDIO AMPLIFIER
Q403	121-877	PRE-DRIVER
Q404	121-1006	DRIVER
Q405	121-927-01	OUTPUT
Q406	121-926-01	
Q451	121-433	PRE-AMPLIFIER
Q452	121-1005	AUDIO AMPLIFIER
Q453	121-877	PRE-DRIVER
Q454	121-1006	DRIVER
Q455	121-927-01	OUTPUT
Q456	121-926-01	
IC301	221-79-01 or 221-65	MULTIPLEX DEMODULATOR

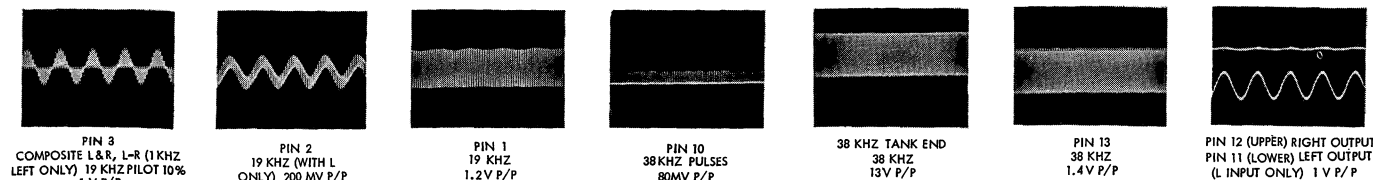
TEST POINTS	
A	F.M. ANTENNA INPUT
D	1st F.M. I.F. INPUT
G	3rd F.M. OUTPUT
H	F.M. DETECTOR OUTPUT
H+	RATIO DETECTOR PRIMARY TUNING
L	A.M. R.F. & I.F. INPUT
M	19 KHz A.C. GAIN
M1	19 KHz D.C. GAIN



TRANSISTORS		
No.	PART No.	DESCRIPTION
Q1	I2I-953	F.M.-R.F.
Q2	I2I-613	F.M. CONVERTER
Q101	I2I-735	A.M. CONVERTER
Q201	I2I-614	A.M.-F.M. 1st I.F.
Q202	I2I-950	A.M.-F.M. 2nd I.F.
Q203		F.M. 3rd I.F.
Q204	I2I-433	TUNING METER CONTROL
Q401		PRE-AMPLIFIER
Q402	I2I-1005	AUDIO AMPLIFIER
Q403	I2I-877 or I2I-768	PRE-DRIVER
Q404	I2I-1006	DRIVER
Q405	I2I-927-01	OUTPUT
Q406	I2I-926-01	OUTPUT
Q451	I2I-433	PRE-AMPLIFIER
Q452	I2I-1005	AUDIO AMPLIFIER
Q453	I2I-877 or I2I-768	PRE-DRIVER
Q454	I2I-1006	DRIVER
Q455	I2I-927-01	OUTPUT
Q456	I2I-926-01	OUTPUT
IC301	22I-79-01 or 22I-65	MULTIPLEX DEMODULATOR

TEST POINTS	
A	F.M. ANTENNA INPUT
D	1st F.M. I.F. INPUT
G	3rd F.M. OUTPUT
H	F.M. DETECTOR OUTPUT
H+	RATIO DETECTOR PRIMARY TUNING
L	A.M. R.F. & I.F. INPUT
M	19KHz A.C. GAIN
MI	19KHz D.C. GAIN

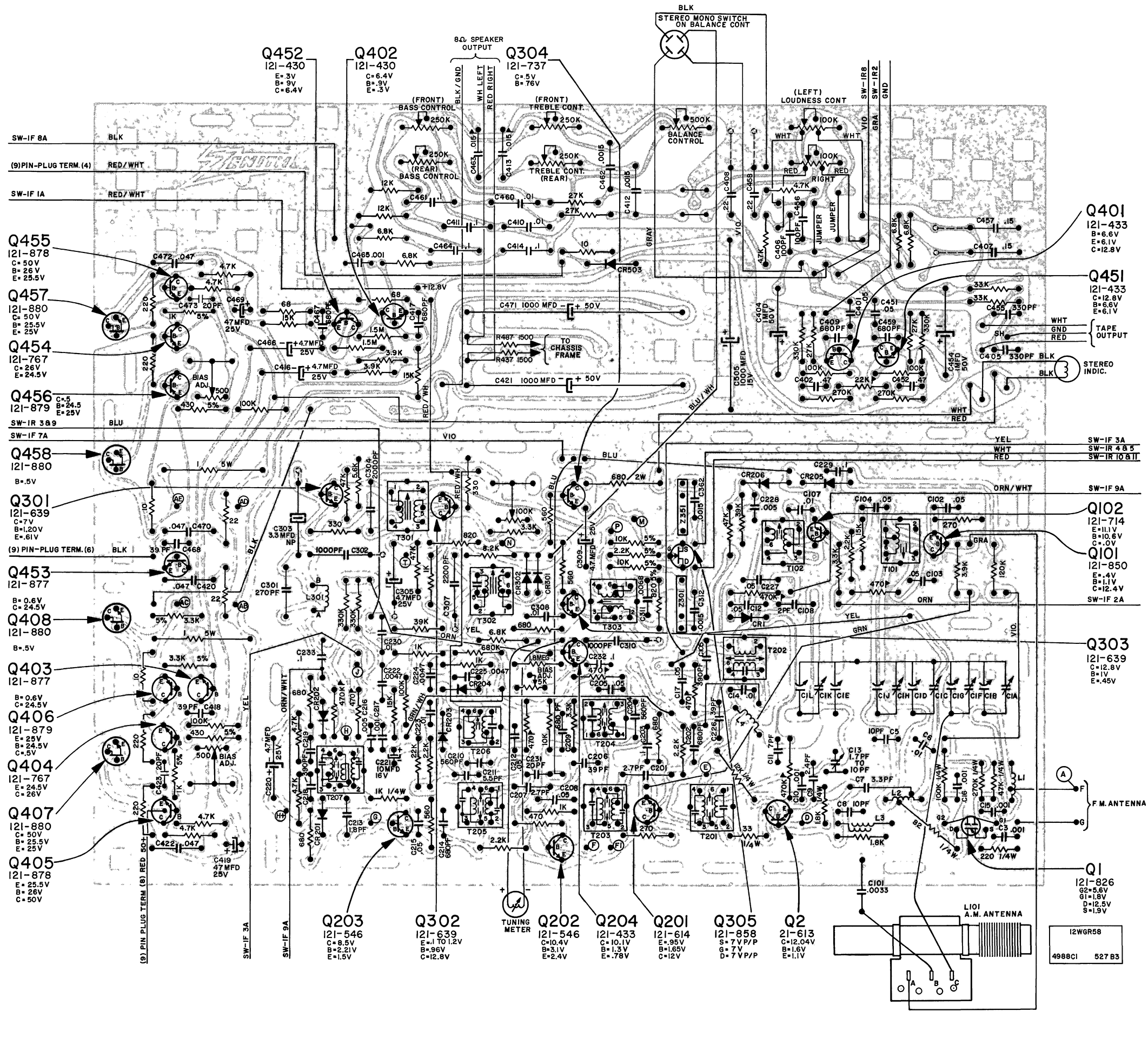




ITEM NO	PART NUMBER	DESCRIPTION	ITEM NO	PART NUMBER	DESCRIPTION
C1A	FM	OSCILLATOR DETECTOR	R230	83-1897	470K OHM 1/2W
C1B	FM	OSCILLATOR TUNING	R231	83-9024-50	1.5K OHM 5% (ALT. 63-7822 1/2W 100)
C1C	FM	OSCILLATOR TUNING	R232	83-9024-50	1.5K OHM 5% (ALT. 63-7822 1/2W 100)
C1D	FM	OSCILLATOR TUNING	R233	83-9024-50	20 OHM METER CONTROL
C1E	FM	OSCILLATOR TUNING	R234	83-9024-50	12K OHM 5% (ALT. 63-7824 1/2W 100)
C1F	FM	OSCILLATOR TUNING	R235	83-9024-50	12K OHM 5% (ALT. 63-7824 1/2W 100)
C1G	FM	OSCILLATOR TUNING	R236	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1H	FM	OSCILLATOR TUNING	R237	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1I	FM	OSCILLATOR TUNING	R238	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1J	FM	OSCILLATOR TUNING	R239	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1K	FM	OSCILLATOR TUNING	R240	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1L	FM	OSCILLATOR TUNING	R241	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1M	FM	OSCILLATOR TUNING	R242	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1N	FM	OSCILLATOR TUNING	R243	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1O	FM	OSCILLATOR TUNING	R244	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1P	FM	OSCILLATOR TUNING	R245	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1Q	FM	OSCILLATOR TUNING	R246	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1R	FM	OSCILLATOR TUNING	R247	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1S	FM	OSCILLATOR TUNING	R248	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1T	FM	OSCILLATOR TUNING	R249	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1U	FM	OSCILLATOR TUNING	R250	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1V	FM	OSCILLATOR TUNING	R251	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1W	FM	OSCILLATOR TUNING	R252	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1X	FM	OSCILLATOR TUNING	R253	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1Y	FM	OSCILLATOR TUNING	R254	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C1Z	FM	OSCILLATOR TUNING	R255	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C20	FM	OSCILLATOR TUNING	R256	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C21	FM	OSCILLATOR TUNING	R257	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C22	FM	OSCILLATOR TUNING	R258	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C23	FM	OSCILLATOR TUNING	R259	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C24	FM	OSCILLATOR TUNING	R260	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C25	FM	OSCILLATOR TUNING	R261	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C26	FM	OSCILLATOR TUNING	R262	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C27	FM	OSCILLATOR TUNING	R263	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C28	FM	OSCILLATOR TUNING	R264	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C29	FM	OSCILLATOR TUNING	R265	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C30	FM	OSCILLATOR TUNING	R266	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C31	FM	OSCILLATOR TUNING	R267	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C32	FM	OSCILLATOR TUNING	R268	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C33	FM	OSCILLATOR TUNING	R269	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C34	FM	OSCILLATOR TUNING	R270	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C35	FM	OSCILLATOR TUNING	R271	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C36	FM	OSCILLATOR TUNING	R272	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C37	FM	OSCILLATOR TUNING	R273	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C38	FM	OSCILLATOR TUNING	R274	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C39	FM	OSCILLATOR TUNING	R275	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C40	FM	OSCILLATOR TUNING	R276	83-9024-50	10K OHM 5% (ALT. 63-7822 1/2W 100)
C41	FM	OSCILLATOR TUNING	R277		

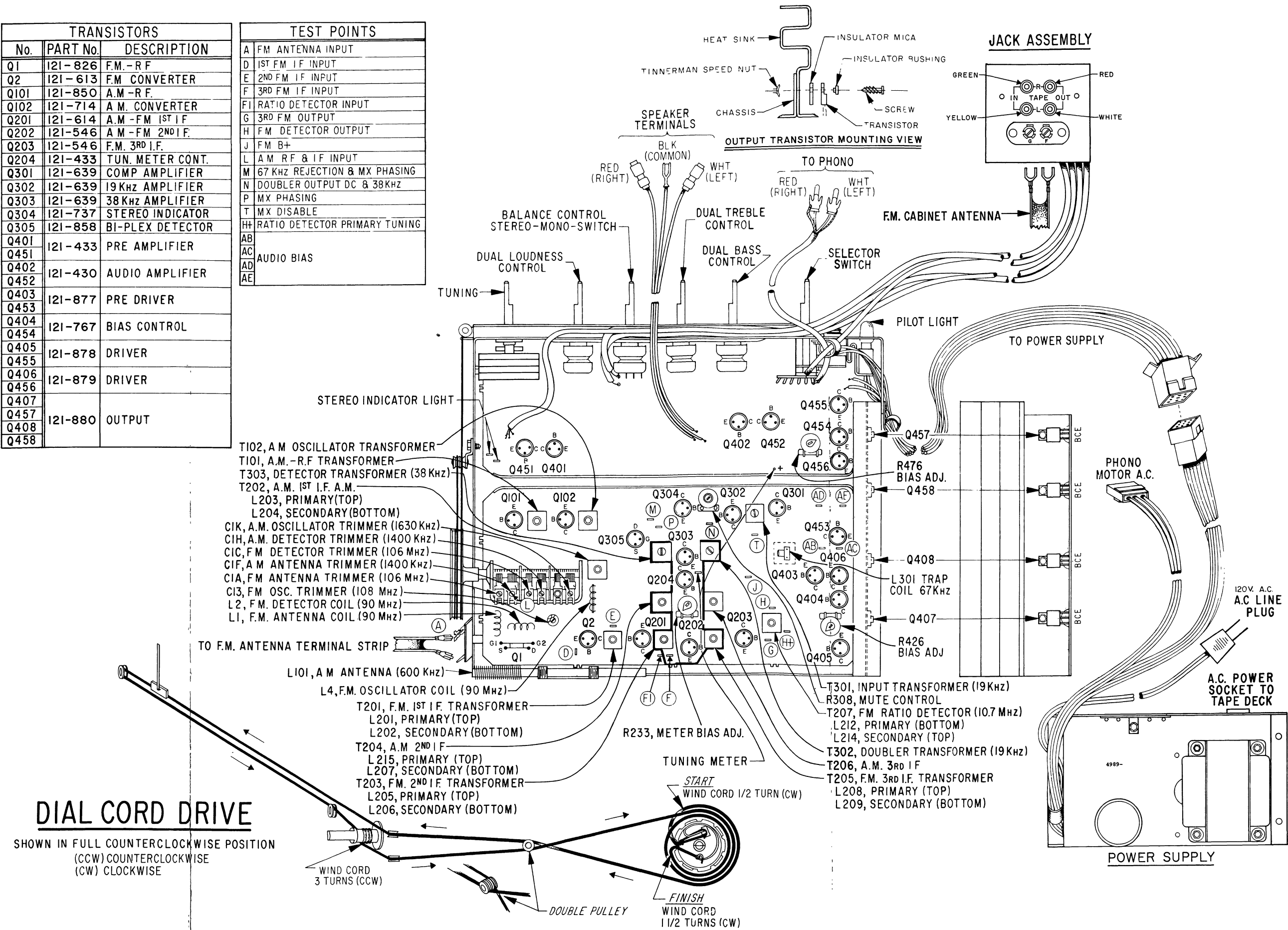


ITEM NO.	PART NUMBER	DESCRIPTION	ITEM NO.	PART NUMBER	DESCRIPTION
C1A	FM -ANT TRIMMER		R226	330K OHM 5% (ALT: 67-7850 10% 12W)	
F1A	FM -ANT TUNING		R227	10K OHM 5% (ALT: 67-7850 10% 12W)	
F1B	FM -ELECTOR TRIMMER		R233	330K OHM 5% (ALT: 67-7850 10% 12W)	
F1C	FM -ELECTOR TUNING		R234	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1E	AM -OSCILLATOR TRIMMER		R235	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
A1	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R236	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1F	AM -ANT TUNING		R237	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
A1	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R238	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1G	AM -OSCILLATOR TRIMMER		R239	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
A1	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R240	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1H	AM -ELECTOR TUNING		R241	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
F1D	AM -ELECTOR TUNING		R242	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1I	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R243	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1J	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R244	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1K	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R245	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1L	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R246	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1M	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R247	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1N	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R248	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1O	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R249	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1P	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R250	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1Q	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R251	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1R	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R252	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1S	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R253	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1T	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R254	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1U	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R255	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1V	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R256	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1W	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R257	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1X	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R258	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1Y	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R259	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C1Z	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R260	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C20	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R261	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C21	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R262	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C22	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R263	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C23	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R264	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C24	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R265	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C25	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R266	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C26	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R267	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C27	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R268	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C28	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R269	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C29	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R270	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C30	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R271	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C31	247562	10K OHM 5% (ALT: 67-7850 10% 12W)	R272	1.8K OHM 5% (ALT: 67-7850 10% 12W)	
C32	247562	10K OHM 5% (ALT: 6			



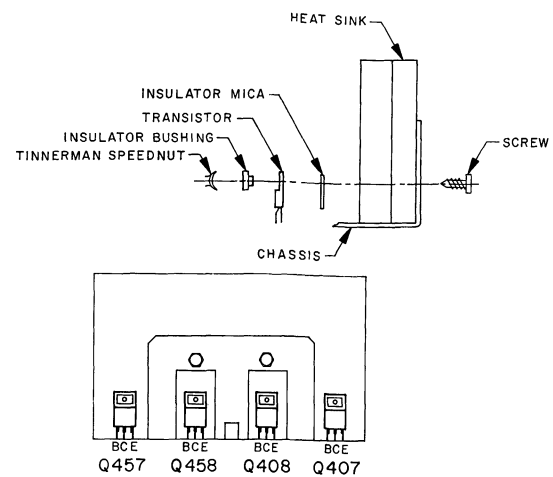
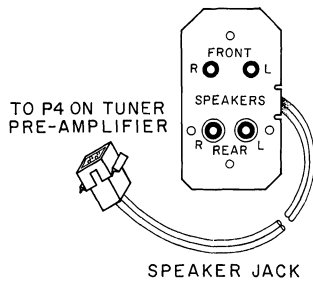
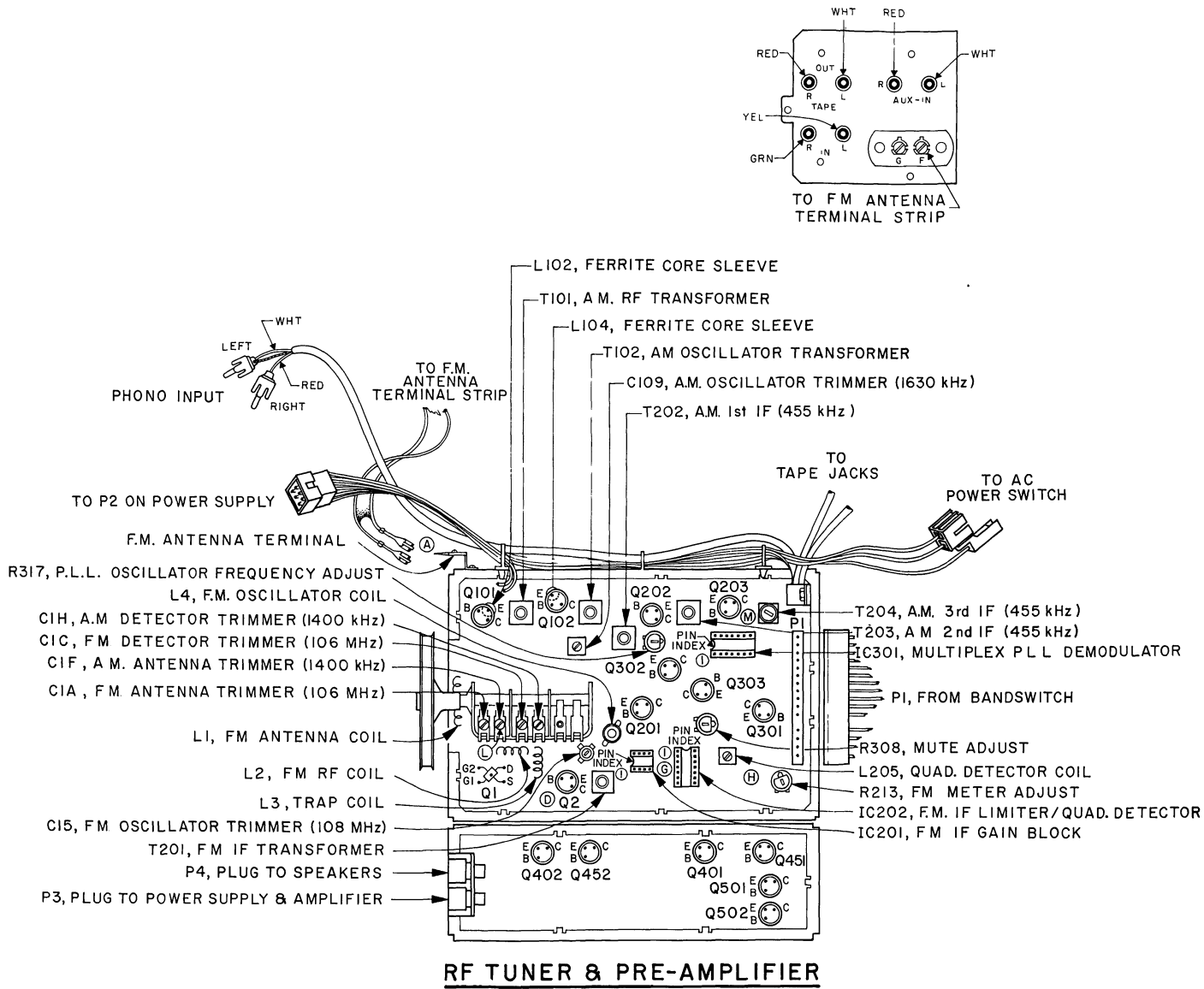
TRANSISTORS		
No.	PART No.	DESCRIPTION
Q1	121-826	F.M.-R.F.
Q2	121-613	F.M. CONVERTER
Q101	121-850	A.M.-R.F.
Q102	121-714	A.M. CONVERTER
Q201	121-614	A.M.-FM 1 ST I.F.
Q202	121-546	A.M.-FM 2 ND I.F.
Q203	121-546	F.M. 3 RD I.F.
Q204	121-433	TUN. METER CONT.
Q301	121-639	COMP. AMPLIFIER
Q302	121-639	19 KHz AMPLIFIER
Q303	121-639	38 KHz AMPLIFIER
Q304	121-737	STEREO INDICATOR
Q305	121-858	BI-PLEX DETECTOR
Q401	121-433	PRE AMPLIFIER
Q451		
Q402	121-430	AUDIO AMPLIFIER
Q452		
Q403	121-877	PRE DRIVER
Q453		
Q404	121-767	BIAS CONTROL
Q454		
Q405	121-878	DRIVER
Q455		
Q406	121-879	DRIVER
Q456		
Q407		
Q457	121-880	OUTPUT
Q408		
Q458		

TEST POINTS	
A	FM ANTENNA INPUT
D	1 ST FM I.F. INPUT
E	2 ND FM I.F. INPUT
F	3 RD FM I.F. INPUT
FI	RATIO DETECTOR INPUT
G	3 RD FM OUTPUT
H	FM DETECTOR OUTPUT
J	FM B+
L	A.M. RF & IF INPUT
M	67 KHz REJECTION & MX PHASING
N	DOUBLER OUTPUT DC & 38 KHz
P	MX PHASING
T	MX DISABLE
HH	RATIO DETECTOR PRIMARY TUNING
AB	
AC	AUDIO BIAS
AD	
AE	



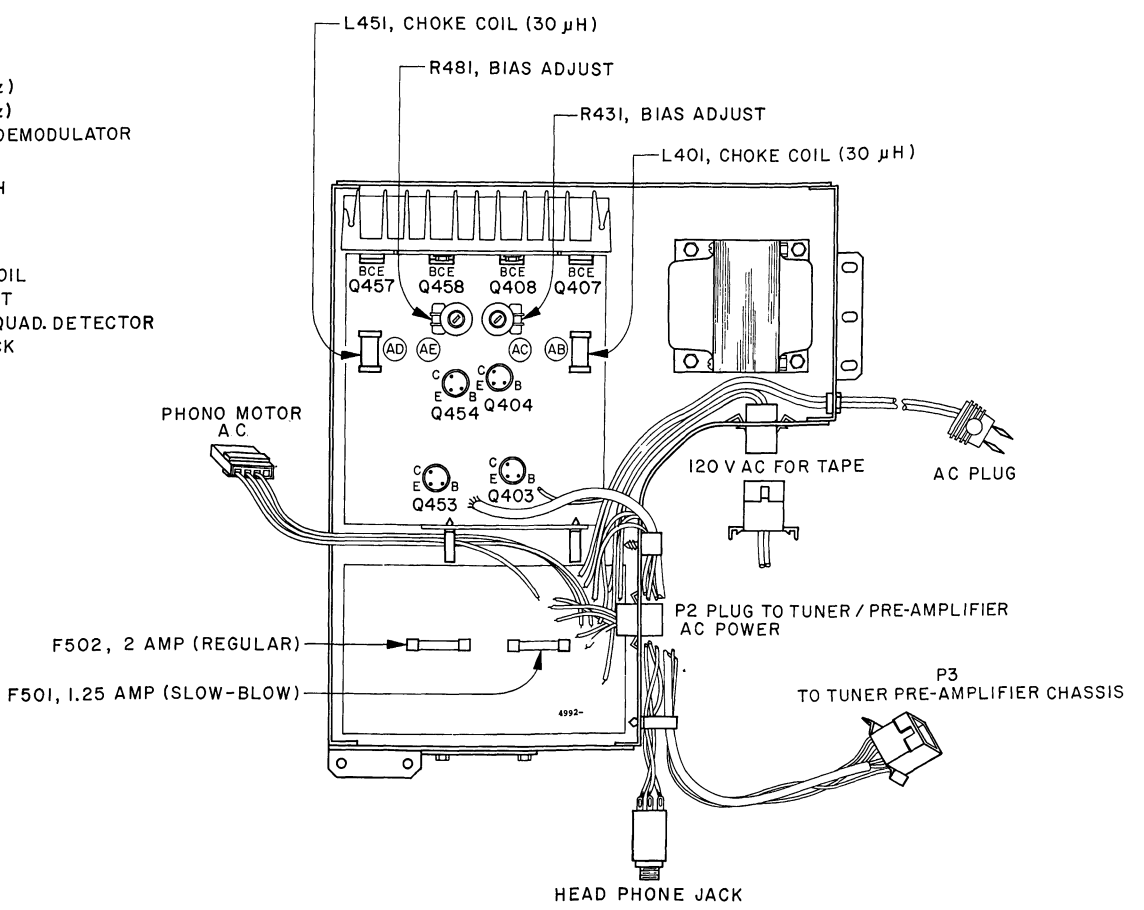
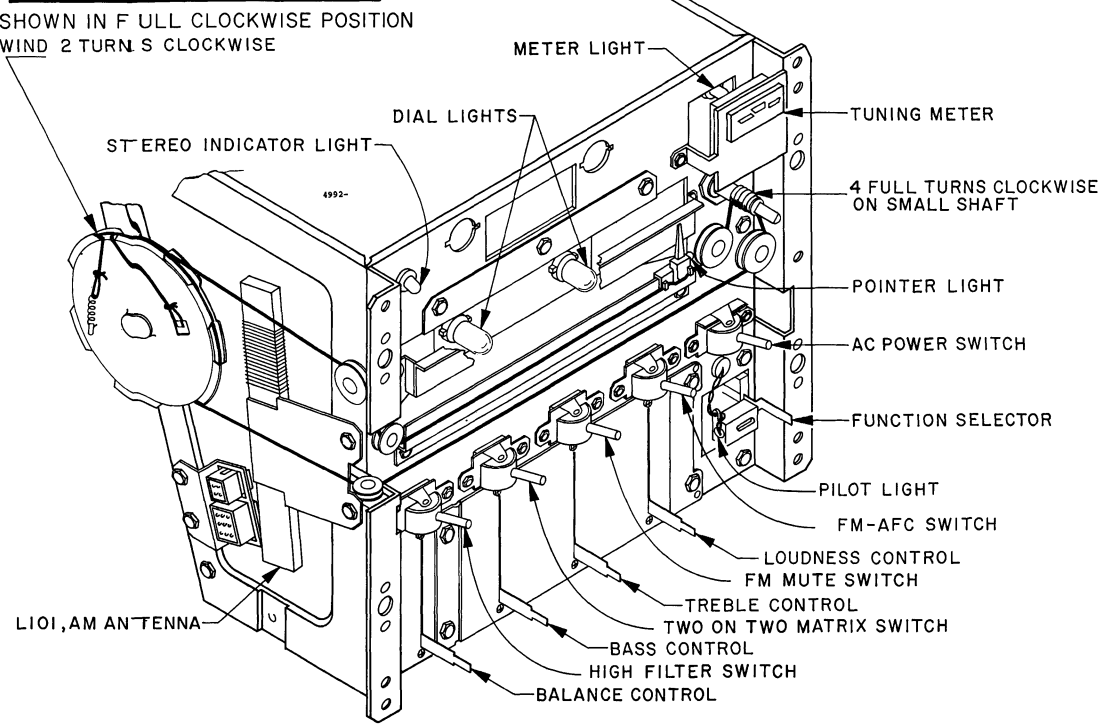
TRANSISTORS		
No	PART No	DESCRIPTION
Q1	121 - 953	FM-RF
Q2	121 - 613	FM CONVERTER
Q101	121 - 850	AM-RF
Q102	121 - 735	AM CONVERTER
Q201		AGC AMPLIFIER
Q202	121 - 950	AM 1st IF
Q203		AM 2nd IF
Q301	121 - 603	MUTE BUFFER
Q302		MUTE AMPLIFIER
Q303	121 - 950	MUTE SWITCH
Q401		PRE-AMPLIFIER
Q402	121 - 433	AUDIO AMPLIFIER
Q403	121 - 1005	PRE-DRIVER
Q404	121 - 877	DRIVER
Q407	121 - 1013	OUTPUT
Q408	121 - 1012	
Q451		PRE-AMPLIFIER
Q452	121 - 433	AUDIO AMPLIFIER
Q453	121 - 1005	PRE-DRIVER
Q454	121 - 877	DRIVER
Q457	121 - 1013	OUTPUT
Q458	121 - 1012	
Q501	121 - 774	FM POWER SWITCH
Q502	121 - 768	
IC201	221 - 89	FM IF GAIN BLOCK
IC202	221 - 90	FM IF LIMITER/QUAD. DETECTOR
IC301	221 - 91	MULTIPLEX PLL DEMODULATOR

TEST POINTS	
A	FM ANTENNA INPUT
D	FM IF INPUT
G	FM IF OUTPUT
H	FM DETECTOR OUTPUT
L	AM RF INPUT
M	19 kHz OSCILLATOR OUTPUT
AB	AUDIO BIAS
AC	
AD	
AE	



TRANSISTOR MOUNTING VIEW

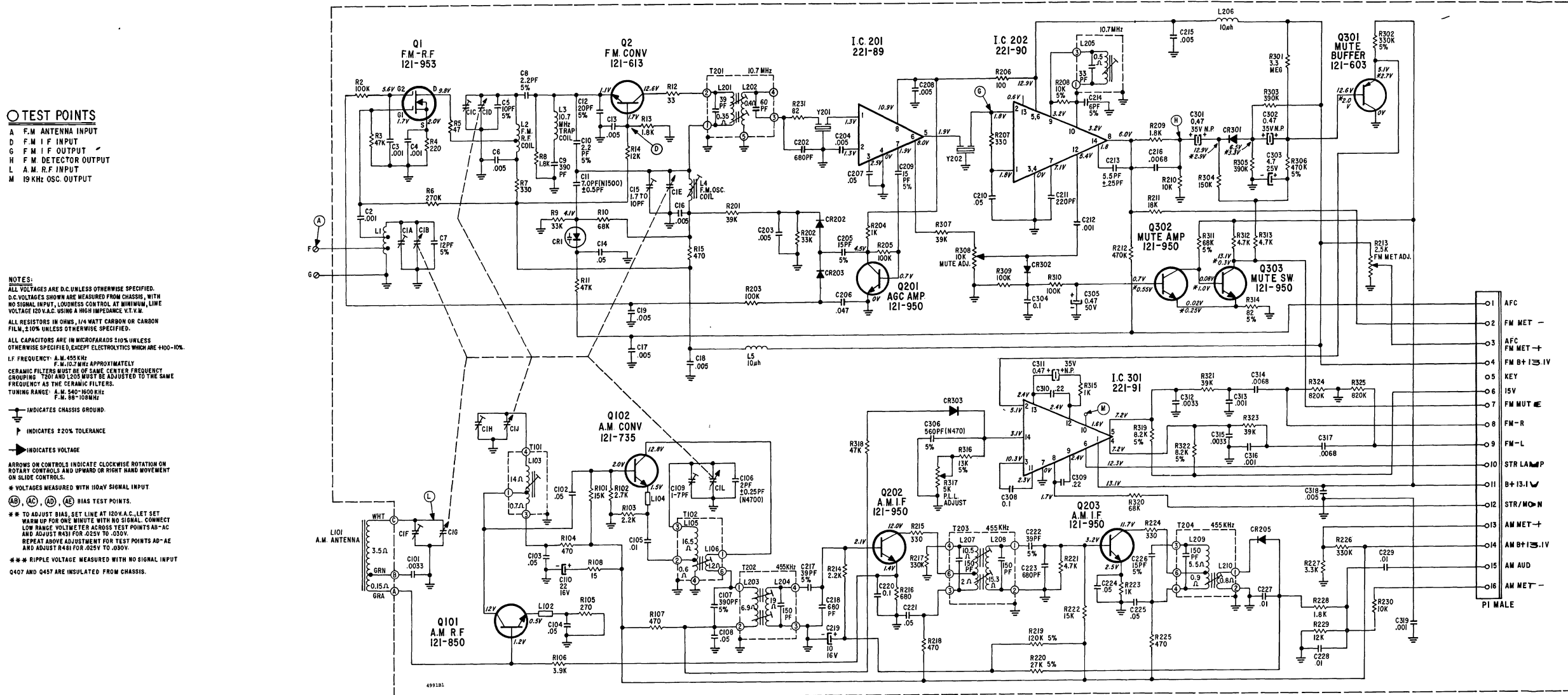
DIAL CORD DRIVE



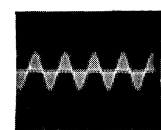
AUDIO AMPLIFIER & POWER SUPPLY

CHASSIS LEGEND 12WGR59

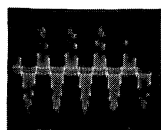
ITEM NO.	PART NUMBER	DESCRIPTION	ITEM NO.	PART NUMBER	DESCRIPTION	ITEM NO.	PART NUMBER	DESCRIPTION
C1A		FM ANTENNA TUNING	R102	93-921-82	2.7K OHM .5% 1/4W ALT - 63-10183	R451	93-922-20	20K OHM .5% 1/4W ALT - 63-7882
C1B		FM ANTENNA TUNING	R103	93-921-83	2.2K OHM .5% 1/4W ALT - 63-10182	R452	93-922-28	27K OHM .5% 1/4W ALT - 63-7883
C1C		FM TRIMMER	R104	93-921-84	2.2K OHM .5% 1/4W ALT - 63-10183	R453	93-922-36	33K OHM .5% 1/4W ALT - 63-7884
C1D		FM OSCILLATOR TUNING	R105	93-921-85	270 OHM .5% 1/4W ALT - 63-10183	R454	93-922-44	39K OHM .5% 1/4W ALT - 63-7885
C1E	22-6245-01	AM ANTENNA TUNING	R106	93-921-86	3.0K OHM .5% 1/4W ALT - 63-10183	R455	93-922-52	47K OHM .5% 1/4W ALT - 63-7886
C1F		AM TRIMMER	R107	93-921-87	3.0K OHM .5% 1/4W ALT - 63-10183	R456	93-922-60	56K OHM .5% 1/4W ALT - 63-7887
C1G		AM OSCILLATOR TUNING	R108	93-921-88	47K OHM .5% 1/4W ALT - 63-10183	R457	93-922-68	68K OHM .5% 1/4W ALT - 63-7888
C1H	22-3729	.001 MFD DISC 50V	R109	93-921-89	10K OHM .5% 1/4W ALT - 63-10183	R458	93-922-76	82K OHM .5% 1/4W ALT - 63-7889
C1I	22-3729	.001 MFD DISC 50V	R110	93-921-90	15 OHM .5% 1/4W ALT - 63-10183	R459	93-922-84	100K OHM .5% 1/4W ALT - 63-7890
C1J	22-3729	.001 MFD DISC 50V	R111	93-921-91	20 OHM .5% 1/4W ALT - 63-10183	R460	93-922-92	120K OHM .5% 1/4W ALT - 63-7891
C1K	22-3729	.001 MFD DISC 50V	R112	93-921-92	33K OHM .5% 1/4W ALT - 63-10183	R461	93-922-100	150K OHM .5% 1/4W ALT - 63-7892
C1L	22-3729	.001 MFD DISC 50V	R113	93-921-93	47K OHM .5% 1/4W ALT - 63-10183	R462	93-922-108	180K OHM .5% 1/4W ALT - 63-7893
C1M	22-3729	.001 MFD DISC 50V	R114	93-921-94	68K OHM .5% 1/4W ALT - 63-10183	R463	93-922-116	220K OHM .5% 1/4W ALT - 63-7894
C1N	22-3729	.001 MFD DISC 50V	R115	93-921-95	100K OHM .5% 1/4W ALT - 63-10183	R464	93-922-124	270K OHM .5% 1/4W ALT - 63-7895
C1O	22-3729	.001 MFD DISC 50V	R116	93-921-96	220K OHM .5% 1/4W ALT - 63-10183	R465	93-922-132	330K OHM .5% 1/4W ALT - 63-7896
C1P	22-3729	.001 MFD DISC 50V	R117	93-921-97	330K OHM .5% 1/4W ALT - 63-10183	R466	93-922-140	470K OHM .5% 1/4W ALT - 63-7897
C1Q	22-3729	.001 MFD DISC 50V	R118	93-921-98	470K OHM .5% 1/4W ALT - 63-10183	R467	93-922-148	680K OHM .5% 1/4W ALT - 63-7898
C1R	22-3729	.001 MFD DISC 50V	R119	93-921-99	680K OHM .5% 1/4W ALT - 63-10183	R468	93-922-156	1M OHM .5% 1/4W ALT - 63-7899
C1S	22-3729	.001 MFD DISC 50V	R120	93-921-100	1M OHM .5% 1/4W ALT - 63-10183	R469	93-922-164	1.5M OHM .5% 1/4W ALT - 63-7900
C1T	22-3729	.001 MFD DISC 50V	R121	93-921-101	2.2K OHM .5% 1/4W ALT - 63-10183	R470	93-922-172	2.2K OHM .5% 1/4W ALT - 63-7901
C1U	22-3729	.001 MFD DISC 50V	R122	93-921-102	2.2K OHM .5% 1/4W ALT - 63-10183	R471	93-922-180	2.2K OHM .5% 1/4W ALT - 63-7902
C1V	22-3729	.001 MFD DISC 50V	R123	93-921-103	2.2K OHM .5% 1/4W ALT - 63-10183	R472	93-922-188	2.2K OHM .5% 1/4W ALT - 63-7903
C1W	22-3729	.001 MFD DISC 50V	R124	93-921-104	2.2K OHM .5% 1/4W ALT - 63-10183	R473	93-922-196	2.2K OHM .5% 1/4W ALT - 63-7904
C1X	22-3729	.001 MFD DISC 50V	R125	93-921-105	2.2K OHM .5% 1/4W ALT - 63-10183	R474	93-922-204	2.2K OHM .5% 1/4W ALT - 63-7905
C1Y	22-3729	.001 MFD DISC 50V	R126	93-921-106	2.2K OHM .5% 1/4W ALT - 63-10183	R475	93-922-212	2.2K OHM .5% 1/4W ALT - 63-7906
C1Z	22-3729	.001 MFD DISC 50V	R127	93-921-107	2.2K OHM .5% 1/4W ALT - 63-10183	R476	93-922-220	2.2K OHM .5% 1/4W ALT - 63-7907
C20	22-4482	.001 MFD DISC 50V	R128	93-921-108	2.2K OHM .5% 1/4W ALT - 63-10183	R477	93-922-228	2.2K OHM .5% 1/4W ALT - 63-7908
C21	22-4482	.001 MFD DISC 50V	R129	93-921-109	2.2K OHM .5% 1/4W ALT - 63-10183	R478	93-922-236	2.2K OHM .5% 1/4W ALT - 63-7909
C22	22-4482	.001 MFD DISC 50V	R130	93-921-110	2.2K OHM .5% 1/4W ALT - 63-10183	R479	93-922-244	2.2K OHM .5% 1/4W ALT - 63-7910
C23	22-4482	.001 MFD DISC 50V	R131	93-921-111	2.2K OHM .5% 1/4W ALT - 63-10183	R480	93-922-252	2.2K OHM .5% 1/4W ALT - 63-7911
C24	22-4482	.001 MFD DISC 50V	R132	93-921-112	2.2K OHM .5% 1/4W ALT - 63-10183	R481	93-922-260	2.2K OHM .5% 1/4W ALT - 63-7912
C25	22-4482	.001 MFD DISC 50V	R133	93-921-113	2.2K OHM .5% 1/4W ALT - 63-10183	R482	93-922-268	2.2K OHM .5% 1/4W ALT - 63-7913
C26	22-4482	.001 MFD DISC 50V	R134	93-921-114	2.2K OHM .5% 1/4W ALT - 63-10183	R483	93-922-276	2.2K OHM .5% 1/4W ALT - 63-7914
C27	22-4482	.001 MFD DISC 50V	R135	93-921-115	2.2K OHM .5% 1/4W ALT - 63-10183	R484	93-922-284	2.2K OHM .5% 1/4W ALT - 63-7915
C28	22-4482	.001 MFD DISC 50V	R136	93-921-116	2.2K OHM .5% 1/4W ALT - 63-10183	R485	93-922-292	2.2K OHM .5% 1/4W ALT - 63-7916
C29	22-4482	.001 MFD DISC 50V	R137	93-921-117	2.2K OHM .5% 1/4W ALT - 63-10183	R486	93-922-300	2.2K OHM .5% 1/4W ALT - 63-7917
C30	22-4482	.001 MFD DISC 50V	R138	93-921-118	2.2K OHM .5% 1/4W ALT - 63-10183	R487	93-922-308	2.2K OHM .5% 1/4W ALT - 63-7918
C31	22-4482	.001 MFD DISC 50V	R139	93-921-119	2.2K OHM .5% 1/4W ALT - 63-10183	R488	93-922-316	2.2K OHM .5% 1/4W ALT - 63-7919
C32	22-4482	.001 MFD DISC 50V	R140	93-921-120	2.2K OHM .5% 1/4W ALT - 63-10183	R489	93-922-324	2.2K OHM .5% 1/4W ALT - 63-7920
C33	22-4482	.001 MFD DISC 50V	R141	93-921-121	2.2K OHM .5% 1/4W ALT - 63-10183	R490	93-922-332	2.2K OHM .5% 1/4W ALT - 63-7921
C34	22-4482	.001 MFD DISC 50V	R142	93-921-122	2.2K OHM .5% 1/4W ALT - 63-10183	R491	93-922-340	2.2K OHM .5% 1/4W ALT - 63-7922
C35	22-4482	.001 MFD DISC 50V	R143	93-921-123	2.2K OHM .5% 1/4W ALT - 63-10183	R492	93-922-348	2.2K OHM .5% 1/4W ALT - 63-7923
C36	22-4482	.001 MFD DISC 50V	R144	93-921-124	2.2K OHM .5% 1/4W ALT - 63-10183	R493	93-922-356	2.2K OHM .5% 1/4W ALT - 63-7924
C37	22-4482	.001 MFD DISC 50V	R145	93-921-125	2.2K OHM .5% 1/4W ALT - 63-10183	R494	93-922-364	2.2K OHM .5% 1/4W ALT - 63-7925
C38	22-4482	.001 MFD DISC 50V	R146	93-921-126	2.2K OHM .5% 1/4W ALT - 63-10183	R495	93-922-372	2.2K OHM .5% 1/4W ALT - 63-7926
C39	22-4482	.001 MFD DISC 50V	R147	93-921-127	2.2K OHM .5% 1/4W ALT - 63-10183	R496	93-922-380	2.2K OHM .5% 1/4W ALT - 63-7927
C40	22-4482	.001 MFD DISC 50V	R148	93-921-128	2.2K OHM .5% 1/4W ALT - 63-10183	R497	93-922-388	2.2K OHM .5% 1/4W ALT - 63-7928
C41	22-4482	.001 MFD DISC 50V	R149	93-921-129	2.2K OHM .5% 1/4W ALT - 63-10183	R498	93-922-396	2.2K OHM .5% 1/4W ALT - 63-7929
C42	22-4482	.001 MFD DISC 50V	R150	93-921-130	2.2K OHM .5% 1/4W ALT - 63-10183	R499	93-922-404	2.2K OHM .5% 1/4W ALT - 63-7930
C43	22-4482	.001 MFD DISC 50V	R151	93-921-131	2.2K OHM .5% 1/4W ALT - 63-10183	R500	93-922-412	2.2K OHM .5% 1/4W ALT - 63-7931
C44	22-4482	.001 MFD DISC 50V	R152	93-921-132	2.2K OHM .5% 1/4W ALT - 63-10183	R501	93-922-420	2.2K OHM .5% 1/4W ALT - 63-7932
C45	22-4482	.001 MFD DISC 50V	R153	93-921-133	2.2K OHM .5% 1/4W ALT - 63-10183	R502	93-922-428	2.2K OHM .5% 1/4W ALT - 63-7933
C46	22-4482	.001 MFD DISC 50V	R154	93-921-134	2.2K OHM .5% 1/4W ALT - 63-10183	R503	93-922-436	2.2K OHM .5% 1/4W ALT - 63-7934
C47	22-4482	.001 MFD DISC 50V	R155	93-921-135	2.2K OHM .5% 1/4W ALT - 63-10183	R504	93-922-444	2.2K OHM .5% 1/4W ALT - 63-7935
C48	22-4482	.001 MFD DISC 50V	R156	93-921-136	2.2K OHM .5% 1/4W ALT - 63-10183	R505	93-922-452	2.2K OHM .5% 1/4W ALT - 63-7936
C49	22-4482	.001 MFD DISC 50V	R157	93-921-137	2.2K OHM .5% 1/4W ALT - 63-10183	R506	93-922-460	2.2K OHM .5% 1/4W ALT - 63-7937
C50	22-4482	.001 MFD DISC 50V	R158	93-921-138	2.2K OHM .5% 1/4W ALT - 63-10183	R507	93-922-468	2.2K OHM .5% 1/4W ALT - 63-7938
C51	22-4482	.001 MFD DISC 50V	R159	93-921-139	2.2K OHM .5% 1/4W ALT - 63-10183	R508	93-922-476	2.2K OHM .5% 1/4W ALT - 63-7939
C52	22-4482	.001 MFD DISC 50V	R160	93-921-140	2.2K OHM .5% 1/4W ALT - 63-10183	R509	93-922-484	2.2K OHM .5% 1/4W ALT - 63-7940
C53	22-4482	.001 MFD DISC 50V	R161	93-921-141	2.2K OHM .5% 1/4W ALT - 63-10183	R510	93-922-492	2.2K OHM .5% 1/4W ALT - 63-7941
C54	22-4482	.001 MFD DISC 50V	R162	93-921-142	2.2K OHM .5% 1/4W ALT - 63-10183	R511	93-922-500	2.2K OHM .5% 1/4W ALT - 63-7942
C55	22-4482	.001 MFD DISC 50V	R163	93-921-143	2.2K OHM .5% 1/4W ALT - 63-10183	R512	93-922-508	2.2K OHM .5% 1/4W ALT - 63-7943
C56	22-4482	.001 MFD DISC 50V	R164	93-921-144	2.2K OHM .5% 1/4W ALT - 63-10183	R513	93-922-516	2.2K OHM .5% 1/4W ALT - 63-7944
C57	22-4482	.001 MFD DISC 50V	R165	93-921-145	2.2K OHM .5% 1/4W ALT - 63-10183	R514	93-922-524	2.2K OHM .5% 1/4W ALT - 63-7945
C58	22-4482	.001 MFD DISC 50V	R166	93-921-146	2.2K OHM .5% 1/4W ALT - 63-10183	R515	93-922-532	2.2K OHM .5% 1/4W ALT - 63-7946
C59	22-4482	.001 MFD DISC 50V	R167	93-921-147	2.2K OHM .5% 1/4W ALT - 63-10183	R516	93-922-540	2.2K OHM .5% 1/4W ALT - 63-7947
C60	22-4482	.001 MFD DISC 50V	R168	93-921-148	2.2K OHM .5% 1/4W ALT - 63-10183	R517	93-922-548	2.2K OHM .5% 1/4W ALT - 63-7948
C61	22-4482	.001 MFD DISC 50V	R169	93-921-149	2.2K OHM .5% 1/4W ALT - 63-10183	R518	93-922-556	2.2K OHM .5% 1/4W ALT - 63-7949
C62	22-4482	.001 MFD DISC 50V	R170	93-921-150	2.2K OHM .5% 1/4W ALT - 63-10183	R519	93-922-564	2.2K OHM .5% 1/4W ALT - 63-7950
C63	22-4482	.001 MFD DISC 50V	R171	93-921-151	2.2K OHM .5% 1/4W ALT - 63-10183	R520	93-922-572	2.2K OHM .5% 1/4W ALT - 63-7951
C64	22-4482	.001 MFD DISC 50V	R172	93-921-152	2.2K OHM .5% 1/4W ALT - 63-10183	R521	93-922-580	2.2K OHM .5% 1/4W ALT - 63-7952
C65	22-4482	.001 MFD DISC 50V	R173	93-921-153	2.2K OHM .5% 1/4W ALT - 63-10183	R522	93-922-588	2.2K OHM .5% 1/4W ALT - 63-7953
C66	22-4482	.001 MFD DISC 50V	R174	93-921-154	2.2K OHM .5% 1/4W ALT - 63-10183	R523	93-922-596	2.2K OHM .5% 1/4W ALT - 63-7954
C67	22-4482	.001 MFD DISC 50V	R175	93-921-155	2.2K OHM .5% 1/4W ALT - 63-10183	R524	93-922-604	2.2K OHM .5% 1/4W ALT - 63-7955
C68	22-4482	.001 MFD DISC 50V	R176	93-921-156	2.2K OHM .5% 1/4W ALT - 63-10183	R525	93-922-612	2.2K OHM .5% 1/4W ALT - 63-7956
C69	22-4482	.001 MFD DISC 50V	R177	93-921-157	2.2K OHM .5% 1/4W ALT - 63-10183	R526	93-922-620	2.2K OHM .5% 1/4W ALT - 63-7957
C70	22-4482	.001 MFD DISC 50V	R178	93-921-158	2.2K OHM .5% 1/4W ALT - 63-10183	R527	93-922-628	2.2K OHM .5% 1/4W ALT - 63-7958
C71	22-4482	.001 MFD DISC 50V	R179	93-921-159	2.2K OHM .5% 1/4W ALT - 63-10183	R528	93-922-636	2.2K OHM .5% 1/4W ALT - 63-7959
C72	22-4482	.001 MFD DISC 50V	R180	93-921-160	2.2K OHM .5% 1/4W ALT - 63-10183	R529	93-922-644	2.2K OHM .5% 1/4W ALT - 63-7960
C73	22-4482	.001 MFD DISC 50V	R181	93-921-161	2.2K OHM .5% 1/4W ALT - 63-10183	R530	93-922-652	2.2K OHM .5% 1/4W ALT - 63-7961
C74	22-4482	.001 MFD DISC 50V	R182	93-921-162	2.2K OHM .5% 1/4W ALT - 63-10183	R531	93-922-660	2.2K OHM .5% 1/4W ALT - 63-7962
C75	22-4482	.001 MFD DISC 50V	R183	93-921-163	2.2K OHM .5% 1/4W ALT - 63-10183	R532	93-922-668	2.2K OHM .5% 1/4W ALT - 63-7963
C76	22-4482	.001 MFD DISC 50V	R184	93-921-164	2.2K OHM .5% 1/4W ALT - 63-10183	R533	93-922-676	2.2K OHM .5% 1/4W ALT - 63-7964
C77	22-4482	.001 MFD DISC 50V	R185	93-921-165	2.2K OHM .5% 1/4W ALT - 63-10183	R534	93-922-684	2.2K OHM .5% 1/4W ALT - 63-7965
C78	22-4482	.001 MFD DISC 50V	R186	93-921-166	2.2K OHM .5% 1/4W ALT - 63-10183	R535	93-922-692	2.2K OHM .5% 1/4W ALT - 63-7966
C79	22-4482	.001 MFD DISC 50V	R187	93-921-167	2.2K OHM .5% 1/4W ALT - 63-10183	R536	93-922-700	2.2K OHM .5% 1/4W ALT - 63-7967
C80	22-4482	.001 MFD DISC 50V	R188	93-921-168	2			



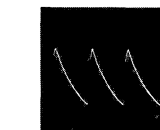
PC1 AM/FM, RF, IF & FM MPX



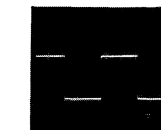
PIN 2-COMPOSITE INPUT
L+R, L-R (1 KHZ LEFT ONLY)
19 KHZ PILOT 10%
0.5V P/P (0.5 MILLISEC.)



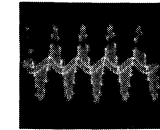
**PINS 3 AND 11-
COMPOSITE AMPLIFIED
L+R, L-R (1 KHZ LEFT ONLY)
19 KHZ PILOT 10%
1.4V P/P (0.5 MILLISEC.)**



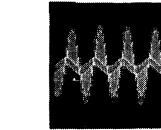
**PIN 14-VOLTAGE CONTROLLED
OSCILLATOR ADJUSTMENT
3.5V P/P (5.0 MICROSEC.)**



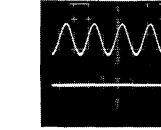
**D PIN 10-19 KHZ TEST POINT
2.7V P/P (10.0 MICROSEC.)**



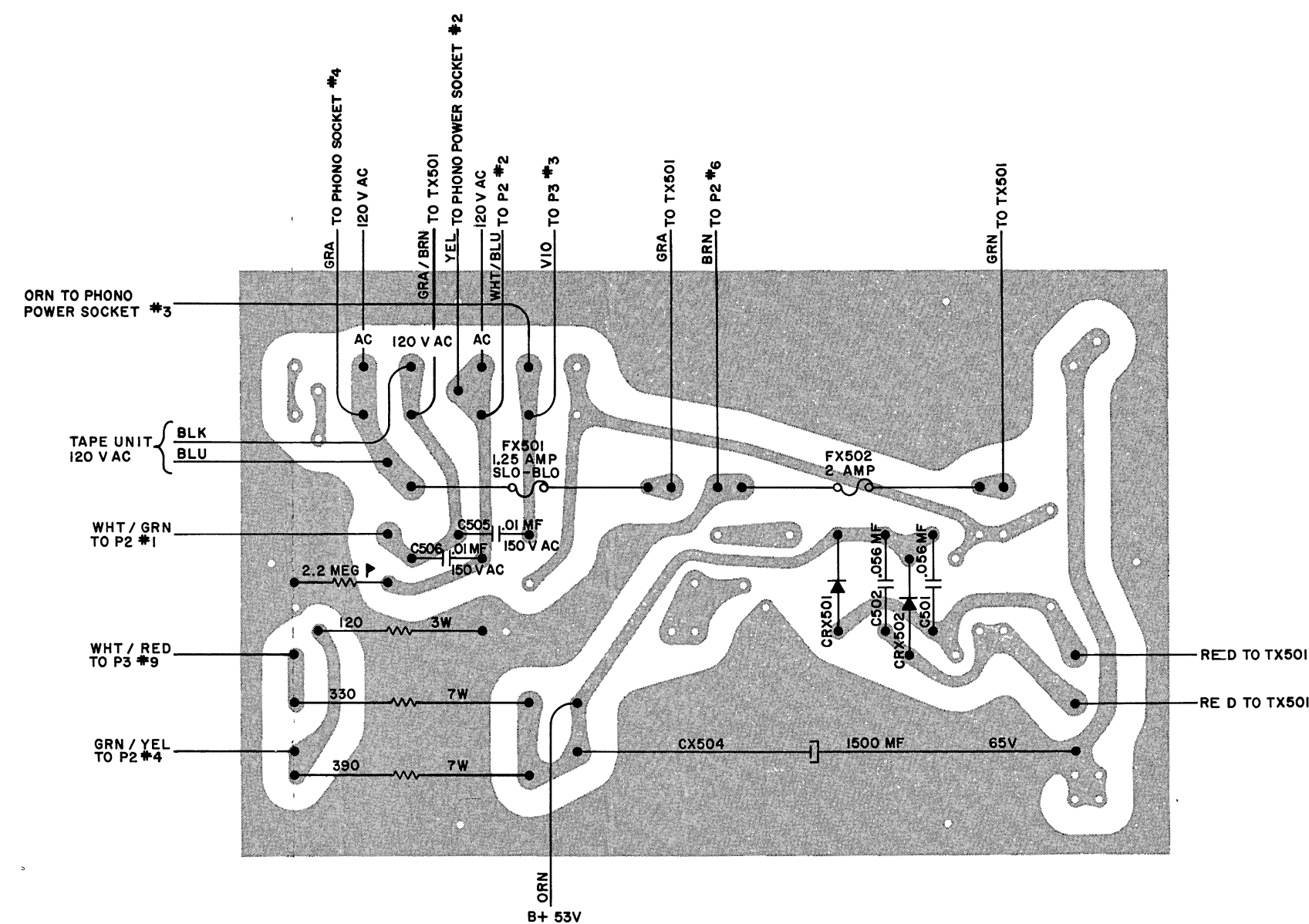
**PINS 12 AND 13-FILTER-
PHASE DETECTOR
0.14V P/P (0.5 MILLISEC.)**



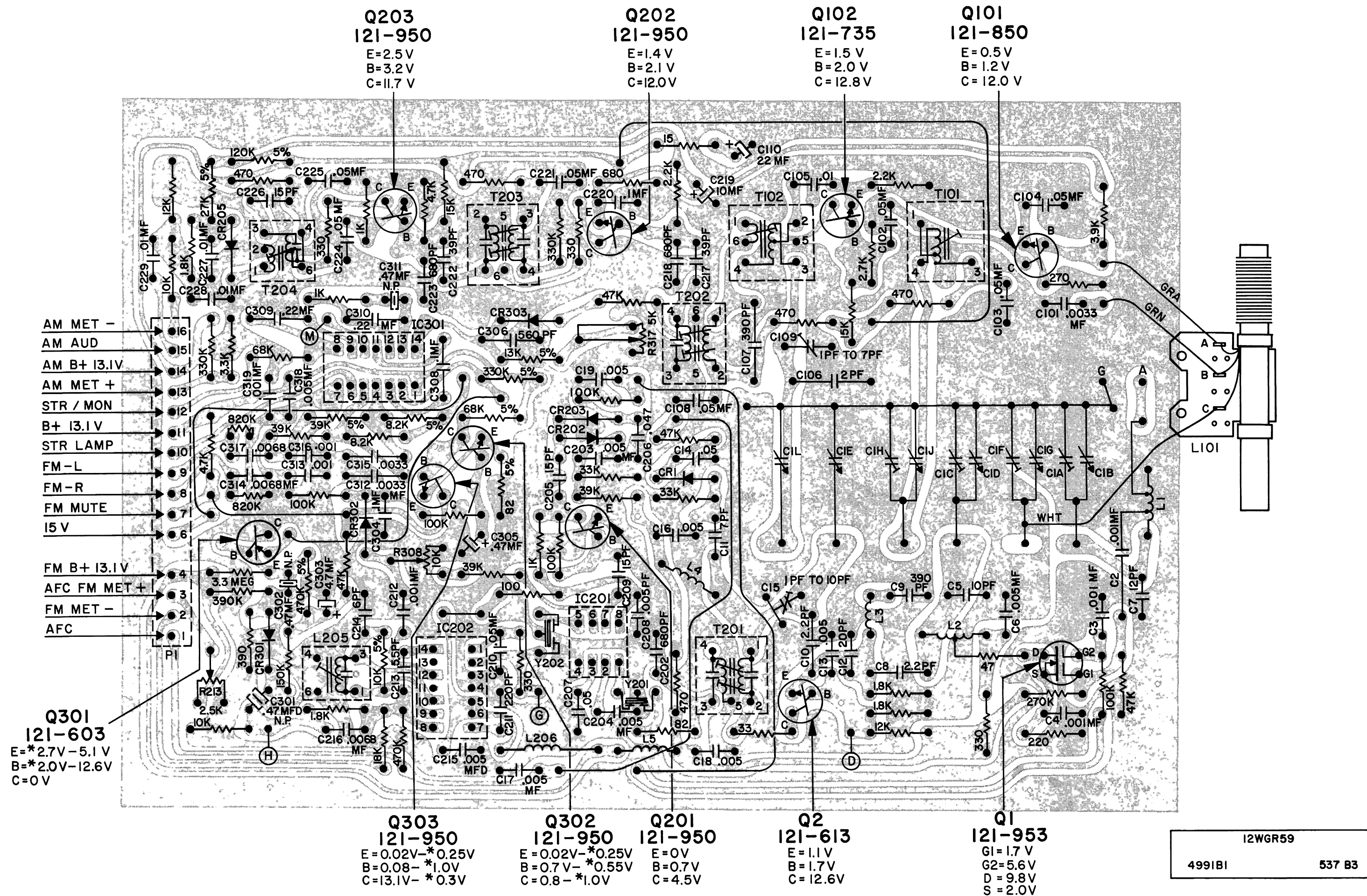
**PINS 8 AND 9-FILTER-
AMPLITUDE DETECTOR
0.47V P/P (0.5 MILLISEC.)**

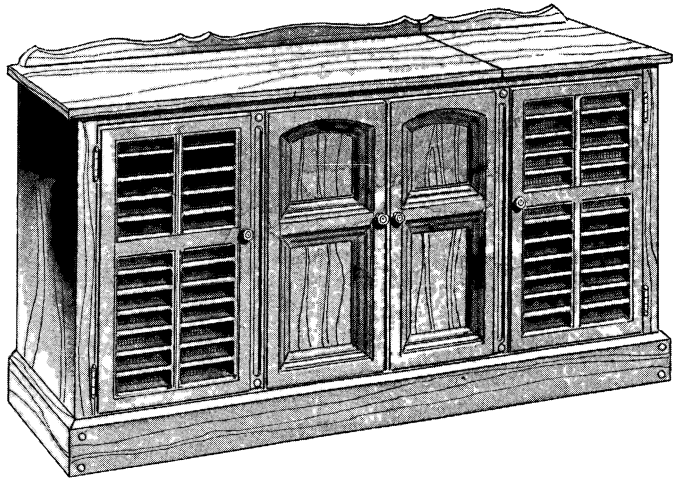


AT PLUG P1
P1, #9-(UPPER) LEFT OUTPUT
0.57V P/P (0.5 MILLISEC.)
P1, #8-(LOWER) RIGHT OUTPUT
0.05V P/P (0.5 MILLISEC.)

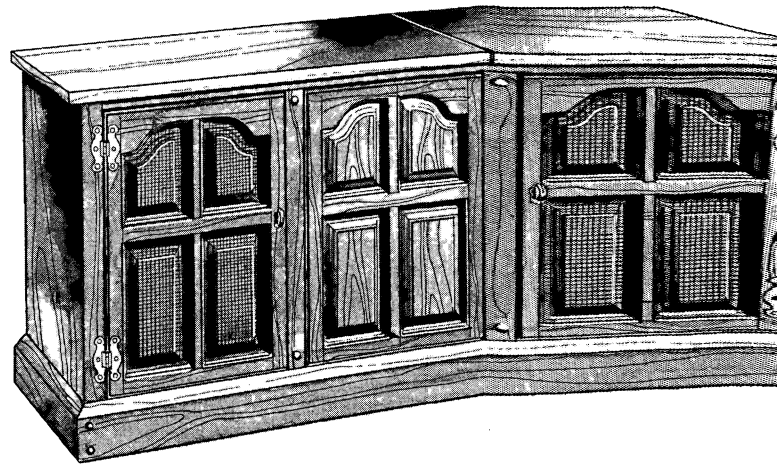


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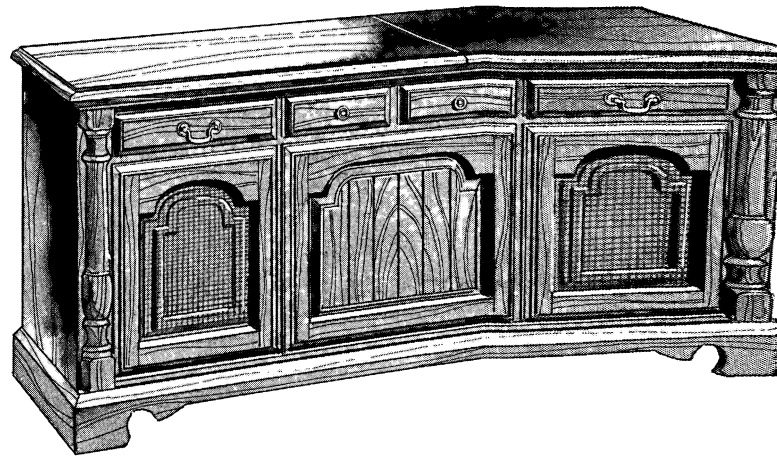




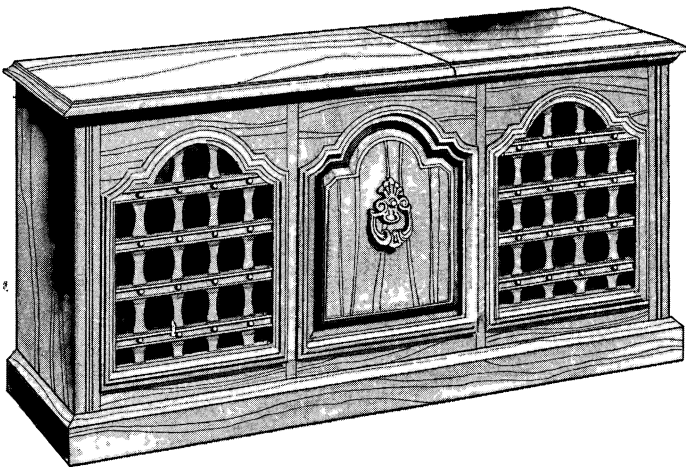
G916M



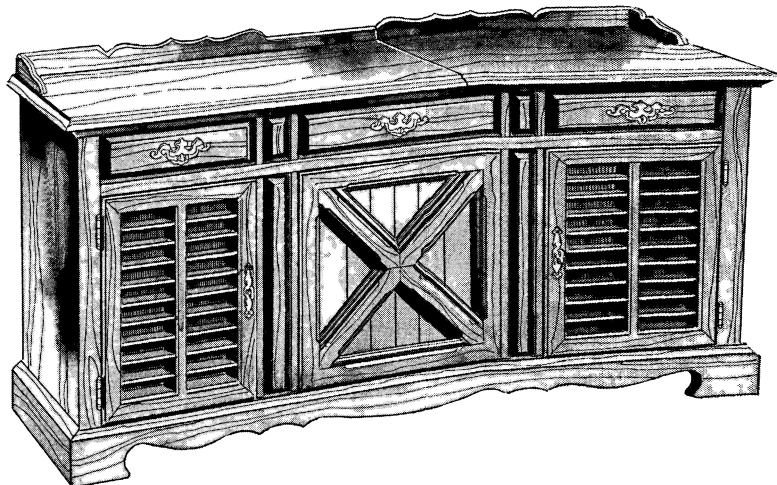
G914P



G920AE



G921P



G922M

HF-31